ELECTRICAL MACHINES TEST 6

Number of Questions: 25

Directions for questions 1 to 25: Select the correct alternative from the given choices.

- A three phase *Y* connected 50Hz two pole synchronous machine has a stator with 2000 turns/phase. What rotor flux is required to produce line to line voltage of 5kV?
 (A) 1.2 × 10⁻²Wb
 (B) 1.95 × 10⁻²Wb
 (C) 6.5 × 10⁻³Wb
 (D) 3.75 × 10⁻³Wb
- 2. A location requires 300kW of 60Hz ac power. Power sources are available only at 50Hz. Power is to be generated using synchronous motor alternator set. How many poles should each of the machines have to convert 50Hz power to 60Hz power?
 - (A) 10 pole motor, 12 pole generator
 - (B) 12 pole motor, 10 pole generator
 - (C) 10 pole motor, 10 pole generator
 - (D) 12 pole motor, 12 pole generator
- 3. If the frequency of an alternator is changed form f_1 to f_2 its synchronous reactance (X_s) becomes _____.

(A)
$$(f_1/f_2) X_s$$

(B) $(f_2/f_1) X_s$
(C) X_s
(D) X_c/f_2

4. Given synchronous generator phasor diagram



- θ_1, θ_2 indicate (respectively)
- (A) torque angle, power factor angle
- (B) power factor angle, torque angle
- (C) power factor angle, internal voltage angle
- (D) internal voltage angle, torque angle
- 5. _____ torque of synchronous motor can cause the motor to slip and step out of synchronism.

| (A) | accelerating | (B) | Pull - in |
|-----|--------------|-----|-----------|
| | | | |

- (C) pull out (D) load
- **6.** In the following characteristics of an alternator *BC* represents.



Section Marks: 90

- (A) field current necessary to overcome demagnetizing effect of armature reaction at full load.
- (B) armature reaction drop at full load.
- (C) field current necessary to overcome cross magnetizing effect of armature reaction at full load.
- (D) armature resistance drop at full load.
- 7. Which of the following equation represent the maximum mechanical power developed in synchronous motor?

(A)
$$\frac{E_b V}{Z_s} - \frac{E_b^2}{Z_s}$$
 (B) $\frac{E_b V}{Z_s} - \frac{E_b^2}{Z_s} \sin\theta$
(C) $\frac{E_b V}{Z_s} - \frac{E_b^2}{Z_s} \cos\theta$ (D) $\frac{E_b V}{Z_s} \cos\theta$

8. In an alternator chording angle for fundamental flux wave is α . Then its value for 7th harmonic is

(A)
$$\frac{a}{7}$$
 (B) $7a$

(C)
$$\frac{6a}{7}$$
 (D) $\frac{8a}{7}$

- 9. Synchronous motors are :
 - (A) self starting
 - (B) started manually
 - (C) started with a squirrel cage
 - (D) started with a capacitor
- **10.** A 40 MVAr synchronous condenser operates on a 34.5 kV bus. Synchronous reactance is 150%. Estimate the field excitation required to get 40 MVAr power.
 - (A) 100% (B) 200%
 - (C) 250% (D) 50%
- **11.** A 480V, 60Hz six pole synchronous motor draws 80A form the line at UPF, full load. Assuming that motor is lossless. Then what is the output torque?
 - (A) 629 Nm (B) 429 Nm
 - (C) 529 Nm (D) 729 Nm
- **12.** For the circuit given below, what real and reactive power are provided by the generator when the switch is closed?



(C) 252 kW, 152kVAr (D) 108 kW, 52.8kVAr

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13. A 100MVA, 11.5kV, 0.75pf lagging, 50Hz two pole *Y* – connected synchronous generator has a per unit reactance of 0.9 and a per unit armature resistance of 0.012. The magnitude of internal generated voltage at rated conditions is _____ and the torque angle is ______ (A) 10750, 23° (B) 11556, 37°

| · · | · · · | | |
|-----|------------|-----|------------|
| (C) | 10750, 37° | (D) | 11556, 23° |

14. A three phase synchronous generator has negligible armature resistance and synchronous reactance $X_d = 1.5$ P.u. This machine is connected to an infinite bus at voltage $1 \angle 0^{\circ}$ P.u. what is the internal voltage of the machine when it delivers a current of $1 \angle 30^{\circ}$ P.u to the infinite bus

| (A) | 1.44∠83° | (B) | 1.23∠82° |
|-----|----------|-----|-------------------|
| (C) | 1.32∠79° | (D) | None of the above |

- 15. A three phase two pole winding is installed in six slots on a stator. There are 80 turns of wire in each slot of the windings. The three phases are Δ connected, all coils in each phase are connected in series. What is the frequency of voltage produced by this winding? (N = 3600 rm)
 - (A) 50 Hz (B) 60 Hz
 - (C) 80 Hz (D) 48 Hz
- **16.** What may be the highest speed at which two generators mounted on the same shaft be driven, if frequency of one generator is 25 Hz and that of the other is 60 Hz? They cannot have more than 26 poles.
 - (A) 120 rpm (B) 360 rpm
 - (C) 300 rpm (D) 3000 rpm
- 17. A 50 kVA, 200 V, 50 Hz, 1Φ alternator has an effective armature resistance of 0.02 ohm and an armature leakage of 0.08 ohm. Compute the voltage induced in the armature, when the alternator is delivering rated current at a load power factor of 0.8 leading.

| (A) | 216.39 V | (B) | 192.93 V |
|-----|-----------|-----|-----------|
| (C) | 468.25 kV | (D) | 372.25 kV |

18. A 3-phase alternator has a direct axis synchronous reactance of 0.6 p.u and a quadrature axis synchronous reactance of 0.3 p.u. Calculate the direct axis current when the alternator delivers a full load current at 0.7 p.f lagging.
(A) 0.71
(B) 0.58

| (n) | 0.71 | (D) | 0.50 |
|-----|------|-----|------|
| (C) | 0.82 | (D) | 0.17 |

19. A 600 kVA, 11 kV, 6-pole, $3 - \Phi$ star connected alternator has percentage resistance and reactance of 2 and 10 respectively. Calculate the synchronizing power per mechanical degree of displacement at full load 0.9 power factor lagging.

- (A) 111.50 W/phase (B) 111.50 kW/phase
- (C) 334.5 W/phase (D) 334.5 kW/phase
- **20.** Two alternators *A* and *B* operate in parallel and supply a load of 20 MW at 0.75 p.f lagging. Calculate the power factor of alternator *B* when alternator *A* supplies 14,000 kW at 0.9 lagging power factor.
 - (A) 0.48 lagging (B) 0.77 lagging
 - (C) 0.62 lagging (D) 0.53 lagging
- 21. Calculate the power angle when a2000 kVA, 11 kV, 3-phase, *Y*-connected alternator having a resistance of 0.5 ohm and a reactance of 5 ohm per phase delivers full load current at normal rated voltage and 0.8 p.f lagging.
 (A) 6.60°
 (B) 40.16°
 - (A) 6.60°
 (B) 40.16°
 (C) 3.30°
 (D) 36.24°
- **22.** A 2000V star connected synchronous motor has a resistance of 0.4 ohm per phase and a synchronous reactance of 3.0 ohm per phase. The motor is operating at 0.8 power factor leading with a line current of 300 A. Calculate the value of the generated e.m.f per phase.
 - (A) 692.89 V/phase
 - (B) 1370.19 V/phase
 - (C) 1782.36 V/phase
 - (D) 1200.12 V/phase
- 23. A 1500 V, 3-phase, 6-pole, Y-connected synchronous motor runs at 1000 rpm. The excitation is constant and corresponds to an open-circuit terminal voltage of 1500 V. The resistance is negligible as compared with synchronous reactance of 4 Ω per phase. Calculate the torque developed for an armature current of 300 A.
 - (A) 5627.44 N-m(B) 5374.21 N-m(C) 562.74 N-m(D) 537.42 N-m

Common data questions for 24 and 25:

24. A 480V, 200kW, two pole, three phase, 50 Hz synchronous generators prime mover has the no load speed of 3040rpm and full load speed of 2975rpm. It operates in parallel with a 480 V, 180 kW, four pole, 50 Hz synchronous generator whose prime mover has a no load speed of 1500rpm and full load speed of 1485rpm. Together, they supply 200kW at 0.85PF lagging. Speed drops of generator 1 and generator 2 are respectively. (in percent)

| | (A) | 2.18, 1.01 | | (B) | 1.01, 2.18 |
|-----|--------|--------------|---|-----|--------------|
| | (C) | 0.218, 0.101 | | (D) | 0.101, 0.218 |
| ~ - | X X 71 | 1 | 1 | | |

25. What is the power given by generator 2?

| (A) | 128 kW | (B) | 72 kW |
|-----|--------|-----|--------|
| (C) | 100 kW | (D) | 200 kW |

| Answer Keys | | | | | | | | | |
|-------------|--------------|--------------|--------------|--------------|-------------|-------------|-------------|--------------|--------------|
| 1. C | 2. A | 3. B | 4. A | 5. C | 6. A | 7. C | 8. B | 9. C | 10. C |
| 11. C | 12. B | 13. D | 14. C | 15. B | 16. C | 17. B | 18. C | 19. B | 20. A |
| 21. C | 22. C | 23. B | 24. A | 25. B | | | | | |

HINTS AND EXPLANATIONS

Choice (B)

1.
$$V_{\text{phase}} = \frac{5000}{\sqrt{3}} = 2886.8$$

 $E = \sqrt{2}\pi N_c \varphi f$
 $\Rightarrow \phi = \frac{E}{\sqrt{2}\pi N_c f} = \frac{2886.8}{\sqrt{2}\pi \times 2000 \times 50} \approx 6.5 \times 10^{-3} \text{Wb}$
Choice (C)

2.
$$N_s = \frac{120 f}{p}$$

But since shafts are coupled, mechanical speed of motor and generator should be equal.

Hence,
$$\frac{120 \times 50}{P_1} = \frac{120 \times 60}{P_2}$$

 $\Rightarrow \frac{P_2}{P_1} = \frac{6}{5}$

Hence 12 pole generator, 10 pole motor will be suitable. Choice (A)

3. Since armature reaction αf

 $\therefore X_s \alpha f$

- Choice (A)
 Choice (C)
- 6. Choice (A)
- 7. Choice (C)
- 8. Choice (B)
- 9. Choice (C)

10.
$$V_t = E + j I_a X_s$$

 $1 \angle 0^\circ = E \angle 0^\circ + j I_a(1.5)$
 $1 - E = 1.5I_a \angle (90^\circ + 90^\circ)$

At
$$|I_a| = 1$$

 $1 - E = -1.5$
 $|E| = 2.5$

 \therefore Field excitation should be 250% Choice (C)

11. For lossless motor, $P_{\text{OUT}} = P_{\text{IN}}$

$$\tau = \frac{p}{\omega} = \frac{\sqrt{3} V_T I_L \cos \theta}{\left(\frac{120 \times 60}{6}\right) \frac{2\pi}{60}}$$
$$= \frac{66.5 \times 1000}{\left(\frac{1200 \times 2\pi}{60}\right)} \approx 529 \text{Nm} \qquad \text{Choice (C)}$$

12. $P_3 = 80 \text{kW}$ $Q_3 = P \tan \theta = P \tan(\cos^{-1}(.85)) = 80 \text{ kW} \times \tan(-31.79^\circ)$ = -49.6 KVAr $P_2 = S \cos\theta = 90 \text{KVA} \times 0.8 = 72 \text{kW}$ $Q_2 = \sin \theta = 90 \text{KVA} \times 0.6 = 54 \text{KVA}r$ $P_1 = 100 \text{kW}$

$$Q_{1} = P \tan \theta = 100 \text{ kW}(\tan(\cos^{-1}0.9)) = 100\tan(25.8) = 48.4\text{KVAr}$$

$$\therefore \text{ Total real power = 252\text{kW}}$$

$$\text{Total reactive power = 52.8\text{KVAr} \text{ Choice (B)}$$

13. $V_{\text{phase}} = \frac{11500}{\sqrt{3}} = 6640\text{V}$
 $Z_{\text{base}} = \frac{3(6640)^{2}}{100 \times 10^{6}} = 1.32\Omega$
 $R_{d} = 0.012 \times 1.32 = 0.0158\Omega$
 $X_{s} = 0.9 \times 1.32 = 1.188\Omega$
Rated armature current $= \frac{S}{\sqrt{3}V_{T}} = \frac{100 \times 10^{6}}{\sqrt{3} \times 11.5 \times 10^{3}}$
 $= 5020\text{A}$
 $Pf = 0.75 \text{ lagging}, \therefore I_{a} = 5020\angle -41.41^{\circ}$
 $\therefore E_{A} = V_{\text{phase}} + R_{A}I_{A} + jX_{s}I_{A}$
 $= 6640\angle 0^{\circ} + (0.0158)(5020\angle -41.41^{\circ}) + j1.188(5020\angle -41.41^{\circ})$
 $= 6640 + 79.316 + j1(472.82 - j3936]$
 $= 6640 + 79.316 + j4472.82$
 $\therefore E_{A} = 11556.03\angle 22.73^{\circ} \approx 11556\angle 23^{\circ}$ Choice (D)
14. $E\angle 8 = V_{\angle} 20^{\circ} + I_{a}\angle 0 X_{a}\angle 90^{\circ}$
 $= 1\angle 0^{\circ} + 1.5\angle (90 + 30^{\circ})$
 $= 1 + (-0.75) + j1.3$
 $= 1.324\angle 79.1^{\circ} \approx 1.32\angle 79^{\circ}$ Choice (C)
15. $f = \frac{np}{120} = \frac{3600 \times 2}{120} = 60\text{Hz}$ Choice (B)
16. $N = \frac{120f_{1}}{P_{1}} = \frac{120f_{2}}{P_{2}}$
 $= \frac{120 \times 60}{R_{1}} = \frac{120 \times 25}{R_{2}}$
 $P_{1}/P_{2} = \frac{60}{25}$
 $P_{1}, P_{2} \leq 26$
 $\therefore P_{1}, P_{2} = 24, 10$
 $\therefore N = \frac{120 \times 26}{10} = 300 \text{ rpm}$
 $= \frac{120 \times 25}{10} = 300 \text{ rpm}$ Choice (C)
17. $I = 50000/200 = 250\text{A}$

17. I = 50000/200 = 250A $E = [(V\cos \Phi + IR_a)^2 + (V\sin \Phi - IX_L)^2]^{11/2}$ $= [(200 \times 0.8 + 250 \times 0.02)^2 +$ $(200 \times 0.6 - 250 \times 0.08)]^{1/2} = 192.93V$ Choice (B) 18. V = 1 p.u $X_d = 0.6$ p.u $X_a = 0.3$ p.u

$$\cos \phi = 0.7 \implies \phi = \cos^{-1}(0.7) = 45.57^{\circ}$$

$$\sin \phi = 0.7$$

$$I_a = 1 \text{ p.u}$$

$$\tan \delta = \frac{I_a X_q \cos \varphi}{V + I_a X_q \sin \varphi} = \frac{1 \times 0.3 \times 0.7}{1 + 1 \times 0.37 + 0.7} = 0.173$$

$$\delta = 9.81^{\circ}$$

$$I_d = I_a \sin[\Phi + \delta] = 1 \times \sin(45.57^{\circ} + 9.81^{\circ}) = 0.82$$

Choice (C)

19. Full load current
$$I = \frac{600 \times 10^3}{\sqrt{3} \times 11 \times 10^3} = 31.5 \text{A}$$

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$$V_{ph} = \frac{11000}{\sqrt{3}} = 6350V$$

$$IR_{a} = 0.02 \times 6350 = 127V$$

$$IX_{s} = 0.1 \times 6350 = 635 V \Longrightarrow X_{s} = 20.15 \Omega$$

$$E = [(V\cos \Phi + IR_{a})^{2} + (V\sin \Phi + IX_{s})^{2}]^{1/2}$$

$$= [(6350 \times 0.9 + 127)^{2} + (6350 \times 0.435 + 635)^{2}]^{1/2}$$

$$= 6757.97V$$

 $\alpha \text{ (mech)} = 1^{\circ} \Longrightarrow \alpha \text{ (elect)} = 1 \times \frac{6}{2} = 3^{\circ}$
 $\alpha = 3\pi/180 = \pi/60 \text{ elect.radi}$

$$P_{sy} = \frac{\frac{\pi}{60} \times 6757.97 \times 6350}{20.15} = 111.50 \text{ kW/phase}$$

Choice (B)

20.
$$\cos \phi = 0.75 \Rightarrow \phi = 41.40^{\circ}$$

Load kW = 20000 kW
Load KVAR = 20000 tan Φ
= 17632.37 KVAR
Load kw supplied by alternator *A*, kw₁ = 14000 kW
Load kw supplied by alternator *B*, kw₂ = 6000 kW
Load KVAR supplied by alternator *A* KVAR₁
= kw₁ × tan ϕ_1
 $\cos \phi_1 = 0.9 \Rightarrow \phi_1 = 25.84^{\circ}$
KVAR₁ = 14000 × tan(25.84)
= 6779.92 KVAR
Load KVAR₂ supplied by alternator *B* KVAR₂
= 17632.37 - 6779.92
= 10852.45 KVAR
KVA₂ = 6000 - ,10852.45
= 12400∠-61.06^{\circ}
 $\cos \phi_2 = 0.48$ lagging
Choice (A)
21. $\cos \Phi = 0.8 \Rightarrow \Phi = 36.86^{\circ}$
 $I = \frac{2000 \times 10^3}{\sqrt{3} \times 111 \times 10^3} = 104.97A$
 $IR_a = 104.97 \times 0.5 = 52.48V$
 $IX_s = 104.97 \times 5 = 524.85V$
 $V/\text{phase} = 11000/\sqrt{3} = 6350.85V$
 $V \sin \varphi + I X_s$
 $6350.85 \times 0.6 + 524.85$

$$\tan(\phi + \delta) = \frac{V \sin \phi + I X_s}{V \cos \phi + I R_a} = \frac{6550.85 \times 0.6 + 524.85}{6350.85 \times 0.8 + 52.48}$$
$$\tan(\phi + \delta) = 0.844$$

$$\begin{split} \phi + \delta &= 40.16 \Rightarrow \delta = 40.16 - 36.86^{\circ} \\ \Rightarrow \delta &= 3.30^{\circ} \\ \end{split}$$
Choice (C)
22. $\phi = \cos^{-1}(0.8) = 36.86^{\circ} \\ \theta &= \tan^{-1}\left(\frac{3}{0.4}\right) = 82.40^{\circ} \\ \theta + \phi &= 82.40 + 36.86 = 119.26^{\circ} \\ V &= \frac{2000}{\sqrt{3}} = 1154.70V \\ Z_s &= \sqrt{0.4^2 + 3^2} = 3.02 \ \Omega \\ IZ_s &= 300 \times 3.02 = 906 \ \Omega \\ E_b &= \sqrt{V^2 + E_R^2 - 2V \ E_R \cos(\theta + \varphi)} \\ &= \sqrt{(1154.70)^2 + (906)^2 - 2 \times 1154.70 \times 906 \times \cos(119.26)} \\ &= 1782.36 \ \text{volt/phase} \\ \text{Choice (C)} \\ 23. \ \text{Voltage/phase} &= \frac{1500}{\sqrt{3}} = 866.02V \\ \text{Induced e.m.f} &= 866.02V \\ \text{Induced e.m.f} &= 866.02V \\ \text{Impedance drop} &= 300 \times 4 = 1200V \\ 866^2 &= 866^2 + 1200^2 - 2 \times 866 \times 1200 \times \cos(90 - \Phi) \\ \sin \phi &= 0.692 \Rightarrow \phi &= 43.78^{\circ} \\ \text{Power input} &= \sqrt{3} \times 1500 \times 300 \times \cos(43.78^{\circ}) \\ &= 562.74kW \\ \text{Torque } T &= \frac{9.55 \times 562.74}{1000} = 5374.21 \ \text{N-m} \\ \end{split}$

24.
$$F_{nl1} = \frac{n_m P}{120} = \frac{3040 \times 2}{120} = 50.67 \text{Hz}$$

 $F_{fl1} = \frac{2975 \times 2}{120} = 49.58 \text{Hz}$
 $F_{nl2} = \frac{1500 \times 4}{120} = 50 \text{Hz}$
 $F_{fl2} = \frac{1485 \times 4}{120} = 49.5 \text{Hz}$
 $SD_1 = \frac{n_{nl} - n_{fl}}{n_{fl}} \times 100\% = \frac{3040 - 2975}{2975} \times 100 = 2.18\%$
 $SD_2 = \frac{1500 - 1485}{1485} \times 100 = 1.01\%$ Choice (A)

25.
$$P_2 = S_{P2} (f_{nl2} - f_{sys}) = 360[50 - 49.8] = 72 \text{kW}$$

 $S_{P2} = \frac{P}{f_{nl} - f_{fl}} = \frac{180 \text{kW}}{50 - 49.5} = 360 \text{kW/Hz}$
 $(S_{pl} = 183.48 \text{KW/Hz})$
 $P_{Load} = S_{pl} (f_{nL} - f_{sys}) + S_{p2} (f_{nl} - f_{sys})$
 $\Rightarrow 200 = 183.48 (50.67 - f_{sys}) + 360 (50 - f_{sys})$
 $\Rightarrow f_{sys} = 49.8$ Choice (B)