Power Electronics and Drives Test I

Number of Questions: 35

Section Marks: 90

Directions for questions 1 to 35: Select the correct alternative from the given choices.





Conduction Angle only extent up to

(A) $0 - \frac{\pi}{2}$ (B) $0 - \pi$ (C) $\pi - 2\pi$ (D) $0 - 2\pi$

2. With small value of Inductance in load side



Which of the following statement is correct.

- (A) i_s always present and a non-zero value.
- (B) V_0 always equal to supply voltage
- (C) I_0 always present and non zero value
- (D) free wheeling diode used for get use of trapped power in inductor, cut off the negative portion of voltage and smooth the current ripple
- 3. A single phase inverter as shown in figure below



Which of the current wave form is true





- 4. Negative triggering the gate of SCR protected by separate protection circuit because it will
 - (A) harm the thyristor life
 - (B) result in to turn off of SCR some time
 - (C) produce unpredictable operation
 - (D) produce higher loss
- - (A) SCR(B) BJT(C) MOSFET(D) GTO
- 6. A six pulse half wave rectifier converter convert two set three phase supply to a single out put. What will be the minimum current handling capacity of each diode. (Source voltage. $V_s = 100$ V) ($R_{Load} = 20$ W) (A) 5 A (B) 12.24 A
 - (A) 5 A (B) 12.24 A (C) 21.21 A (D) 7.07 A
- 7. A three phase Bridge rectifier as shown.



Which is more suitable sequence of operation for maximum out put

- (A) $D_1D_6, D_6D_3, D_3D_4, D_4D_5, D_5D_6, D_6D_3$
- (B) $D_1D_6, D_2D_1, D_2D_3, D_3D_4, D_5D_4, D_5D_6$
- (C) $D_1 D_6, D_6 D_2, D_2 D_3, D_3 D_4, D_5 D_4, D_5 D_6$
- (D) $D_1 D_6, D_1 D_2, D_2 D_3, D_3 D_4, D_5 D_1$
- 8. I_n Dual converter the reactors are connected to (A) Limit the ripples in current
 - (B) Limit the circulating current

3.142 | Power Electronics and Drives Test 1

- (C) Isolate dc component.
- (D) Make continous circuit current
- 9. In a dual converter rectifier working with $\alpha_1 = 60^\circ$ then the inverter firing angle $\alpha_2 =$

(A)
$$60^{\circ}$$
 (B) 300°
(C) 120° (D) 240°

C)
$$120^{\circ}$$
 (D) 24

10.



Each thyristor triggered using common continuous triggering signal; neutral to line voltage is 230 V. Conduction angle for switch D_1 is (B) 120°

(D) 90°

(A) 0° (C) 180°

11.



The circuit as shown with duty cycle of switch, D = 0.5will follow

- (A) unity voltage ripple factor
- (B) voltage ripple factor more than unity
- (C) voltage ripple factor less than unity
- (D) No ripples

12.



The circuit having chopping frequency of 1500 Hz. What will be the maximum ripple current flow through the inductor

- (A) 0.0116
- (B) 7.5×10^{-3} A
- (C) 0.0212 A

(D) 0.015 A

13.

14.



6 identical switches of forward voltage handling capability of $V_{\text{max}} = 400_{\text{rms}}$

(B) 480 KW

(D) 80 KW

$$i_{\rm max} = 100 \, {\rm A}_{\rm rms}$$

The circuit has peak power handling capacity of

(C) 169.7 KW



A single phase DC motor drive as shown which of the following is right for the circuit on the assumption of La>>ra.



15. A thyristor controlled induction motor working at a slip of 0.02 fed from voltage controlled source inverter as shown



Operated at 50 Hz, 6 pole machine. The speed of rotor will be **20.**

(A)	1000 rpm	(B)	2940 rpm
(α)	000		2000

(C) 980 rpm (D) 3000 rpm





Having $L = 20 \mu$ H and $C = 50 \mu$ F, $V_c = V_s$ for a constant load current of 100 A. What will be turn off time for main thyristor T_m

(A)	125µs	(B)) 10	ms
· /	•			

- (C) 25 ms (D) 100µs
- 17. A simple load commutation circuit as shown in figure



works for a long time after 3 years the internal voltage of battery change by the function

 $E_{\text{Battery}} = (20 - 1.2 \times \text{years}) \text{ volt}$

What will be the present triggering angle for continuous gate triggering mode.

- (A) 9.44° (B) 11.54°
- (C) 13.65° (D) 0°
- 18. Inverter controlled with pwm method with pulse width of 160° in each half cycle. What will be the total harmonic distortion (THD)

19.



What will be the value of power dissipated in the resistor

(A)	33 w	(B)	66.2 w

(C) 40.5 w (D) 63.6 w



Inverter arrangement as shown in figure having $V_s = 100$ A and R = 10 W what will be the maximum value of 5th harmonic component.

(A)	2.54 A	(B)	12.56 A
(C)	0 A	(D)	20.12 A

21. A three phase 120 degree mode voltage source inverter connected to a resistive inductive load, $R = 10 \Omega$, $L = 200 \mu$ H. What will be the load power if inverter source voltage is 100 V dc.

(A)	166 W	(B)	500	W
(C)	866 W	(D)	288	W

22. A circuit as shown in figure triggered by resistance firing circuits



Thyristor rating of
$$I_L = 200 \text{ mA}$$

 $I_H = 180 \text{ mA} V_{g \text{ max}} = 20 \text{ V}$
 $V_{g \text{ min}} = 15 \text{ V} R_{2 \text{ min}} = 5 \text{ K} \Omega$
 $R_{2 \text{ max}} = 5.666 \text{ K} \Omega$
What will be the value of R_1 for sure turn ON of SCR at $\omega t = 45^{\circ}$

(A)
$$555.55 \Omega$$
 (B) 823.57Ω

(C)
$$1.1 \text{K} \Omega$$
 (D) 932.29Ω

23.



Commutation circuit as shown in figure having L = C = 1 m units and $V_c = 120$ V maximum voltage a capacitor can store. What will be the minimum current main thyristor can be handling.

(A)	120 A	(B)	80 A
(C)	200 A	(D)	240 A

3.144 | Power Electronics and Drives Test 1

24. A voltage source inverter arrangement as shown figure.



Operated in 180° mode, 50 Hz the peak to peak value of I_0 will be

(A)	5 A	(B)	2.5 A

- (C) 10 A (D) 0 A
- **25.** A separately excited dc motor has rated armature current of 25 A and rated armature voltage 180 V. The power supplied by a step down chopper at a switch frequency of 5 KHz used to control armature voltage. Neglecting all the losses $L_a = 0.2$ mH armature resistance $Ra = 1 \Omega$ Duty ratio of the chopper to obtain 60% rated torque at rated speed and the rated field current is ______



- **26.** A single phase bridge inverter fed from 100 V dc connected to *RL* load of $R = 5 \Omega \& L = 0.01$ H determine the current of 5th harmonic content when inverter operated at 50 Hz two pulse PWM method of $d = 45^{\circ}$ (A) 2.82 A (B) 2 A
 - $\begin{array}{c} (A) & 2.02 \ A \\ (C) & 1 \ A \\ \end{array} \qquad \begin{array}{c} (D) & 2.6 \ A \\ (D) & 5.6 \ A \end{array}$
- 27. The chopper circuit as shown the thyristor T operated at a duty ratio of 0.8 What will be the value of critical
- at a duty ratio of 0.8. What will be the value of critical inductance L for which the current falls to zero



28. A boost converter feeds a resistive load from a battery source. Switch is operated at 5000 Hz with duty ratio of 0.4



What will be the average source current in steady state(A) 4.16 A(B) 0.66 A(C) 3 A(D) 1.851 A

29. A type – A chopper circuit source voltage $V_s = 200$ V chopping frequency 500 Hz Duty cycle D = 0.3



The maximum current *i* is

(A)	21.799 A	(B)	34.2 A
(C)	87.5 A	(D)	26.25 A

30. A 120 kW, 400 V, 1800 rpm separately excited dc motor is energized by $420 V_L$, 50 Hz three phase source through three phase semi converter. The voltage drop in brushes and thyristor are 5V



At no load armature current of 25 A what will be the no load speed at firing angle of 45°.





A 10 volt pulse generator made by using GTO L = 0.1H., $C = 10 \mu$ F.

Power Electronics and Drives Test 1 | 3.145

Consider all devices are ideal what will be the frequency of output pulses.

(A)	2214.5 Hz	(B)	322.5 Hz
(C)	1121.3 Hz	(D)	159.2 Hz

Common data Questions 32 and 33:

A single phase half wave converter with RLE load as shown



Conduction extent up to 200°

32. The average load voltage is (if continuous gate pulses given to SCR).

(A)	80.34 V	(B)	78.79 V
(C)	68.52 V	(D)	72.41 V

33. Circuit conduction time of the circuit (A) 0.05 s (B) 0.02 s (C) 0.01 s (D) 0.6 s

Linked Answer Questions for 34 and 35:

- 34. A single phase inverter operated at single pulse PWM method $2d = 72^{\circ}$; N = 1. The 3rd and 5th frequency component voltages are (A) 0.4 V; 0 V (B) $0.285 V_s; 0.4 V_s V$
 - (D) $0.3 V_s, 0 V$ (C) 0.2854 V, 0 V
- 35. The inverter replaced with N = 2, two pulse width modulation.

The percentage change in third harmonics is $V_{03_{rms}N=1} - V_{03_{rms}N=2} \times 100$

				Ansv	VER KEYS					
1. B	2. D	3. C	4. B	5. C	6. D	7. B	8. B	9. C	10. D	
11. A	12. D	13. B	14. B	15. C	16. D	17. A	18. B	19. B	20. A	
21. B	22. B	23. C	24. A	25. A	26. B	27. C	28. D	29. A	30. A	
31. D	32. B	33. C	34. C	35. B						

HINTS AND EXPLANATIONS

1. The output current wave form of RLC circuit will be an AC



Conduction extent; when current was in forward direction ie, $0 - \pi$

 $\pi - 2 \pi$ direction was opposite

that is, diode only conducts $0 - \pi$.	Choice (B)
--	------------

2. More accurate answer is Choice (D)

3. The output voltage wave form



at
$$D_1 D_3$$
 Path
 $I = \frac{+V_s}{L} \times t + I_{initial} (-ve)$

$$I_{\max} = \frac{V_s}{L} \times T + I_{\text{initial}} (-ve)$$

At $D_2 D_4$ Path
 $I_{\max} = \frac{-V_s}{L} \times T + I_{\text{initial}} (+ve)$

So Choice (C) is correct.

- 4. Choice (B)
- 5. Choice (C)
- 6. For 6 pulse operation at a time one switch is closed. The maximum output switch can give when it is closed.

At
$$\alpha \le 90 \pm \frac{180}{2n} \le \alpha$$

 $\le 90 \pm \frac{180}{12}$ (:: $n = 6$)

 $75 \le \alpha \le 105$ i.e., The maximum current

$$=\frac{V_m}{R}=\frac{\sqrt{2\times100}}{20}=7.07\,A$$

Choice (C)

3.146 | Power Electronics and Drives Test 1

For maximum current of 7.07 Ampere, the diode should have minimum current handling capacity of 7.071 Ampere Choice (D)

7. For maximum output at a time two phases conducts and each set conducts for $\frac{360}{6}$ and each diode $\frac{360}{3}$ degree



- 8. Choice (B)
- 9. For a dual converter firing angle are related by $\alpha_1 + \alpha_2 = 180^\circ | \alpha_1 = 60^\circ$ $\alpha_2 = 180 - \alpha_1 = 120^\circ$. Choice (C)
- **10.** We can remove Diode from this circuit. Diode has no role in conduction

 V_a , V_b , V_c each are more positive $0 - 120^\circ$, $120 - 240^\circ$, $240 - 360^\circ$ respectively

$$V_A = \sqrt{2} \times 230 \sin \omega t$$

$$V_B = \sqrt{2} \times 230 \sin (\omega t - 120)$$

$$D_1 \text{ is forward bias}$$

When $V_m \sin \theta > 230$

$$\sqrt{2} \times 230 \sin \theta > 230$$

$$\theta > 45^{\circ}$$

1

i.e., D_1 forward bias from 45° to 135°



Conduction Angle will be $135^{\circ} - 45^{\circ} = 90^{\circ}$.

1. Voltage ripple factor =
$$\sqrt{\frac{V_{rms^2} - V_{av^2}}{V_{av^2}}}$$

 $V_{av} = \alpha V_s; V_{rms} = \sqrt{\alpha}V_s$
 $V.R.F = \sqrt{\frac{aV_s^2 - a^2V_s^2}{a^2V_s^2}} = 1$
 $\alpha = D = 0.5$ Choice (A)

2. Ripple =
$$\Delta I$$

 $\Delta I_{max} = \frac{V_s}{R} \tan h \left(\frac{R}{4fL} \right)$ here $4fL >> R$
Then $\frac{R}{4fL} \rightarrow 0$
 $\Delta I_{max} = \frac{V_s}{R} \times \frac{R}{4fL}$
 $\Delta I_{max} = \frac{V_s}{4fL}$
i.e., $\Delta I_{max} = \frac{V_s}{4fL} = \frac{90}{4 \times 1500 \times 1}$
 $= 0.015$ A. Choice (D)

1

$$V_{\text{peak}} = 3 V_{\text{max peak}} = 3 \times \sqrt{2} \times 400$$

= 1697.056 V

$$= 1697.056 \text{ V}$$

$$I_{\text{peak}} = 2 I_{\text{max peak}}$$

$$= 2 \times 100 \times \sqrt{2} = 282.84 \text{ A}$$
Peak power = $V_{\text{max}} I_{\text{peak}}$

$$= 480 \text{ KW.}$$
Choice (B)

- 14. Option (b) right; every motor is working under the condition of $L_a >> r_a$ internal resistance of motor very less. High inductance oppose ripple. Choice (B)
- 15. The machine operated at 50 H_z .

Synchronous speed N_s i.e. $N = \frac{120f}{1000} = 1000$

.e.,
$$N_s = \frac{1}{8} = 1000 \text{ rpm}$$

A slip of S = 0.02 $N_r = (1 - S) N_s = 980$ rpm.

Choice (C)

16. Circuit turn off time for main thyristor $I = c \frac{dV_c}{dt}$ at voltage commutation for constant current I_0 ;

i.e.,
$$I_0 = c \frac{V_c}{t}$$

Power Electronics and Drives Test 1 | 3.147

When
$$V_c = V_s$$
; turn off the switch $I_0 = c \frac{V_s}{t}$
 $t = c \frac{V_s}{I_0} = 50 \mu \times \frac{200}{100} = 100 \mu s.$ Choice (D)

17. The SCR is at a state of continuous triggering mode so SCR will ON at forward bias condition. i.e., 100 sin $\omega t \ge E$ Battery voltage After 3 year $E_{3year} = 20 -1.2 \times 3 = 16.4$ Volt $\omega t = \sin^{-1}\left(\frac{16.4}{100}\right) = 9.439^{\circ}$

SCR ON after 9.439° to $(180^{\circ} - 9.439^{\circ})$ triggering Angle = 9.439° . Choice (A)

18. THD =
$$\frac{\sqrt{V_{rms}^2 - V_1^2}}{V_1}$$
; $2d = 160^\circ$

 $d = 80^{\circ}$ $V_1 =$ rms fundamental frequency signal

$$V_{0} = \sum_{n=1,3,5}^{\infty} \frac{4V_{s}}{n\pi} \sin \frac{n\pi}{2} \sin nd \sin n\omega t$$

$$V_{1} = \frac{4V_{s}}{\pi} \sin 80^{\circ} \sin n\omega t$$

$$(V_{1})_{rms} = \frac{1.2538}{\sqrt{2}} V_{s}$$

$$(V_{1})_{rms} = 0.8866 V_{s}$$

$$V_{rms} = \sqrt{\frac{1}{\pi} \frac{\pi^{\frac{\pi}{2}+d}}{\int_{-d}}} V_{s}^{2} d\omega t$$

$$= V_{s} \sqrt{\frac{2d}{\pi}} = 0.9428 V_{s}$$

$$THD = \frac{\sqrt{(0.9428V_{s})^{2} - (0.8866V_{s})^{2}}}{0.8866V_{s}} = 0.3617.$$
Choice (B)

19. The switch forward bias when 200 sin $\omega t > 30$ V

$$\omega t = \sin^{-1} \left(\frac{30}{200} \right) = 0.1505 \text{ rad}$$

= $\frac{200 \sin \omega t - 30}{100}$
 $I_{rms} = \sqrt{\frac{1}{2\pi} \int_{0.1505}^{\pi - 0.1505} \left(\frac{200 \sin \omega t - 30}{100} \right)^2 d\omega t} = 0.8133 \text{ A}$
Power dissipated across resistance of 100 Ω
is = $I^2 R = 0.8133^2 \times 100 = 66.159 \text{ W}.$ Choice (B)

20. The output wave form is like



The fourier series representation of above output voltage.

$$V_{0} = \sum_{n=1,3,5}^{\infty} \frac{4 V_{s}}{n\pi} \sin n \omega t$$

$$I_{0n} = \frac{V_{0n}}{R} \quad I_{5} = \frac{V_{05}}{R}$$

$$= \frac{4 V_{s}}{5\pi \times 10} \sin 5 \omega t \quad I_{5_{max}} = \frac{4 \times 100}{5\pi \times 10} = 2.5464 \text{ A.}$$
Choice (A)

21. The average voltage across the inductor for a complete cycle is zero and also the power dissipated across inductor per cycle is zero So,

The load power only due to resistor
$$\frac{P}{phase} = \frac{\left[V_{phase}\right]^2}{R}$$

 $\frac{V_{rms}}{phase} = 0.4082 V_s = \frac{V_s}{\sqrt{6}} = 40.82 \text{ volt}$
 $\frac{power}{phase} = \frac{(40.82)^2}{10} = 166.62 \text{ Watt}$
for 3 phases = $166.62 \times 3 \approx 500 \text{ Watt.}$ Choice (B)
22. For sure turn ON triggering I_g should be I_{gmax} only when $V_g = V_{gmax} = 20 \text{ V}$
i.e., $V_{R1} = 200 \sin \omega t \left[1 - \frac{R_2}{R_1 + R_2}\right]$
 $\omega t = 45^\circ$
 $20 = 200 (\sin 45^\circ) \left[1 - \frac{5K}{5K + R_1}\right]$
 $R_1 = 823.57\Omega$. Choice (B)
23. $V_c = 120 \text{ V}$

The current through the capacitor $I_c = V_c \sqrt{\frac{C}{L}} \sin \omega_0 t$

$$= 120 \sqrt{\frac{1\mu}{1\mu}} \sin \omega_0 t = 120 \sin \omega_0 t$$

$$I_T \max = 120 + 80$$

$$I_{Tm} = 200 \text{A}$$
Choice (C)

24. A voltage source inverter load current through inductor

is
$$V = L \frac{di}{dt}; \int di = \int \frac{V}{L} dt$$

for 50 Hz $\frac{T}{2}$ time current flow in one direction of slope and another $\frac{T}{2}$ time other direction of slope

$$T = \frac{1}{50} = .02 \text{ sec} \quad \frac{T}{2} = 0.01 \text{ sec}$$

$$I_{\text{max}}$$

$$I_{$$

25.
$$V_a = E_b + I_a R_a$$

 $180 = E_b + 25 \times 1$
 $E_b = 155 \text{ V}$
60% rated torque
 $I = 0.6 \times 25 = 15\text{ A}$
 $V_a = 155 + 15 \times 1 = 170 \text{ V}$
 $D = \frac{V_0}{V_s} = \frac{170}{250} = 0.68$ Choice (A)

26. For two pulse PWM method

$$V = \sum_{n=1,3,5...}^{\infty} \frac{8 V_s}{n\pi} \sin n\gamma \sin \frac{nd}{2} \sin n\omega t$$

Here $= d = 45^{\circ}$
i.e., $\gamma = \frac{\pi - 2d}{N + 1} + \frac{2d}{2N}$
 $N = 2$ pulse
 $\gamma = \frac{180 - 90}{3} + \frac{45}{2}$
 $\gamma = 52.5^{\circ}$
 $V_5 = \frac{8 \times 100}{5 \times \pi} \left[\sin\left(\frac{5 \times 45}{2}\right) \sin(5 \times 52.5) \sin 5\omega t \right]$
 $Z_n = \sqrt{R^2 + (nj\omega L)^2}$
 $= \sqrt{5^2 + (5 \times 2 \times \pi \times 50 \times 0.01)^2} = 16.484$
 $V_5 = -46.65 \sin \omega t$
 $i_5 = \frac{V_5}{Z_5} = \frac{-46.65 \sin 5\omega t}{16.484}$
 $|i_{5 \,\text{rms}}| = \frac{2.829}{\sqrt{2}}$ Amps $\approx 2A$. Choice (B)

27. For dc - dc converter the critical inductance value.

$$L = \frac{(V_s - V_0)}{2f V_s P_0} V_0^2$$

$$V_0 = \alpha V_s = 0.8 \times 100 = 80 \text{ V}$$

$$I_0 = 2A$$
Power $P_0 = V_0 I_0 = 160 \text{ Watt}$

$$f = 500$$

$$L = \frac{(100 - 80)}{2 \times 500 \times 100} \times \frac{80^2}{80 \times 2}$$

$$= 8 \times 10^{-3} H = 8 \text{ mH}.$$
Choice (C)

28. In a Boost converter the average current through capacitor is zero.

$$V_0 = \frac{V_s}{1 - D} = 38.33$$
V

When switch is closed then $|\mathbf{I}_c| = |\mathbf{I}_0|$

When switch is open

$$I_{s} = I_{c} + I_{0}$$

$$I_{c} = I_{s} - I_{0}$$
Average current through capacitor = 0
 $(-I_{0}) \times DT + (I_{s} - I_{0})(1 - D)T = 0$
 $I_{0} = (1 - D)I_{s}$
 $I_{s} = \frac{I_{0}}{1 - D}$
 $I_{0} = \frac{V_{0}}{R}$
 $I_{s} = \frac{V_{0}}{(1 - D)R} = \frac{V_{s}}{(1 - D)^{2}R} = 1.851 \text{ A.}$ Choice (D)
29. $I_{max} = \frac{V_{s}}{R} \left[\frac{1 - e^{\frac{-T_{m}}{T_{a}}}}{1 - e^{\frac{-T}{T_{a}}}} \right] - \frac{E}{R}$
 $T_{a} = \frac{L}{R} = \frac{10 \times 10^{-3}}{2} = 5 \times 10^{-3}$
 $T_{on} = 0.3 \times T$
 $= 0.3 \times \frac{1}{500} = 6 \times 10^{-4} \text{ s}$
 $E = 25$
 $R = 2$
 $I_{max} = 21.799 \text{ A.}$ Choice (A)
30. Converter $O/P: K = 1.8 \text{ Vs/rad}$
 $Ra = 0.1 \Omega$
 $V_{av} = \frac{3 V_{ml}}{2\pi} (1 + \cos a); \alpha = 45^{\circ} = 484.134 \text{ V}$
Converter motor equation.
 $484.134 = E_{a} + I_{a}r_{a} + 5$
 $= K\omega_{m} + 25 \times .1 + 5$

$$\omega_m = 264.79 = \frac{2\pi N_s}{60}$$

 $N_s = 2528.6 \text{ rpm}$

Choice (A)

31. Here all devices are ideal GTO is the device closed when positive gate current applied on gate and off when negative gate current applied i.e., Gate circuit



Voltage across the capacitor $V_c = \frac{1}{c} \int i dt$

$$I_{c}(t) = V_{s}\sqrt{\frac{C}{L}} \sin \omega t$$

$$V_{s} = 10 \text{ V} \omega = \frac{1}{\sqrt{LC}}$$

$$L = 0.1 Hf = \frac{1}{2\pi\sqrt{LC}} = 159.15 \text{ Hz}$$

$$C = 10 \ \mu\text{F} \omega = 1000$$

$$i_{c \max}(t) = 0.1 \text{ Amps}$$

$$i_{c}(t) = 0.1 \sin 1000 t$$

$$V_{c} = \frac{1}{c} \int i \ dt$$

$$= \frac{-1}{c} V_{s} \times \sqrt{\frac{C}{L}} \cdot \cos \omega t \times \omega$$

$$= -V_{s} \cos \omega t$$

 V_c is the voltage for gate triggering. The frequency of gate signal is the frequency of switch ON and OFF. i.e., out put signal frequency is

 $f = 159.15, \cong 159.2 \text{ Hz}$ Choice (D)

32.
$$V_{0} = \frac{1}{2\pi} \begin{bmatrix} V_{m} (\cos a - \cos \beta) \\ + E (2\pi + a - \beta) \end{bmatrix}$$
$$a = \sin^{-1} \left(\frac{E}{V_{m}} \right)$$
$$= \sin^{-1} \left(\frac{24}{220} \right) = 6.2629^{\circ}$$
$$\beta = 200^{\circ}$$
$$V_{0} = 78.791 \text{ V.}$$
Choice (B)

33. The circuit on form α to β $\alpha \le \omega t \le \beta$

$$t_{\rm on} = \frac{\beta - a}{\omega}$$

$$V_{0} = \frac{4 V_s}{\pi} \sum_{n=1,3,5}^{a} \frac{\sin n\omega t}{n} \text{ is the standard output}$$
Single PWM
$$V_{0n} = \frac{4 V_s}{\pi} \sum_{n=1,3,5}^{\infty} \frac{\sin n\pi}{n} \text{ is the standard output}$$

$$V_{0n} = \frac{4 V_s}{\pi} \sum_{n=1,3,5}^{\infty} \left(\sin \frac{n\pi}{2} \sin nd \sin n\omega t \right) \frac{1}{n}$$

$$V_{03_{ms}} = \frac{4 V_s}{\sqrt{2} \times 3\pi} [-0.951056] = 0.2854 V_s$$

$$V_{05} = \frac{4 V_s}{\sqrt{2} \times 5\pi} [-1 \times \sin 0] = 0V$$
Choice (C)

35. $N = 2, 2d = 72^{\circ}$

ton = 0.01076 s

Multi pulse modulation $D = 36^{\circ}$

$$V_{0}$$

$$V = \frac{2 \times 4V_{s}}{\pi} \sum_{n=1,3,5}^{\infty} \left(\sin n\gamma \sin \frac{nd}{2} \sin n\omega t \right) \times \frac{1}{n}$$

$$V = \frac{\pi - 2d}{N + 1} + \frac{d}{N}$$

$$= \frac{180 - 72}{3} + \frac{36}{2} = 54^{\circ}$$

$$V_{03_{rms}} = \frac{8V_{s}}{\sqrt{2} \times 3\pi} \left[\sin (3 \times 54) \sin \frac{3 \times 36}{2} \right]$$

$$= 0.15005 V_{s}$$
Percentage change
$$= \frac{V_{03_{rms}} - V_{03_{rms}}}{V_{03_{rms}}} \times 100$$

$$=\frac{(0.2854-0.15)V_s}{0.2854V_s} \times 100 = 47.42\%$$

Choice (B)