

## "Cams"

Cams:- A cam is rotating or reciprocating member of a mechanism used to impart rotating, reciprocating or oscillating motion to another member called follower through direct contact.

→ Cam and Follower constitutes a higher pair.

Necessary elements of a Cam mechanism are.

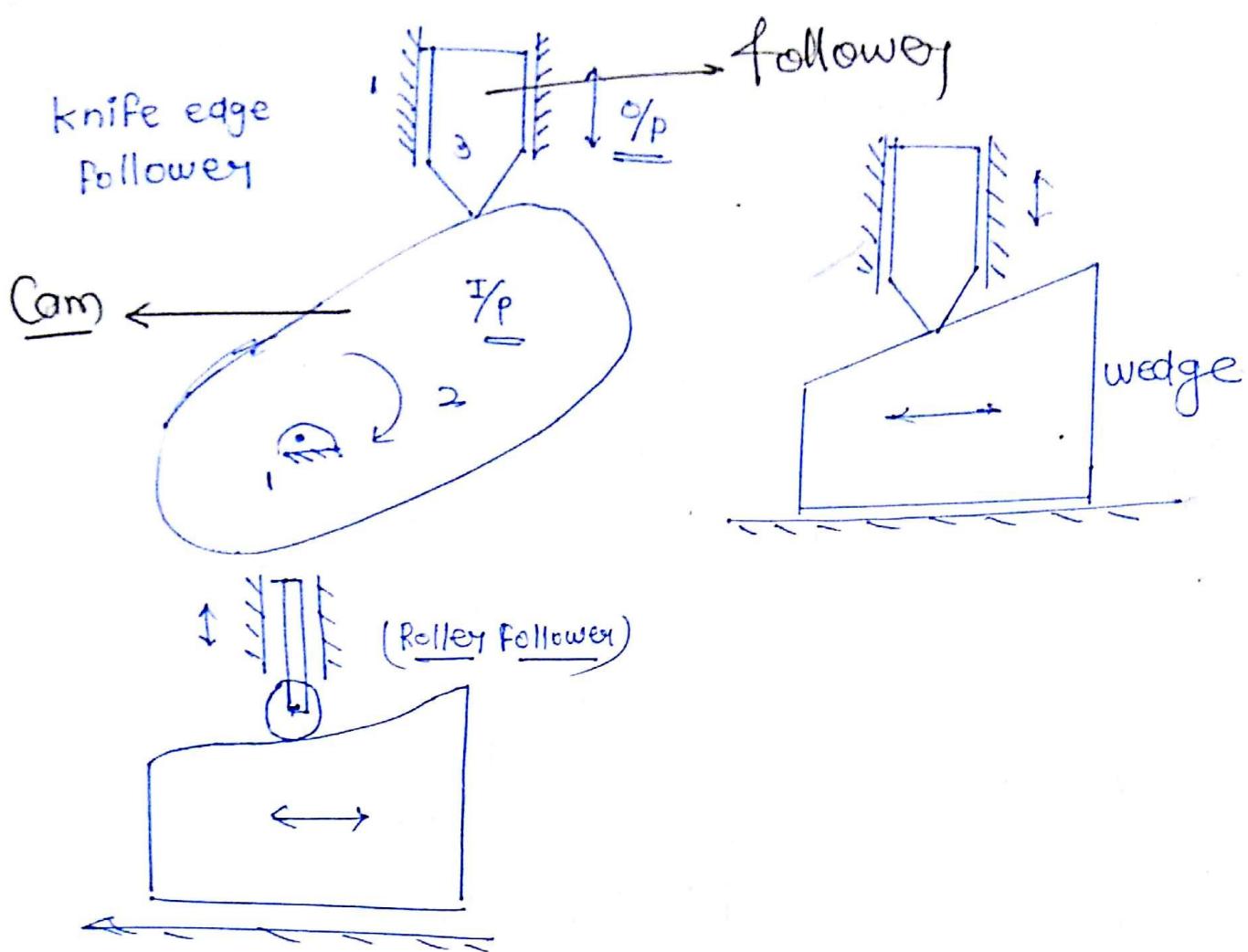
- (1) A driver member called Cam
- (2) A driven member called follower.
- (3) A frame which supports the cam and guides the follower

### Advantages

- ① less space required than the lower pair adjustment
- ② Input & output link are directly connected so has to govern the motion of O/P & only single Y/P have to be designed.

### Disadvantage

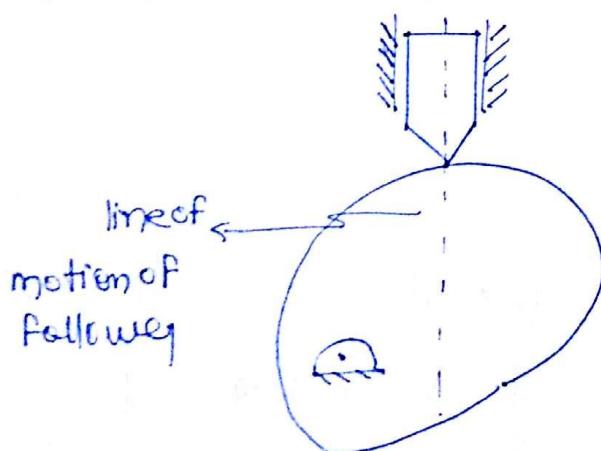
- ① No reversible
- ② High wear, because area of contact where friction force is acting is very small



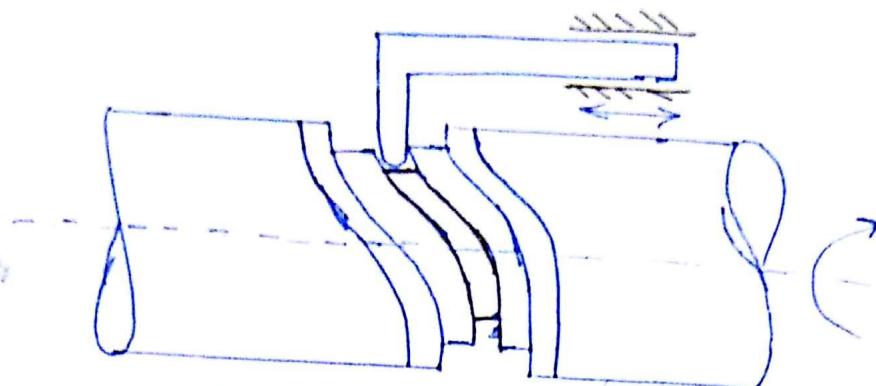
- Types of cams
- Types of follower

⇒  
Types of Cams:-

- i) Radial/Disc Cam: - line of motion of follower is  $\perp$  to the axis of rotation of cam.

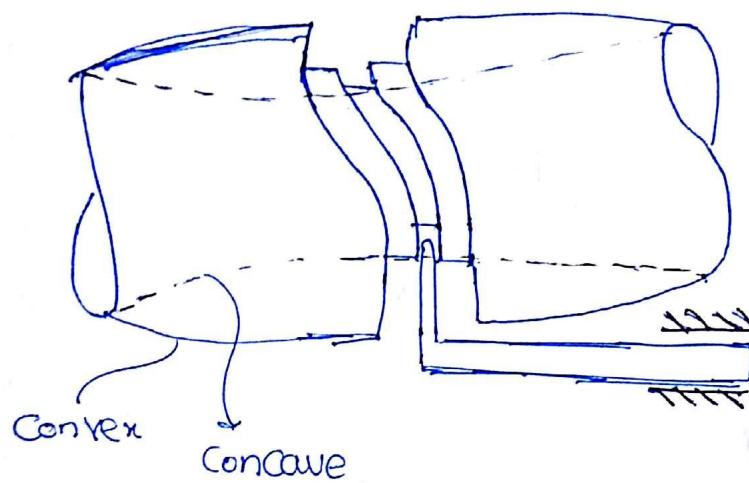


(ii) Cylinder Cam:- line of moment/motion of follower is parallel to the axis of rotation of cam.



Giboidal Cam

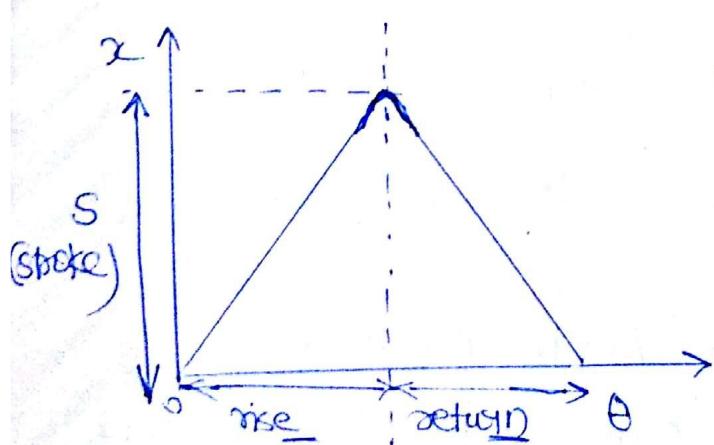
Concave  
Convex



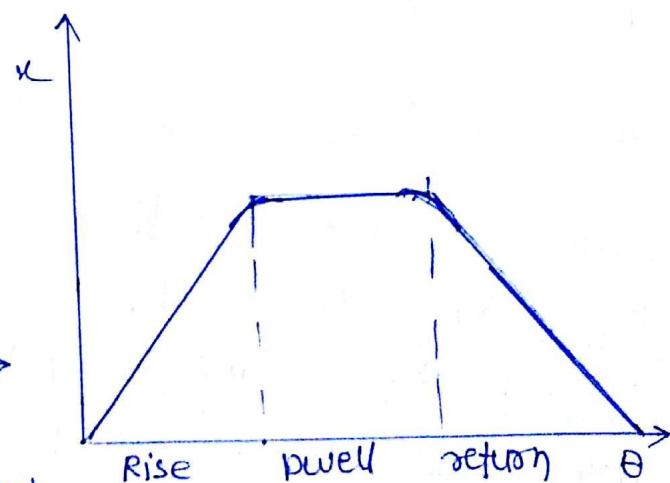
According to Follower ~~movement~~ movement:-

i) Rise- Return Cam:-

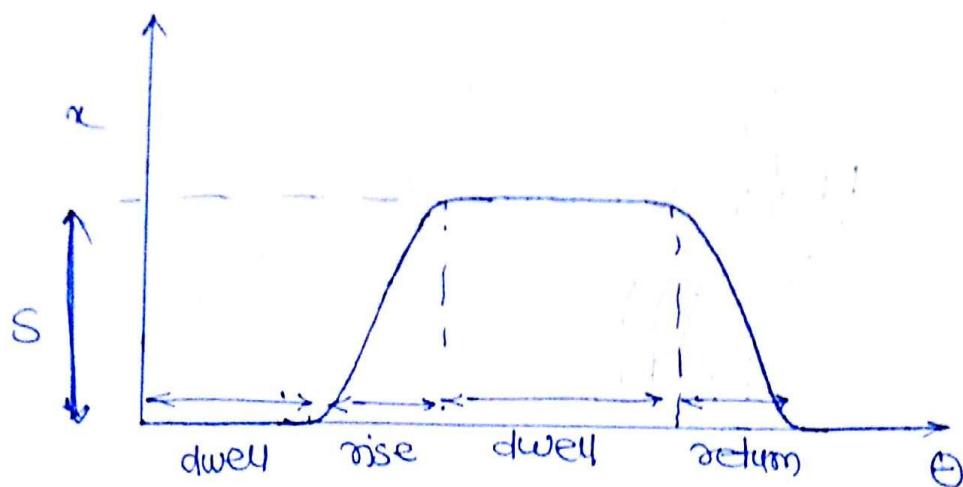
ii) Rise- Dwell - Return Cam:-



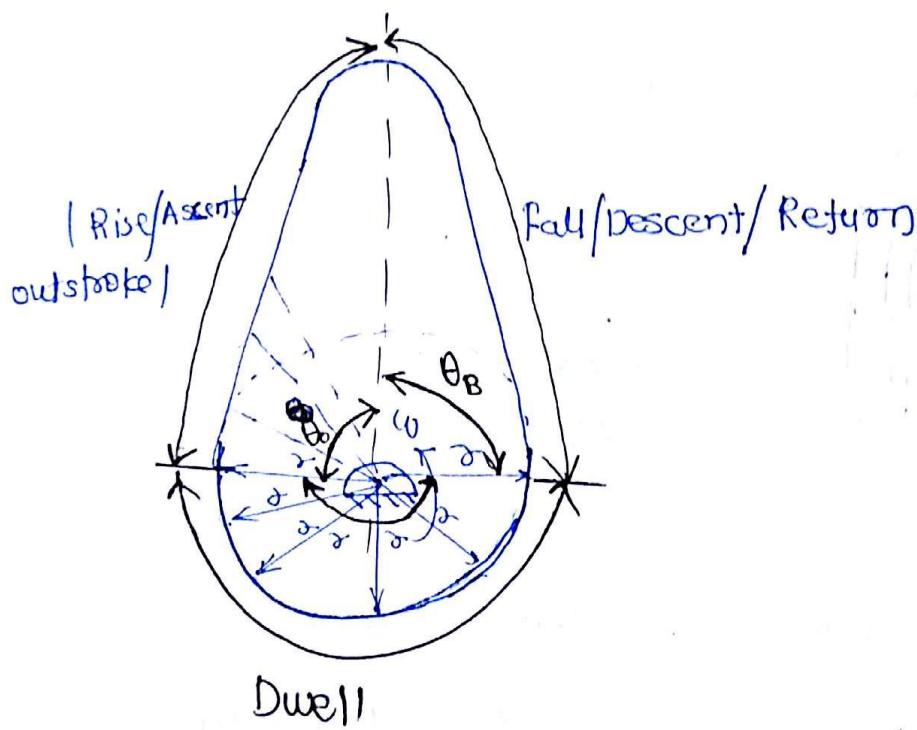
$x$  - follower displacement  
 $\theta$  - Angle of Cam rotation.



(iii) Dwell - rise - dwell - return cam :-



\*



Angles of Cam :-

1) Outstroke Angle:- ( $\theta_o$ ) / Angle of ascent:

Angle through which cam rotates for the rise of follower.

2) Return stroke Angle ( $\theta_r$ ) / Angle of descent

The angle through which cam rotates for the fall/return of follower.

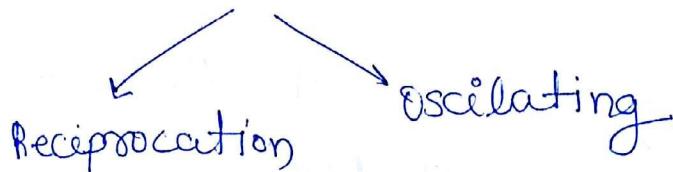
(iii) Dwell ( $\delta$ ) :- The angle of cam rotation for which follower is in rest

(iv) Angle of Action, ( $\theta_a$ ) it is total angle rotated by the cam during the time b/w beginning of rise and the end of return of follower.

$$\theta_a \leq 2\pi$$

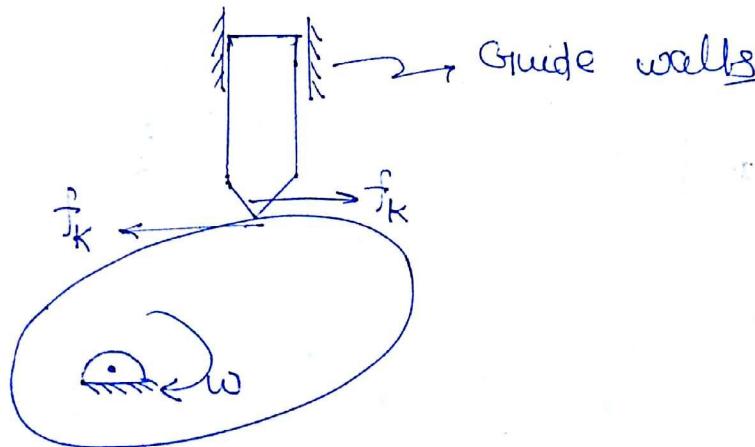
Classification of follower.

① Type of movement



② Acc. to type of contact

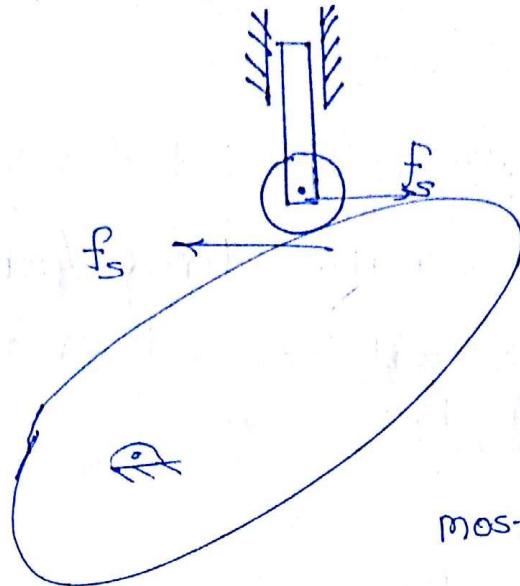
(a) knife edge :- Not practically used due to excessive wear.



Disadvantage:- → Excessive wear because of very sharp contact point

→ Heavy side thrust because of  $f_K$  (kinetic friction) against the guide wall of the follower.

### (b) Roller follower:-



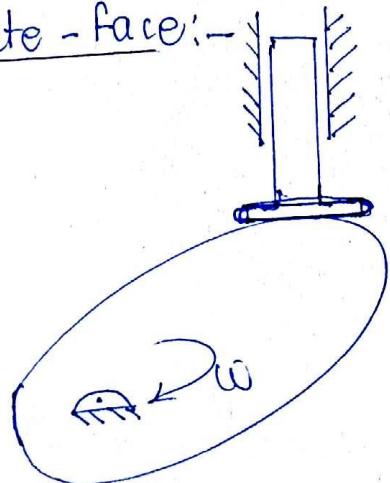
- wear excessively reduced.
- side thrust is reduced as compared to knife edge follower but considerable because  $f_s < f_k$  for most of its range.

→ wide application in aircraft engines.

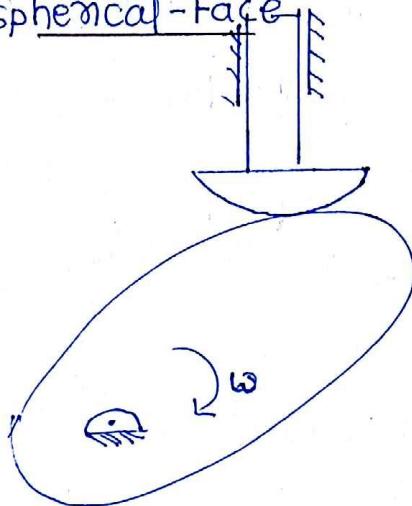
it requires more space because of roller dimension  
i.e. why not used in IC engine

### (c) Mushroom follower:-

#### flat-face:-



#### spherical-face



Flat face:- contact area as compare to knife edge is increase so wear is highly reduced compared to knife edge. but surface stress are generated.

disadvantage: Surface frizzes on cam profile which result in distortion of cam profile that's why instead of flat face, spherical face followers are used

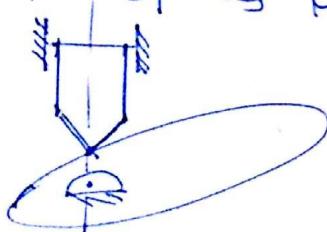
spherical:- There are design to reduce surface contact which in turn to reduce surface stress.

- surface stress are minimise.
- wear slightly more than flat face follower (less contact area)

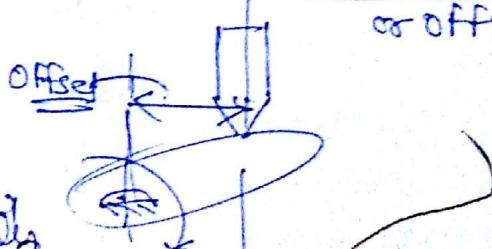
Note: further slight reduction can be obtained by offsetting the follower. (side thrust also reduce)

③ According to location of line of movement of follower

(a) Radial follower:- If line of motion passes through centre of rotation of cam, such a follower is known as radial follower.



(b) Offset-follower:- If line of motion passes away from the centre of rotation of Cam.  
- avoids jamming of follower  
- reduces wear, distributes wear uniformly

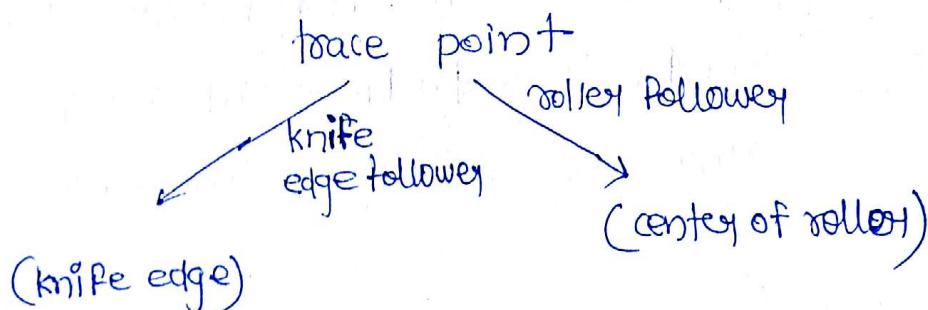


## Cam terminology:-

Base Circle! — The smallest circle drawn from the centre of rotation of cam forming the part of the cam profile is known as base circle. The radius of this circle is called to least radius of cam.

\* The size of any cam is specified by the size of base circle.

Pitch/Trace point and Trace curve: The point on the follower which is required to trace the cam profile is known as trace point and the curve traced by the trace point by keeping the cam stationary and revolving the follower around it is known as pitch curve/trace curve.



Pressure Angle! — ( $\phi$ ) It is the angle b/w the normal to the pitch curve at a point and line of motion of follower. It represents the stiffness of the cam profile.

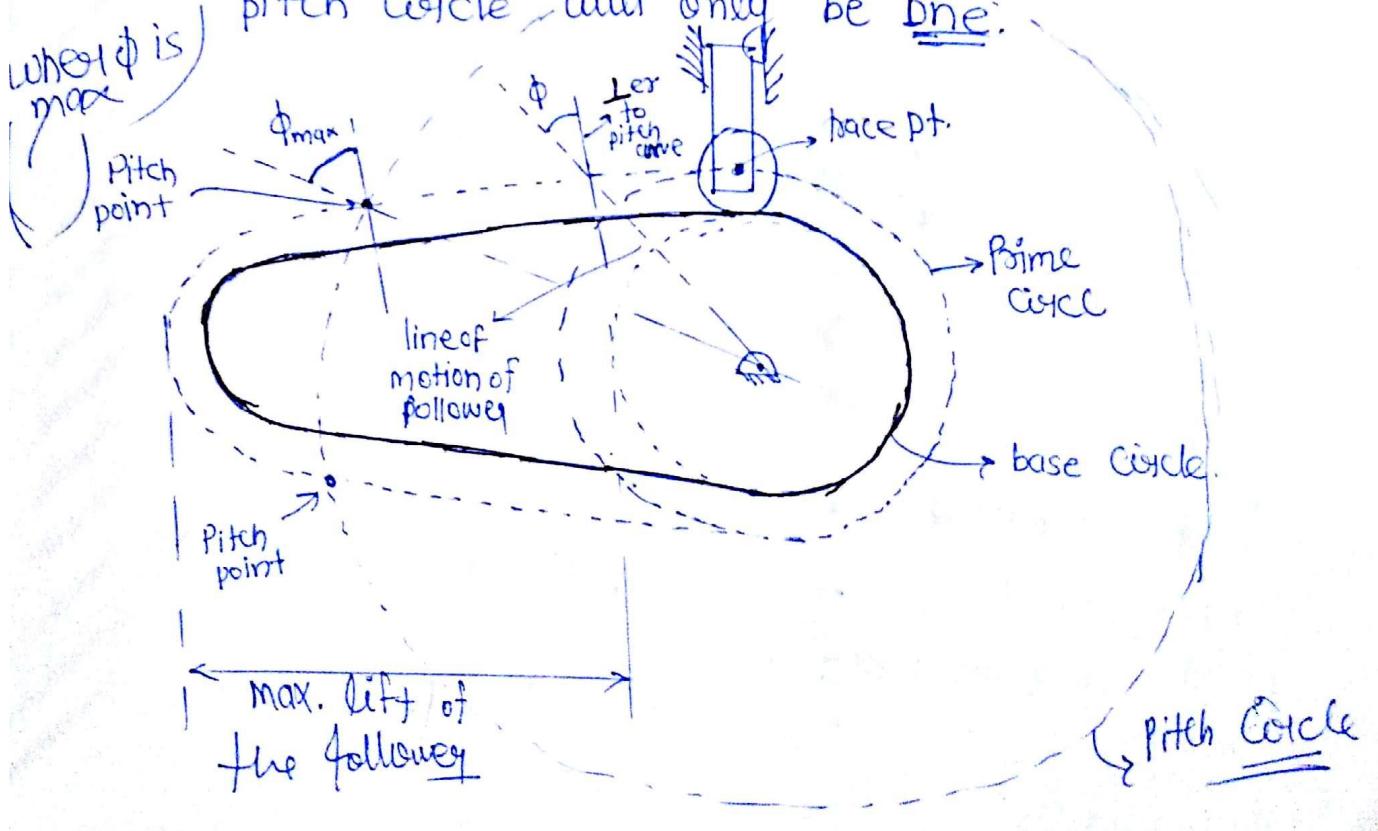
Note:  $\phi$  varies in magnitude at all instant of follower motion a high value of max.  $\phi$  is not desired (usually  $\phi < 30^\circ$ ) as it might jam the follower in the bearing.

Pitch point:- The point on the pitch curve where  $\phi$  is maximum is called pitch point.

Prime circle:- Minimum radius circle of pitch curve from the ~~ext~~ centre of rotation of Cam is known as prime circle.

Pitch circle:- It is the circle passing through the pitch point and concentric with the base circle.

Note: Pitch point can be more than one but pitch circle will only be one.



## Follower Derivative!

$x \rightarrow \theta$  curve

$\omega \rightarrow$  angular Vel. of Cam  $\rightarrow$  constant

1st order derivative

$$\frac{dx}{d\theta}$$

slope of  $x-\theta$  curve

$$\frac{dx}{dt} \times \frac{dt}{d\theta} = \frac{v}{\omega}$$

$$\frac{dx}{dt} \propto v \quad (\text{Vel. of follower})$$

Velocity of Cam not be very - very high that means slope of  $x-\theta$  curve should not be very - very high.

2nd order derivative

$$\frac{d^2x}{d\theta^2}$$

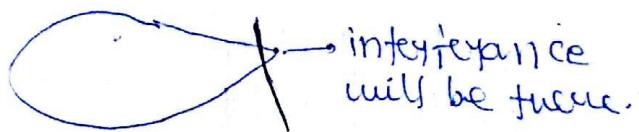
$(x-\theta)$  curve proportion to inverse of radius of curvature of  $x-\theta$  curve

$$\left\{ \frac{1}{R} \propto \frac{dy}{dx^2} \right\}$$

$$\frac{d^2x}{d\theta^2} \propto a \quad (\text{accn of follower})$$

$$\frac{d^2\theta}{d\theta^2} = \frac{d^2x}{(dt)^2} \times \frac{(dt)^2}{d^2\theta} = \frac{a}{\omega^2}$$

If accn of follower is  $\infty$ , then R of  $x-\theta$  curve will be zero that means sharp point on cam profile



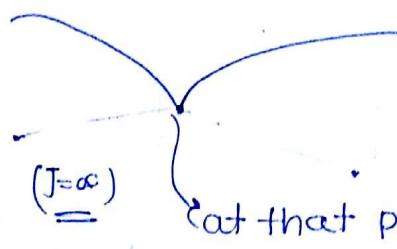
3<sup>rd</sup> order derivative

$$\frac{d^3 r}{d\theta^3}$$

represents  $\frac{d}{d\theta} \left( \frac{d^2 r}{d\theta^2} \right)$  → ~~rate of change~~ represent change of radius of curvature w.r.t  $\theta$

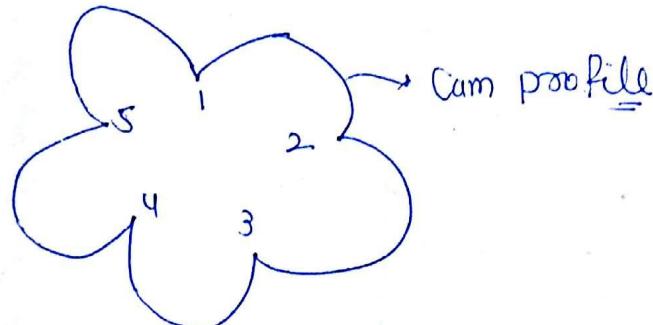
$$\frac{d^3 r}{d\theta^3} \text{ a j ( jerk of follower)}$$

Jerk should not be  $\infty$  level because if  $j$  is  $\infty$ , radius of curvature is changing at  $\infty$  level that means profile will be like



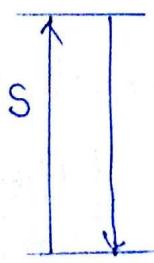
at that point  $j$  will be  $\infty$

⇒ say 5 points are of  $\infty$  jerk -



Types of follower Motion:-

### ① Uniform Velocity :-



$w$  - ang. velocity of cam

$\theta_o$  → angle of outstroke

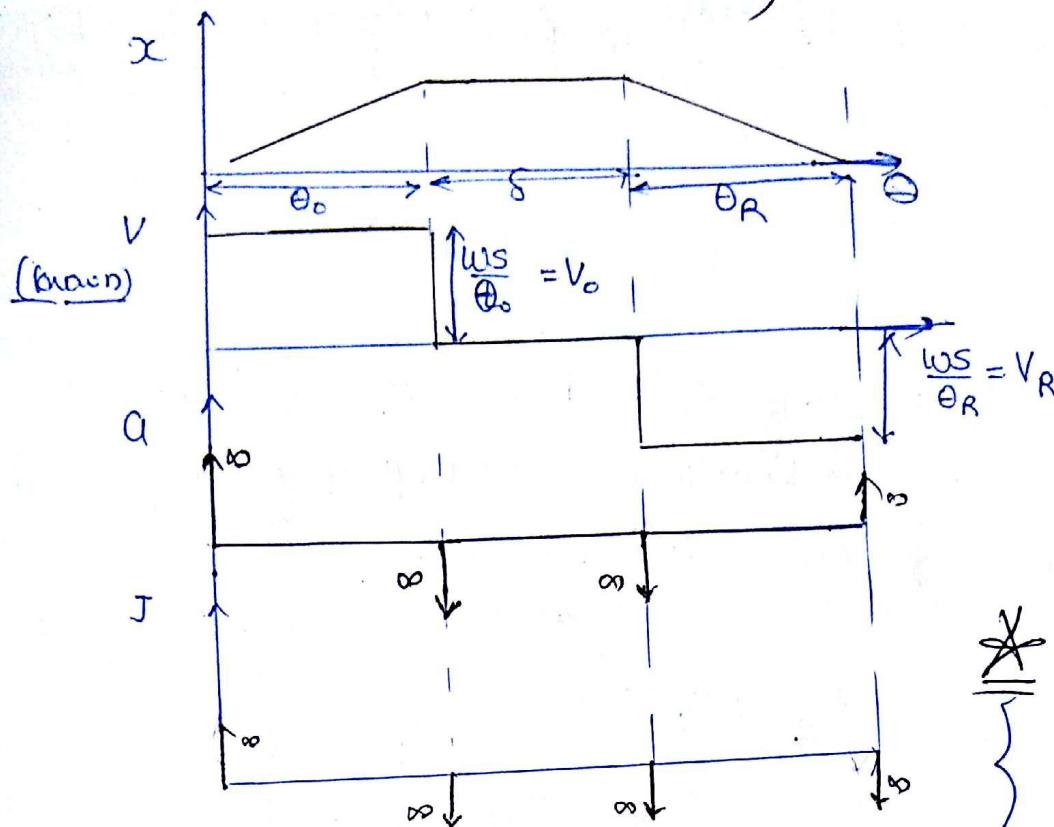
$\theta_R$  → angle of return stroke

$$t_o = \frac{\theta_o}{w}$$

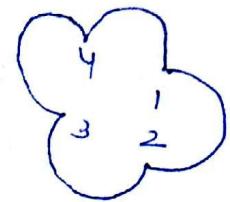
$$\text{outstroke } V_o = \frac{S}{t_o} = \frac{ws}{\theta_o} = (V_{max})_{\text{outstroke}} \quad a_o = 0$$

$$V_R = \frac{ws}{\theta_R}, \quad a_R = 0$$

(ideal uniform Velocity)

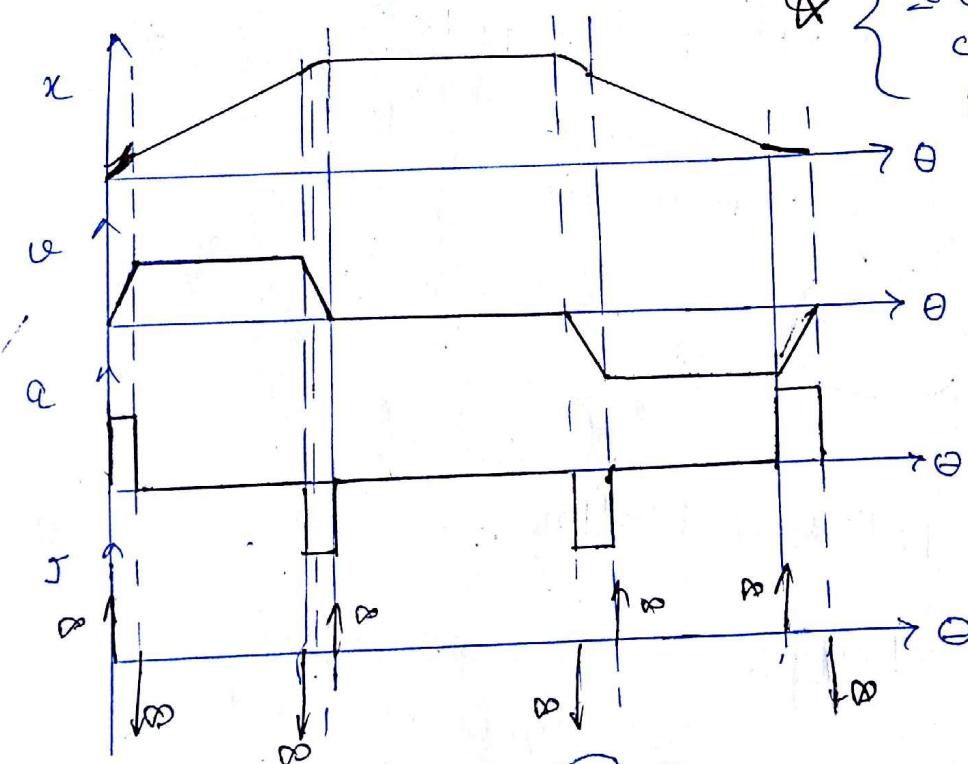


⇒ 4 point of interference.

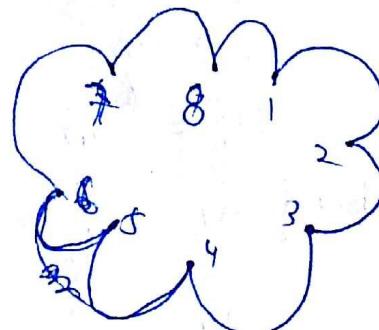


\* This type of can not be used in practical else move the can very very slow speed.

(Actual uniform Velocity)



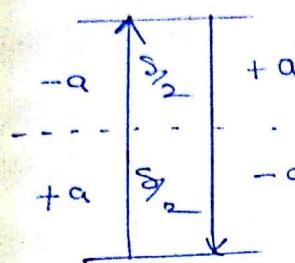
else move the can very very slow speed.



8 point of interference

## ② Uniform acc<sup>n</sup> & Retardation (parabolic)

$$t_0 = \frac{\theta_0}{\omega}$$

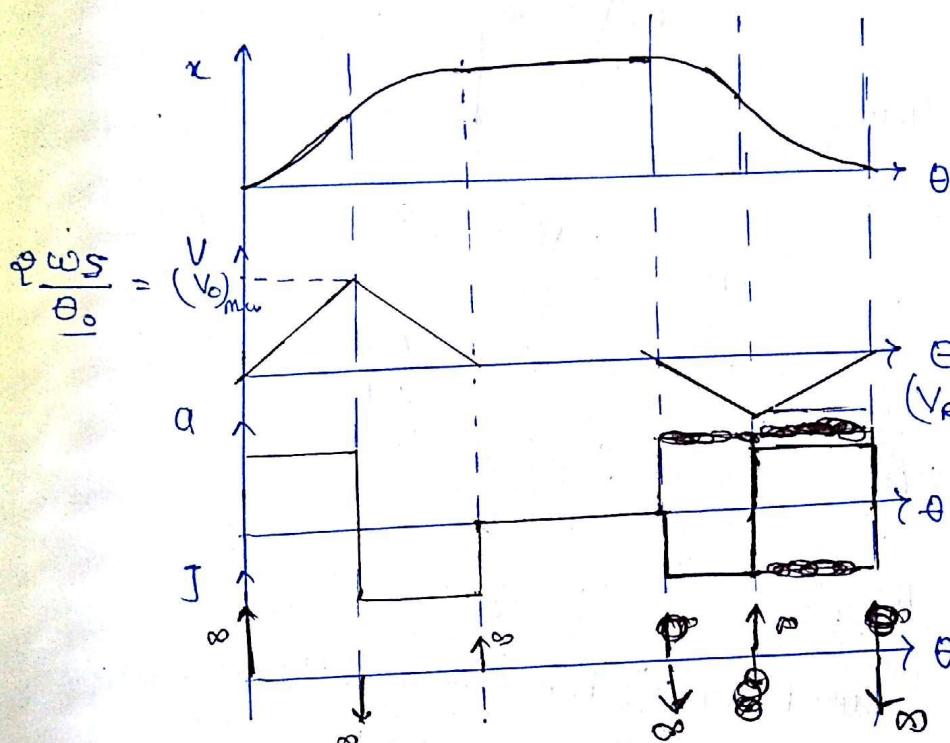


$$(V_0)_{\text{mean}} = \frac{s}{t_0} = \frac{\omega s}{\theta_0}$$

$$(V_0)_{\text{mean}} = \frac{V_{\text{mean}} + V_{\text{max}}}{2}$$

$$V_{\text{max}} = 2(V_0)_{\text{mean}} = \frac{2\omega s}{\theta_0}$$

This type of cam not used practically else moves the cam very slow speed



$$S = ut + \frac{1}{2}at^2$$

$$\frac{S}{2} = \frac{1}{2}a\left(\frac{t_0}{2}\right)^2 = \frac{1}{2}a\left(\frac{\theta_0}{2\omega}\right)^2$$

$$a = \frac{4\omega^2 S}{\theta_0^2}$$

$$y = ut + at \quad t = \frac{t_0}{2}$$

$$(V_0)_{\text{max}} = \frac{4\omega^2 S}{\theta_0^2} \times \left(\frac{\theta_0}{2\omega}\right) \quad (V_{\text{max}}) = \frac{2\omega S}{\theta_0}$$

3. SHM :- when a particle moves in circular path with uniform angular velocity, its projection on diameter will make SHM.

$$\vec{a} = \vec{a}_r$$

$$\vec{a}_t = 0$$

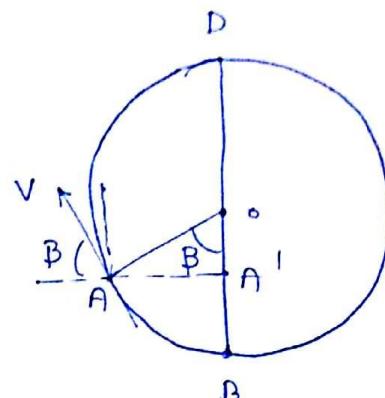
$v = \text{const.}$ ,  $BD = S$

$$V_{A'} = v \sin \beta = V_{\text{follower}}$$

$$v = \frac{\pi s}{2 t_0}$$

$$t_0 = \frac{\theta_0}{\omega}$$

$$v = \frac{\pi \omega s}{2 \theta_0}$$



$$v = \frac{\pi s}{2 t_0} = \frac{\pi s \omega}{2 \theta_0}$$

$$v = \frac{\pi \omega s}{2 \theta_0}$$

Now let in time  $t$

- Point on circumference has moved through angle  $\beta$
- Follower has displaced from point B to A'
- Cam has rotate through an angle  $\theta$

$$\theta_0 \xrightarrow{\text{(cam)}} \frac{\pi}{\theta_0} \text{(particle)}$$

$$t \xrightarrow{\quad} \frac{\pi}{\theta_0}$$

$$\theta \xrightarrow{\quad} \frac{\pi}{\theta_0} \theta = \beta$$

$$\boxed{\beta = \frac{\pi \theta}{\theta_0}}$$

$$\text{so } V_A / V_{\text{outstroke}} / V_{\text{follower}} = V_0 = \frac{\pi \omega s}{2 \theta_0} \sin \left( \frac{\pi \theta}{\theta_0} \right)$$

$$(V_s)_{\max} = \frac{\pi \omega s}{2 \theta_0}$$

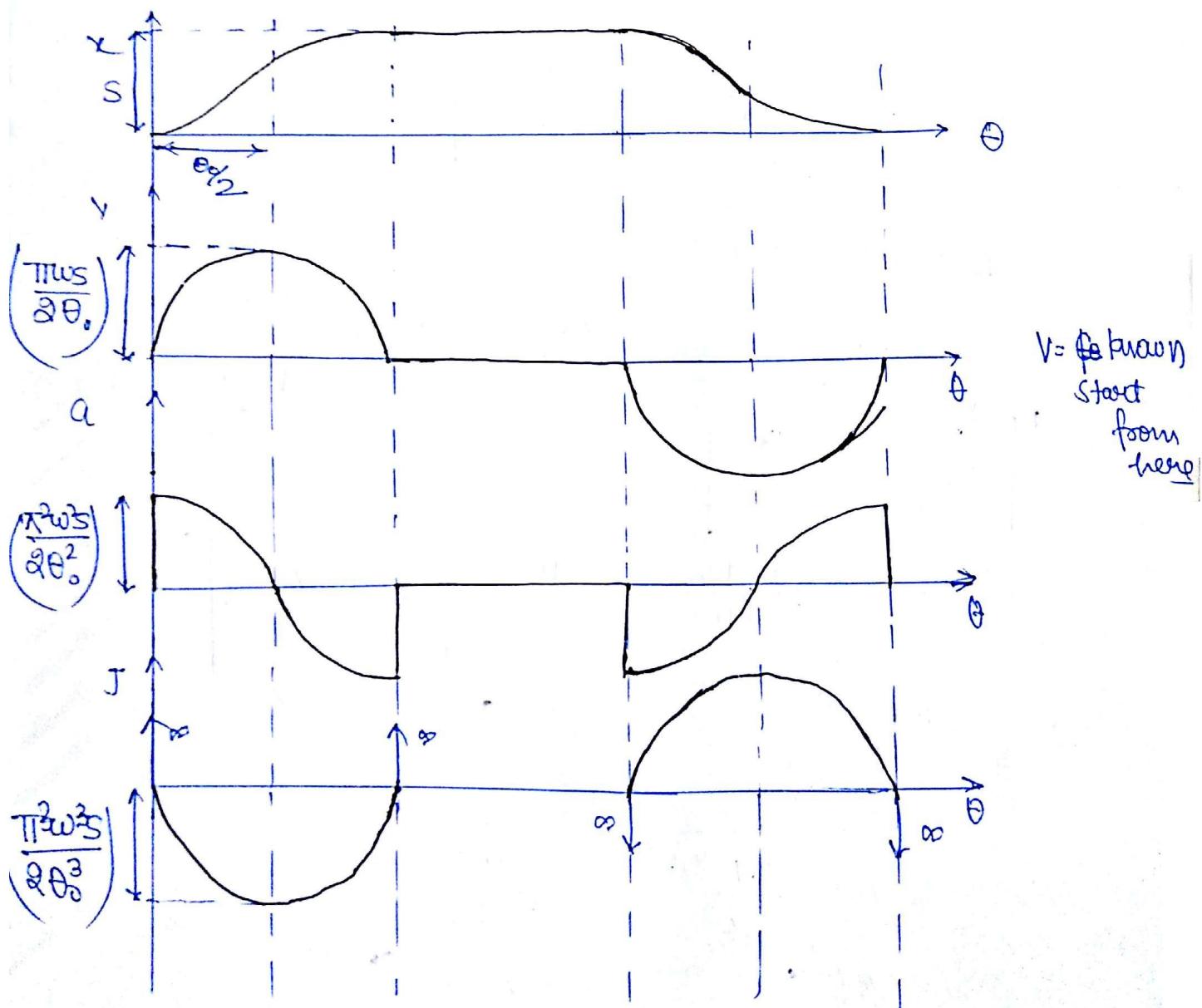
, when  $\frac{\pi \theta}{\theta_0} = \frac{\pi}{2} \Rightarrow \theta = \frac{\theta_0}{2}$

$$a_o = \left(\frac{dv}{d\theta}\right) \omega = \frac{\pi^2 \omega^2 s}{2 \theta_0^2} \cos\left(\frac{\pi \theta}{\theta_0}\right)$$

$$(a_o)_{\max} = \frac{-\pi^2 \omega^2 s}{2 \theta_0^2} \quad \Rightarrow \text{when } \theta = 0^\circ$$

$$J_o = \frac{\pi^3 \omega^3 s}{2 \theta_0^3} \left( -\sin \frac{\pi \theta}{\theta_0} \right)$$

$$(J_o)'_{\max} = \frac{\pi^3 \omega^3 s}{2 \theta_0^3}$$



\* Four infinites point so this motion can be used for medium speeds.

This is better than uniform velocity and uniform acc<sup>n</sup> deceleration.

#### 4 Cycloidal Motion:-

$$\Rightarrow x_0 = s \left[ \frac{\theta}{\theta_0} - \frac{1}{2\pi} \sin \left( \frac{2\pi\theta}{\theta_0} \right) \right]$$

$$v_0 = \frac{dx_0}{d\theta} \omega = \omega s \left[ \frac{1}{\theta_0} - \frac{1}{\theta_0} \cos \left( \frac{2\pi\theta}{\theta_0} \right) \right]$$

$$v_\theta = \frac{\omega s}{\theta_0} \left[ 1 - \cos \left( \frac{2\pi\theta}{\theta_0} \right) \right]$$

$$v_0 \rightarrow \max, \text{ when } \cos \left( \frac{2\pi\theta}{\theta_0} \right) = -1$$

$$\frac{2\pi\theta}{\theta_0} = \pi \Rightarrow \boxed{\theta = \frac{\theta_0}{2}}$$

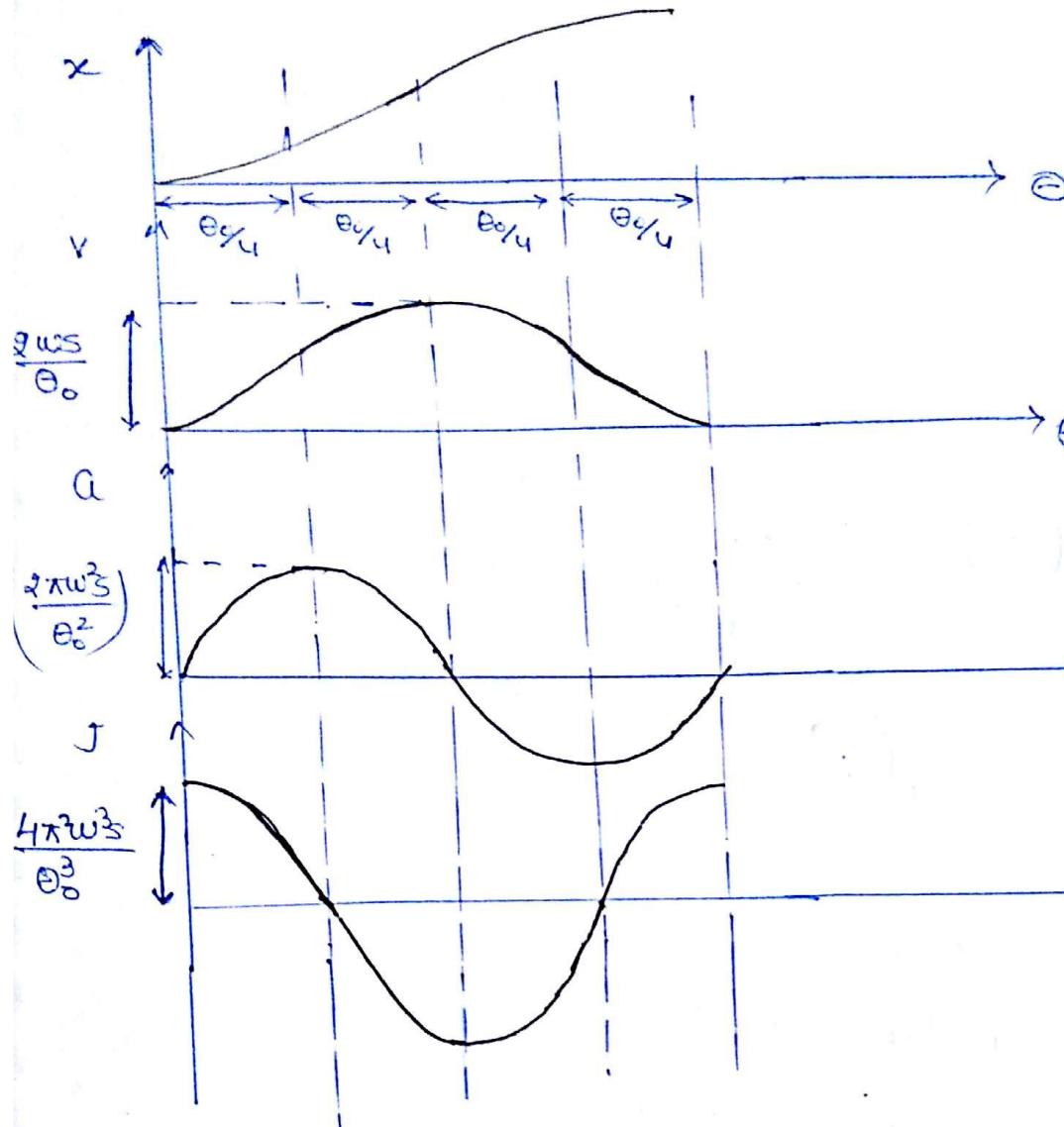
$$\boxed{(v_0)_{\max} = \frac{2\omega s}{\theta_0}}$$

$$a_0 = \omega \left( \frac{dv_0}{d\theta} \right) = \frac{2\pi\omega^2 s}{\theta_0^2} \left[ \sin \left( \frac{2\pi\theta}{\theta_0} \right) \right]$$

$$\boxed{(a_0)_{\max} = \frac{2\pi\omega^2 s}{\theta_0^2}}$$

$$J_0 = \frac{4\pi^2\omega^3 s}{\theta_0^3} \cos \left( \frac{2\pi\theta}{\theta_0} \right)$$

$$\boxed{(J_0)_{\max} = \frac{4\pi^2\omega^3 s}{\theta_0^3}}$$

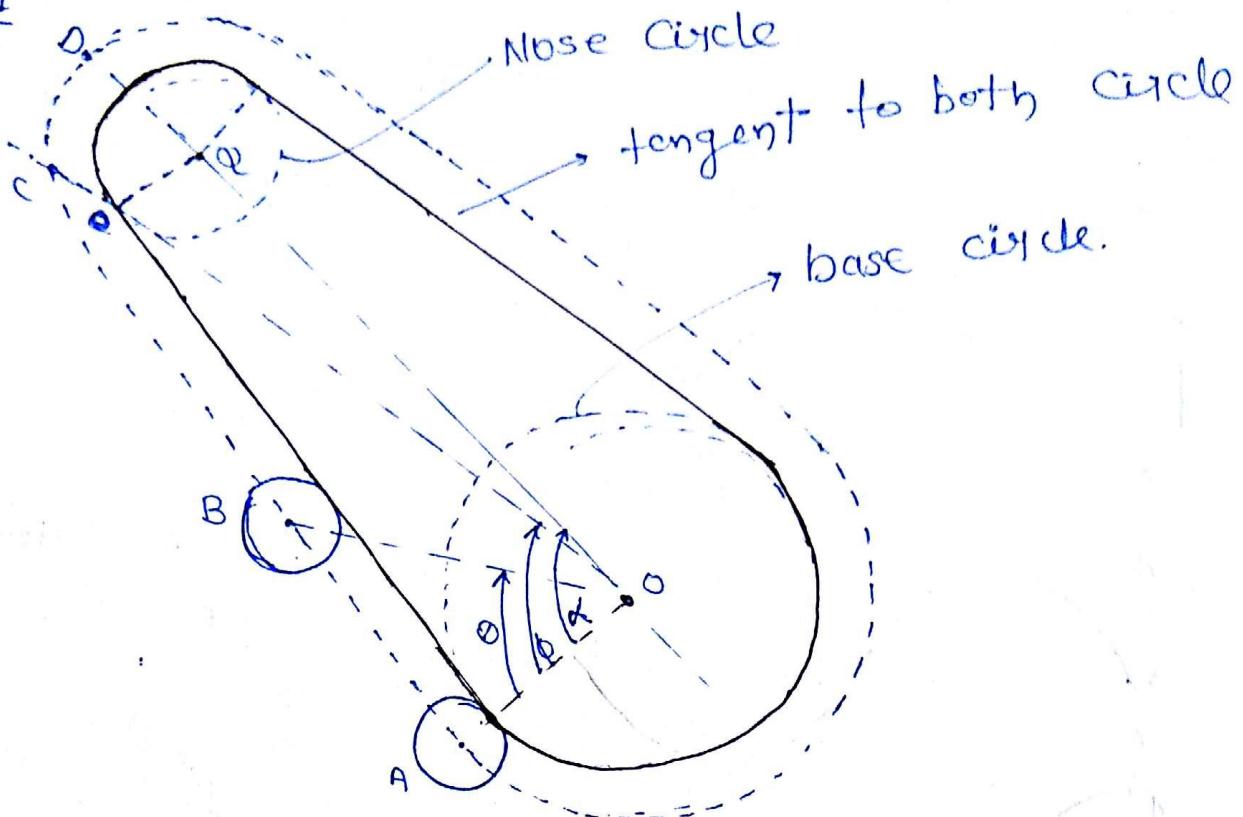


Cams with specified Contours :-

(a) Tangent cam with roller follower :-

when flank of cam is straight and tangential to base circle and nose circle it is known as tangent cam.

Case-1



$\Rightarrow \gamma$  - distance b/w base circle & nose circle =  $OQ$

$\Rightarrow r_1$  - radius of base circle

$\Rightarrow r_2$  - radius of nose circle

$\Rightarrow r_3$  - radius of roller

$\Rightarrow r_2 + r_3 = l$

$\Rightarrow \alpha$  - angle of ascent

(i) When roller is on tangent plank! -

$$0 \leq \theta \leq \phi$$

Following ~~displacement~~ displacement  $x = OB - OA$

$$\Delta OAB \quad OB \cos \theta = OA$$

$$x = \frac{OA}{\cos \theta} - OA$$

$$x = OA \left( \frac{1 - \cos \theta}{\cos \theta} \right)$$

$$x = (\tau_1 + \tau_3) \left[ \frac{1 - \cos \theta}{\cos \theta} \right]$$

$$v = \frac{dx}{dt} = \omega \frac{dx}{d\theta} = \omega (\tau_1 + \tau_3) \left( \frac{\sin \theta}{\cos^2 \theta} \right)$$

$$V_{max} = \omega (\tau_1 + \tau_3) \left( \frac{\sin \phi}{\cos^2 \phi} \right)$$

when  $\theta = \phi$

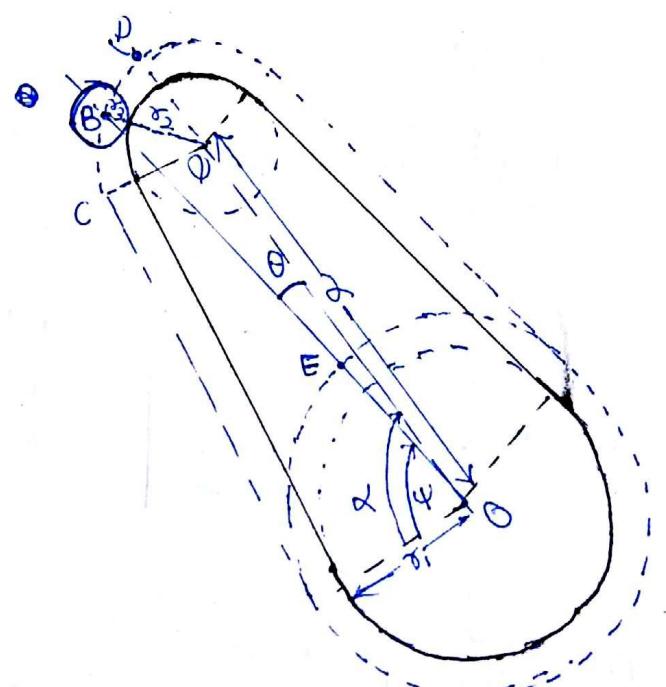
~~Velocity depends on Roller follower and base circle radius.~~

$$a = \omega \frac{dv}{d\theta} = \omega^2 (\tau_1 + \tau_3) \frac{(2 - \cos^2 \theta)}{(\cos^3 \theta)}$$

$$a_{max} = \omega^2 (\tau_1 + \tau_3) \left( \frac{2 - \cos^2 \phi}{\cos^3 \phi} \right)$$

### Case -2

$$\tau_2 + \tau_3 = l$$



(ii) When roller on Nose part:-

$$\phi \leq \Psi < \alpha$$

$$x = OB - OA = OB - OE$$

$$x = \tau \left[ (1 - \cos \theta) + \left( n - \sqrt{n^2 - \sin^2 \theta} \right) \right]$$

$$n = \frac{l}{\tau} = \frac{\tau_2 + \tau_3}{\tau}$$

$$x = \tau \left[ (1 - \cos \theta) + \frac{\tau_2 + \tau_3}{\tau} - \sqrt{\left( \frac{\tau_2 + \tau_3}{\tau} \right)^2 - \sin^2 \theta} \right]$$

$$x = \left[ \tau (1 - \cos \theta) + l - \sqrt{l^2 - \tau^2 \sin^2 \theta} \right]$$

$$\therefore l = \tau_2 + \tau_3$$

$$V = \omega \frac{dx}{d\theta} = \omega \left[ \tau \sin \theta + \frac{(\tau)^2 \sin 2\theta}{2 \sqrt{l^2 - \tau^2 \sin^2 \theta}} \right]$$

$$V = \tau \omega \left[ \sin \theta + \frac{\tau \sin \theta}{\sqrt{l^2 - \tau^2 \sin^2 \theta}} \right]$$

\* Velocity depends  
on Centre distance  
~~from~~, nose  
radius

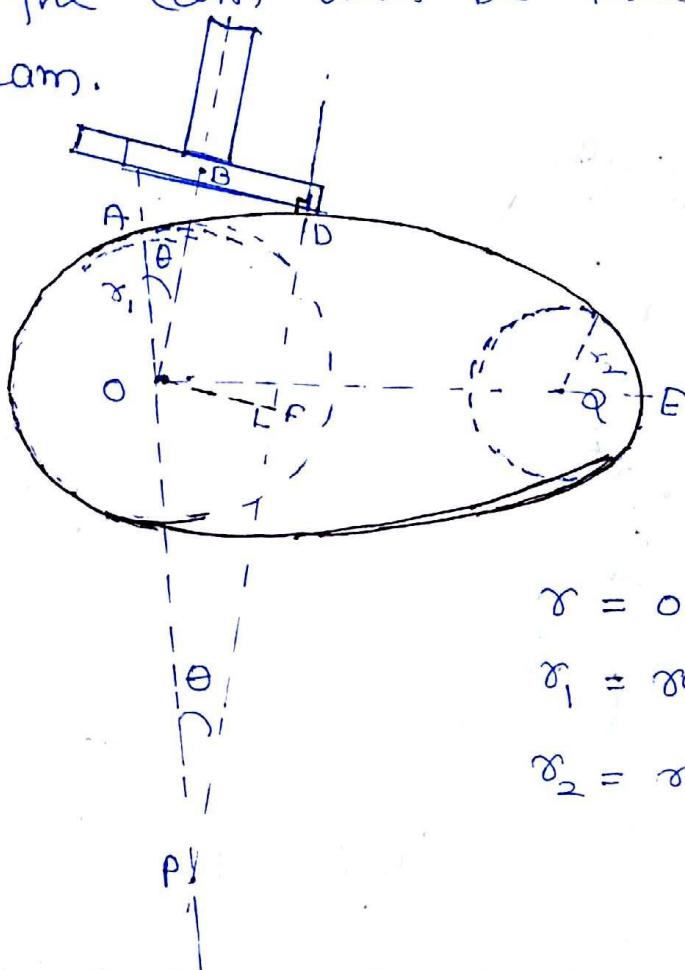
$$a = \frac{dV}{d\theta} \Rightarrow a = \omega^2 \tau \left[ \cos \theta + \frac{(l^2 \tau \cos 2\theta + \tau^3 \sin^4 \theta)}{(l^2 - \tau^2 \sin^2 \theta)^{3/2}} \right]$$

$$\boxed{\theta = \Psi - \Phi}$$

\* when the roller is on the nose part  $OQB$  behaves as a slider crank chain in which  $OQ$  is crank,  $QB$  the connecting rod and  $B$  is the slider.  $OB$  is the line of action.

### b) Circular arc Cam with flat - face Follower:-

when the flanks of the cam are of convex circular arc and tangential to base circle and nose circle then the cam will be known as circular arc cam.



(i) Flat face is on the circular flank:-

$$x = OB - OA$$

$OB$  &  $PD$  are parallel

$$x = ED - OA = (PD - PP') - OA$$

$$x = (PA - OA) - PF$$

\* Velocity depends on base circle radius and circular arc radius.

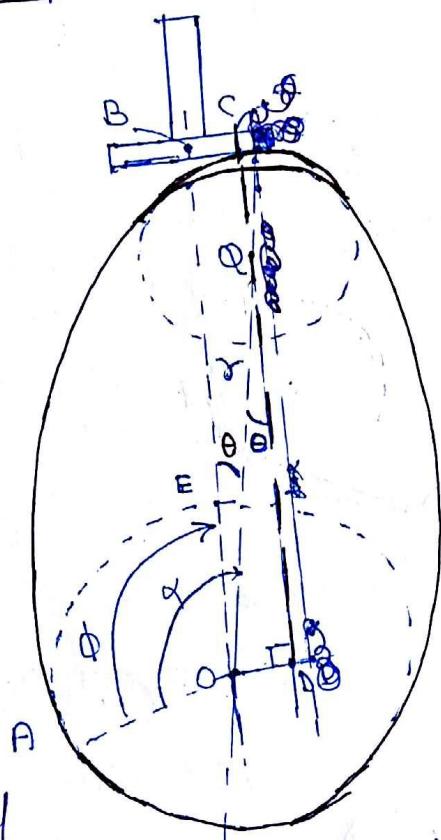
$$x = OP - \odot P \cos \theta$$

$$x = (R - r_1)(1 - \cos \theta)$$

$$v = \omega(R - r_1)(\sin \theta)$$

$$a = \omega^2(R - r_1) \cos \theta$$

### (ii) Flat face follower on the nose



$$x = OB - OA$$

OB & CD are parallel

$$x = CD - OA$$

$$x = BQ + QC - OA$$

in  $\triangle O D Q$

$$DQ = OQ \cos \theta = r \cos \theta$$

$$x = r \cos \theta + r_2 - r_1$$

$$v = \omega r (-\sin \theta)$$

$$a = -\omega^2 r \cos \theta$$

\* Velocity depends on base nose circle radius and centre distance