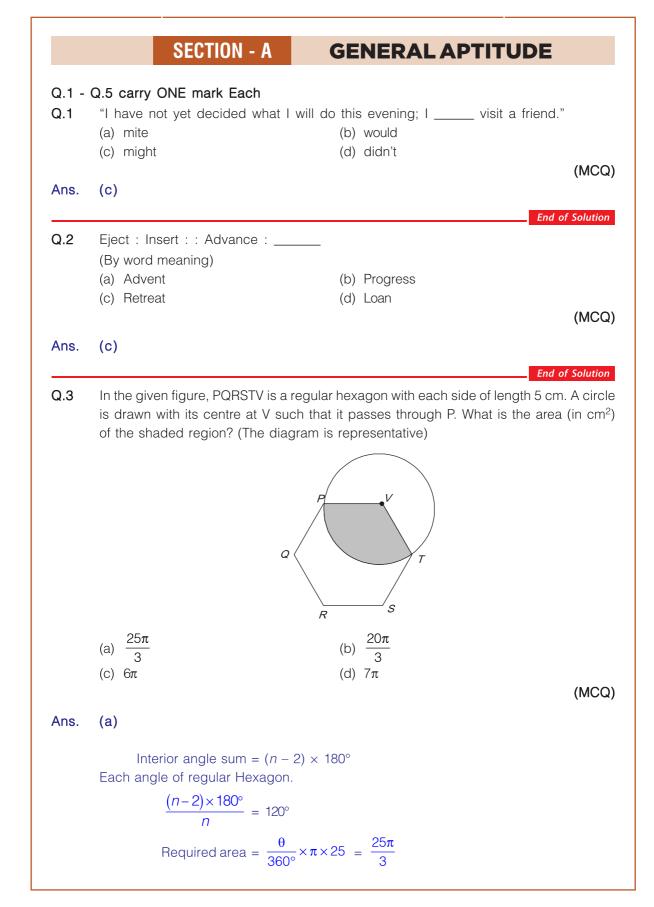
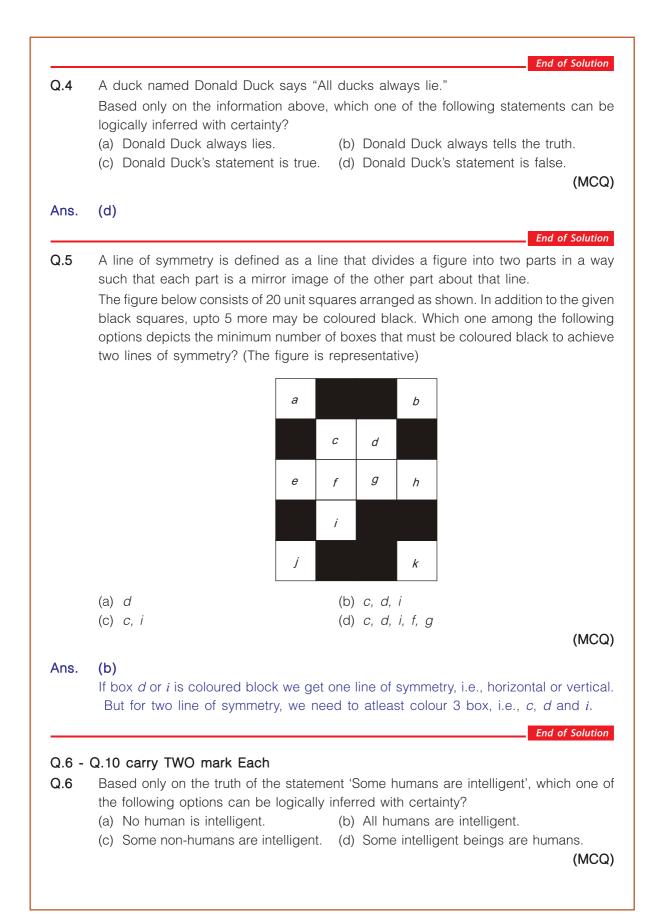
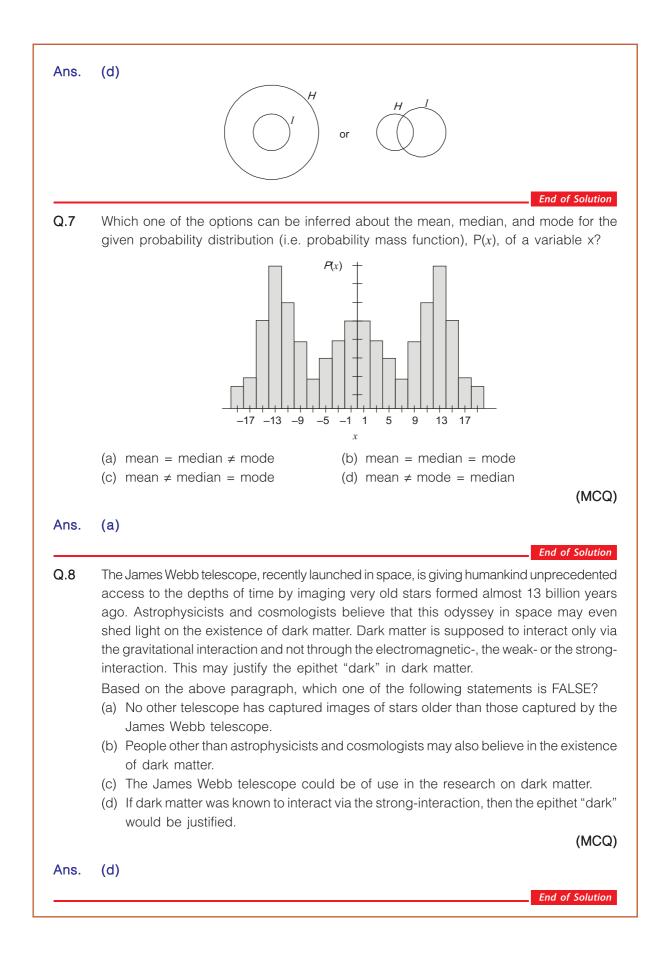
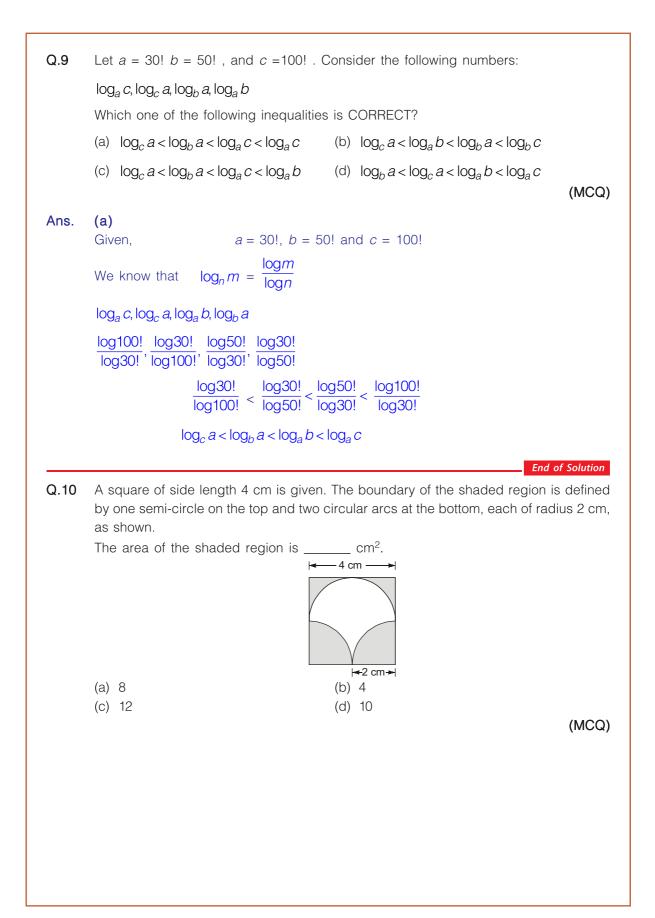
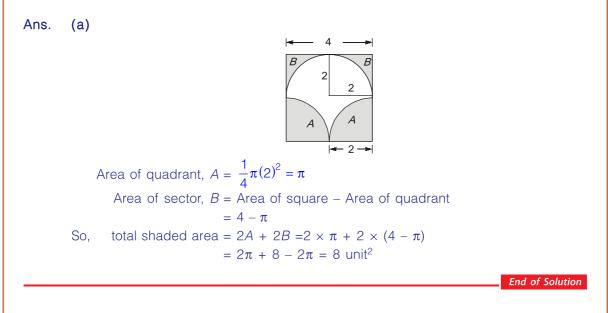
GATE 2023 Civil Engineering Exam Held on : 12-2-2023 Forenoon Session

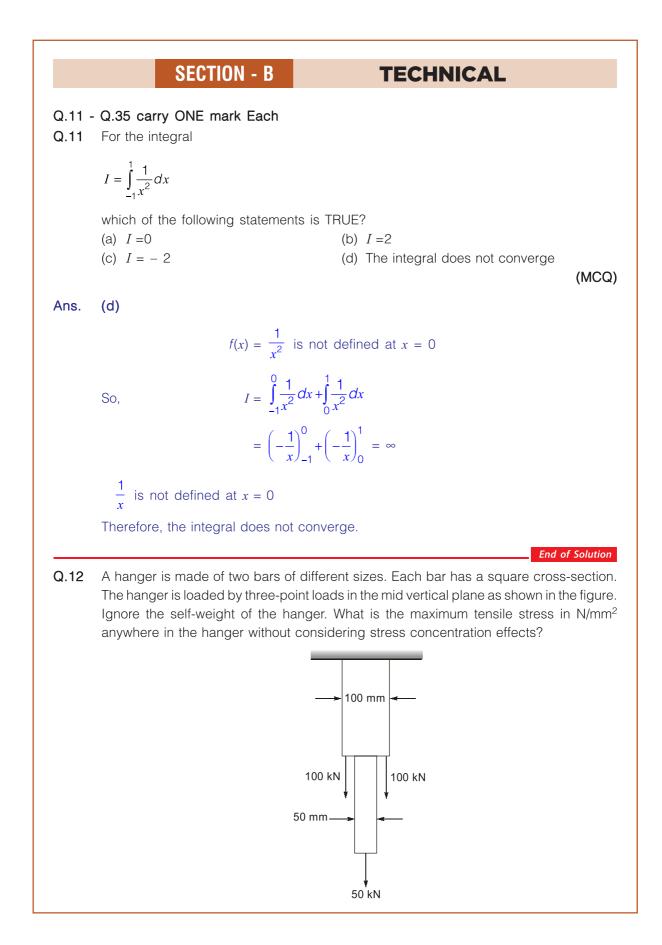


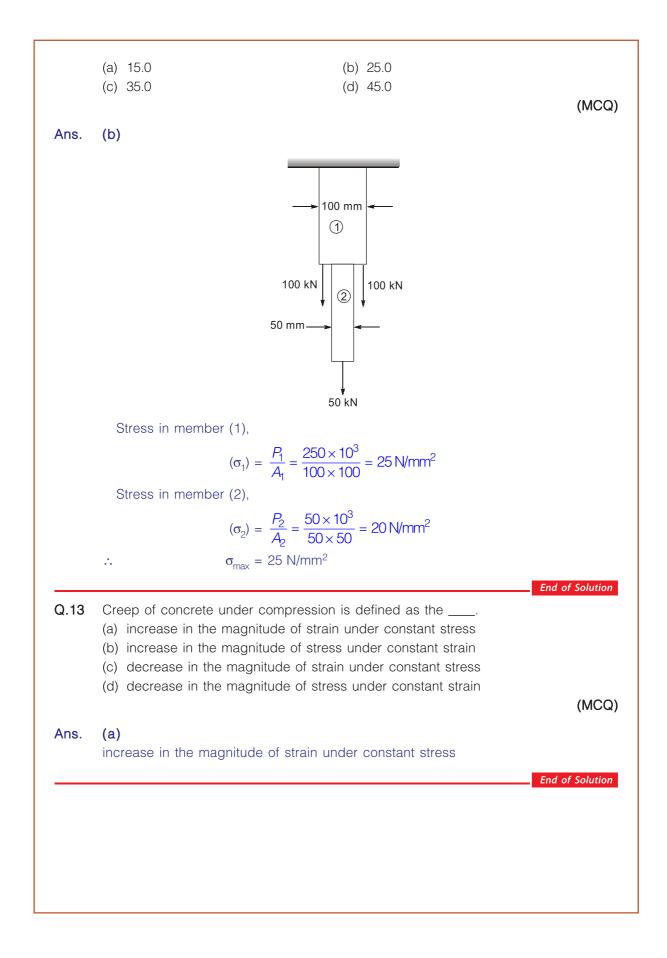


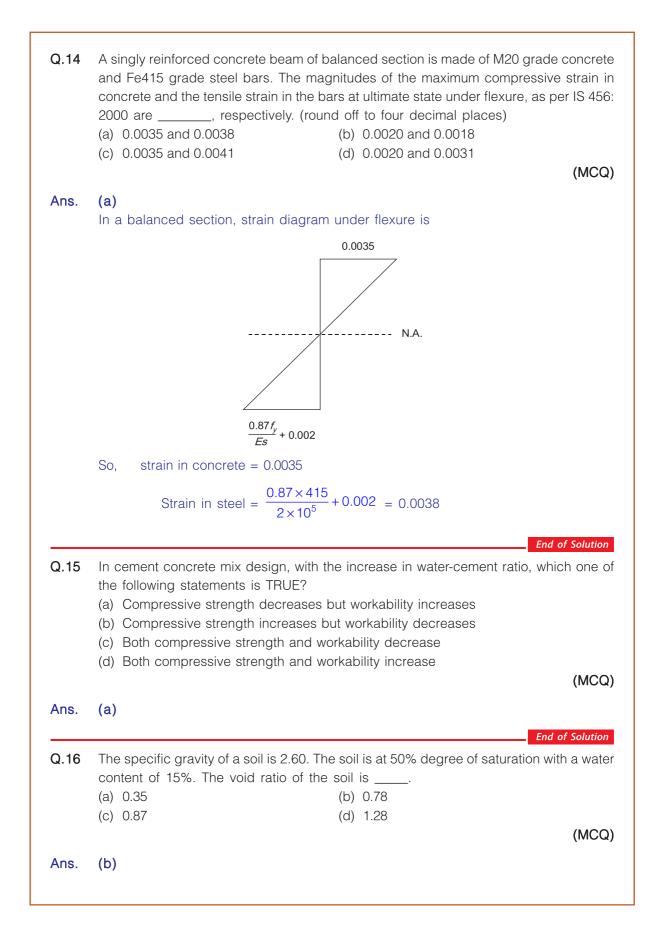


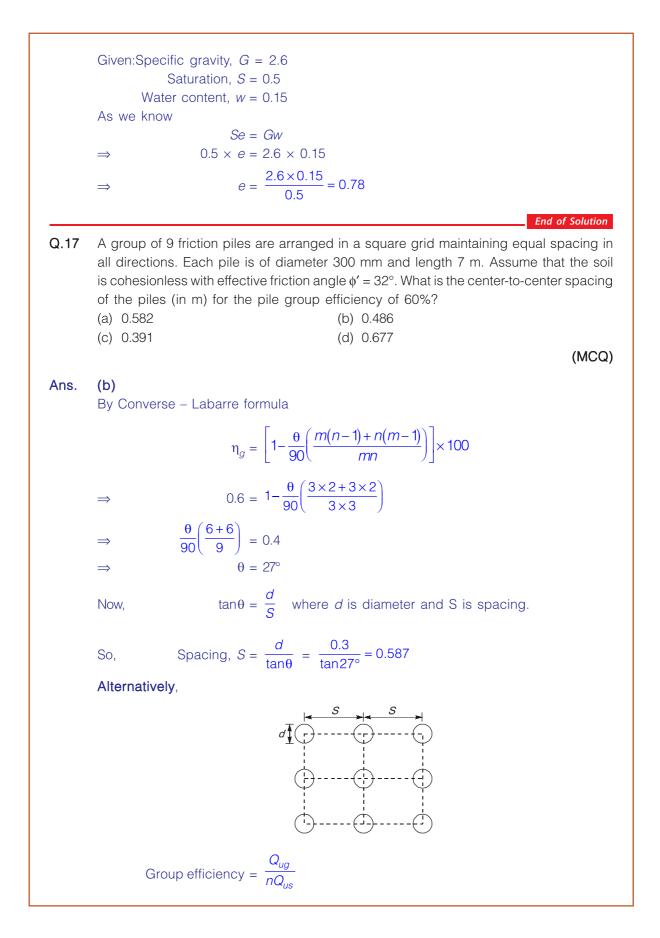


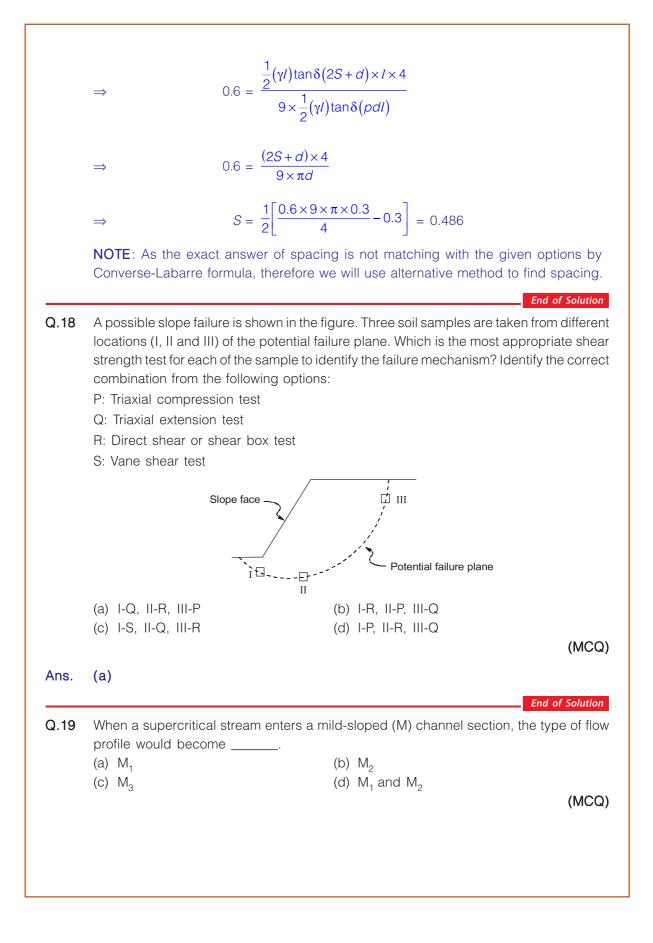


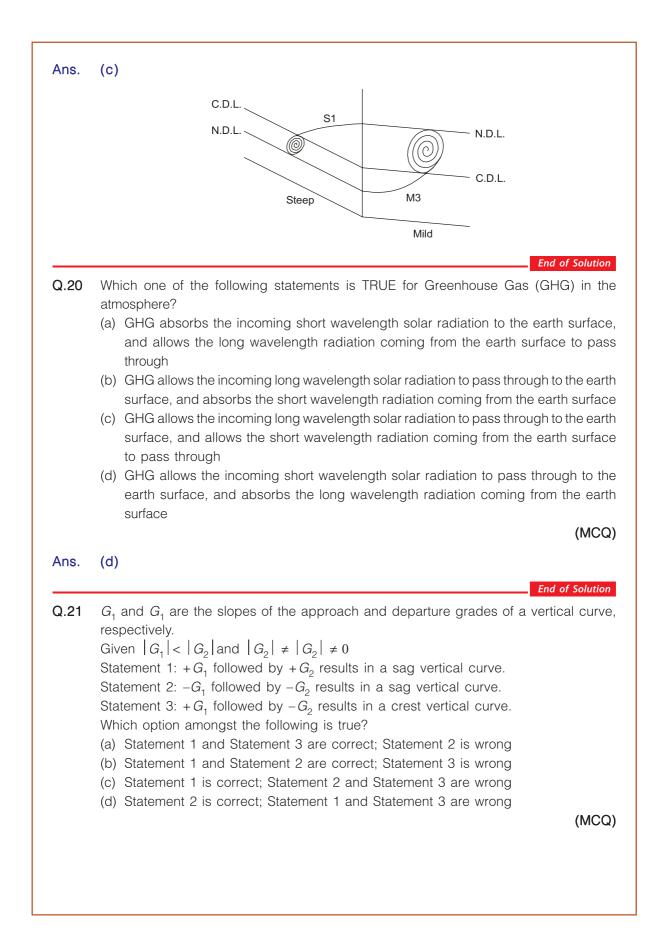


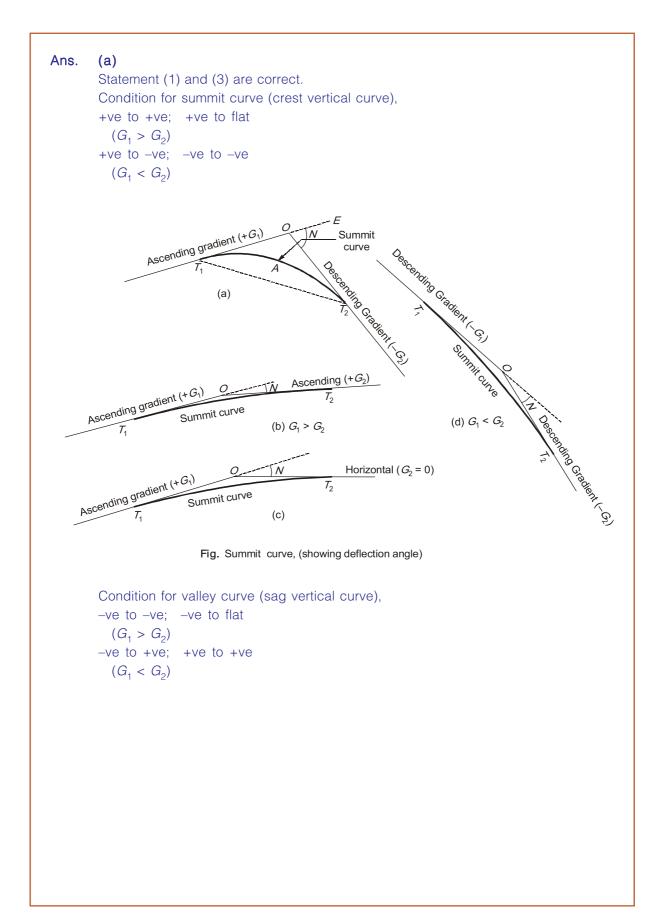


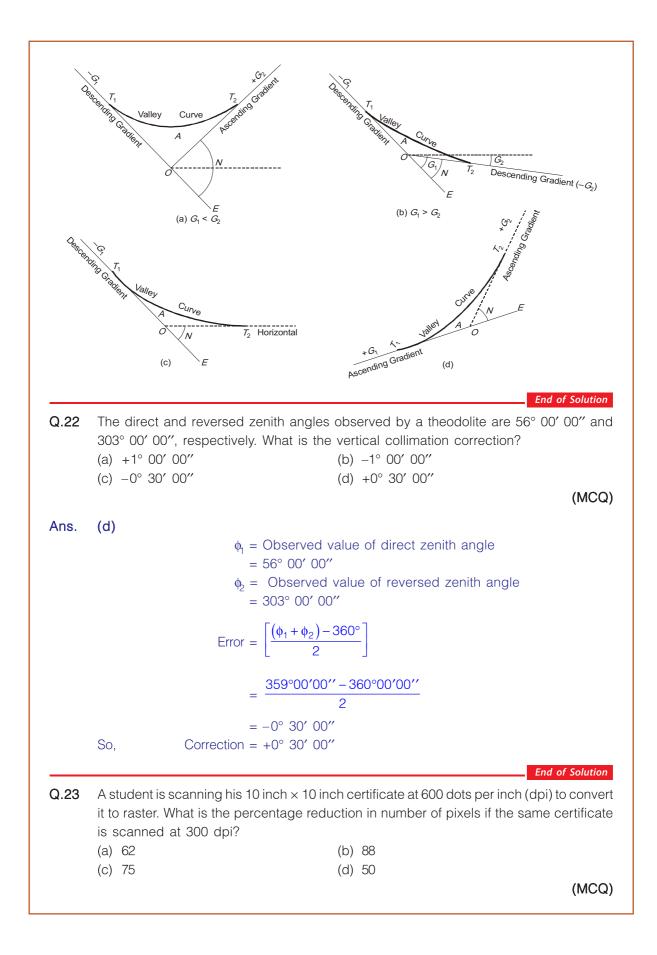












Ans. (c) Number of dots as per 600 dpi = $(10 \times 600)^2$ = 36000000 Number of dots as per 300 dpi = $(10 \times 300)^2 = 9000000$ Percentage reduction in number of pixels End of Solution Q.24 If M is an arbitrary real $n \times n$ matrix, then which of the following matrices will have nonnegative eigenvalues? (b) *MM*^T (a) *M*² (d) $(M^T)^2$ (c) $M^T M$ (MSQ) Ans. (b, c) $M = \begin{bmatrix} 0 & -1 \\ 1 & 0 \end{bmatrix}$ then E. values are $\lambda = \pm i$ Let us take So, Eigen values of M^2 are i^2 and $(-i)^2 = -1, -1$ Eigen values of $(M^T)^2$ are same i.e. -1, -1Now, MM^{T} and $M^{T}M$ are symmetric matrix, as well as the semi definite matrix and it is the property of +ve semi definite matrix that it's eigen values are non -ve. Hence correct answer (b) and (c). End of Solution Q.25 The following function is defined over the interval [-L, L]: $F(x) = \rho x^4 + q x^5$ If it is expressed as a Fourier series, $F(x) = a_0 + \sum_{n=1}^{\infty} \left\{ a_n \sin\left(\frac{\pi x}{L}\right) + b_n \cos\left(\frac{\pi x}{L}\right) \right\}$ which options amongst the following are true? (a) a_n , $n = 1, 2, ..., \infty$ depend on p(b) a_n , $n = 1, 2, ..., \infty$ depend on q(c) b_n , $n = 1, 2, ..., \infty$ depend on p(d) b_n , $n = 1, 2, ..., \infty$ depend on q(MSQ) Ans. (b, c)

$$b_n = \frac{1}{l} \int_{-l}^{l} f(x) \cos \frac{(n\pi x)}{l} dx = \frac{1}{l} \int_{-l}^{l} (px^4 + qx^5) \cos \left(\frac{n\pi x}{l}\right) dx$$
$$= \frac{1}{l} \int_{-l}^{l} px^4 \cos \frac{(n\pi x)}{l} dx + 0 \qquad (\because 2^{nd} \text{ integral is an odd functions})$$

Thus, b_n depend on p

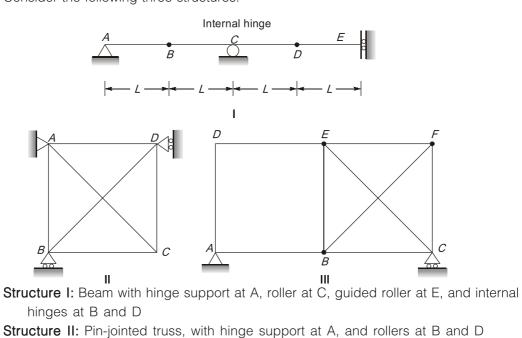
Similarly,
$$a_n = \frac{1}{l} \int_{-l}^{l} f(x) \sin \frac{(n\pi x)}{l} dx = \frac{1}{l} \int_{-l}^{l} (px^4 + qx^5) \sin \left(\frac{n\pi x}{l}\right) dx$$

= $0 + \frac{1}{l} \int_{-l}^{l} qx^5 \sin \frac{(n\pi x)}{l} dx$ (:.1st integral is an odd functions)

Thus, a_n depend on q.

End of Solution

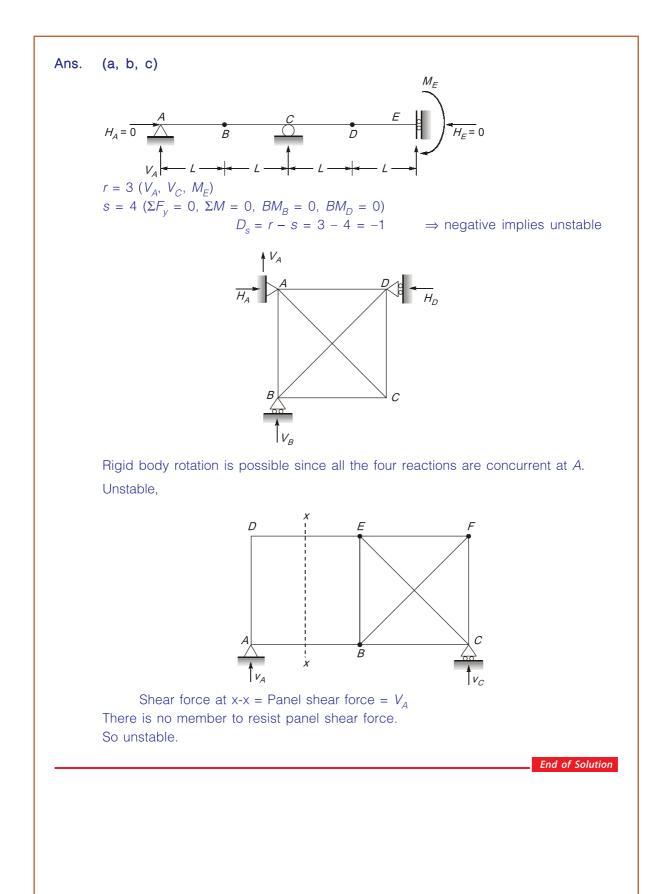
Q.26 Consider the following three structures:



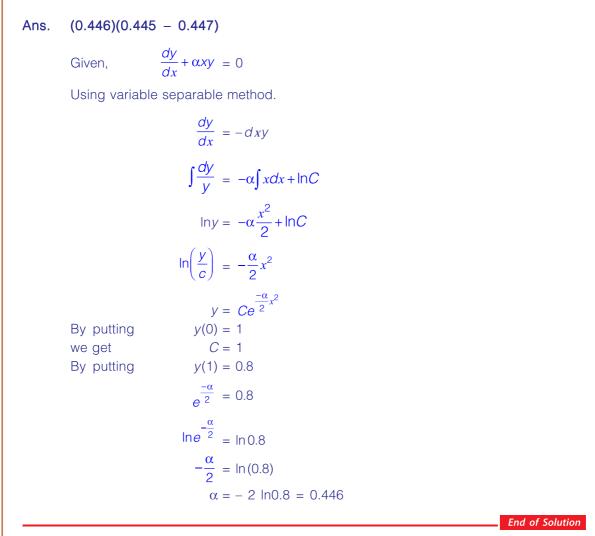
Structure III: Pin-jointed truss, with hinge support at A and roller at C Which of the following statements is/are TRUE?

- (a) Structure I is unstable
- (b) Structure II is unstable
- (c) Structure III is unstable
- (d) All three structures are stable

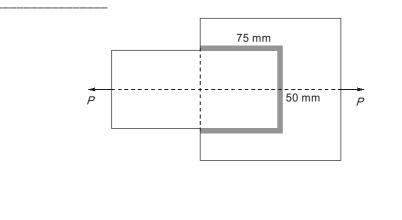
(MSQ)



Q.27	Identify the waterborne diseases caused by viral pathogens:(a) Acute anterior poliomyelitis(b) Cholera(c) Infectious hepatitis(d) Typhoid fever				
Ans.	(MSQ) (a, c)				
Q.28	 Which of the following statements is/are TRUE for the Refuse-Derived Fuel (RDF) in the context of Municipal Solid Waste (MSW) management? (a) Higher Heating Value (HHV) of the unprocessed MSW is higher than the HHV of RDF processed from the same MSW (b) RDF can be made in the powdered form (c) Inorganic fraction of MSW is mostly converted to RDF (d) RDF cannot be used in conjunction with oil 				
Ans.	(b)				
Q.29	2.29 The probabilities of occurrences of two independent events A and B are 0.5 and 0.8 respectively. What is the probability of occurrence of at least A or B (rounded off t one decimal place)?				
Ans.	(NAT) (0.9)(0.9 - 0.9) Given, $P(A) = 0.5$ and $P(B) = 0.8$ and A and B are independents. $P(A \cup B) = P(A) + P(B) - P(A \cap B)$ = P(A) + P(B) - P(A)P(B) $= 0.5 + 0.8 - 0.5 \times 0.8 = 0.9$ End of Solution				
Q.30	In the differential equation $\frac{dy}{dx} + \alpha xy = 0$, α is a positive constant. If $y = 1.0$ at $x = 0.0$, and $y = 0.8$ at $x = 1.0$, the value of α is(rounded off to three decimal places). (NAT)				



Q.31 Consider the fillet-welded lap joint shown in the figure (not to scale). The length of the weld shown is the effective length. The welded surfaces meet at right angle. The weld size is 8 mm, and the permissible stress in the weld is 120 MPa. What is the safe load P (in kN, rounded off to one decimal place) that can be transmitted by this welded joint?



(NAT)

Ans. (134.4) (134 - 136) $S = 8 \text{ mm}, \tau_{vw} = 120 \text{ MPa}, L_w = 2 \times 75 + 50 = 200 \text{ mm}$ Given: The safe load is calculated as per WSM *.*•. $\rho_{\text{safe}} = \tau_{vw} \times A_w$ $= \tau_{_{VW}} \times L_{_W} \times (0.7 \times s)$ $[:: t_t = 0.7s]$ $= 120 \times [2 \times 75 + 50] \times 0.7 \times 8 \times 10^{-3} \text{ kN} = 134.4 \text{ kN}$ End of Solution Q.32 A drained direct shear test was carried out on a sandy soil. Under a normal stress of 50 kPa, the test specimen failed at a shear stress of 35 kPa. The angle of internal friction of the sample is ______degree (round off to the nearest integer). (NAT) Ans. (35)(35 - 35)Given, Normal stress, $\sigma_n = 50$ kPa Shear stress, $\tau = 35$ kPa $\tau = c + \sigma_{p} \tan \phi$ $35 = 50 \tan \phi$ (:: c = 0, sandy soil) \Rightarrow $\tan \phi = 0.7$ \Rightarrow $\phi = 35^{\circ}$ \Rightarrow End of Solution Q.33 A canal supplies water to an area growing wheat over 100 hectares. The duration between the first and last watering is 120 days, and the total depth of water required by the crop is 35 cm. The most intense watering is required over a period of 30 days and requires a total depth of water equal to 12 cm. Assuming precipitation to be negligible and neglecting all losses, the minimum discharge (in m³/s, rounded off to three decimal places) in the canal to satisfy the crop requirement is _ (NAT) Ans. (0.046)(0.045 - 0.047)Area : 100 ha Given: Total depth of water, Δ_2 = 35 cm Total time period, $B_2 = 120$ days Kor depth, $\Delta_1 = 12$ cm Kor period, $B_1 = 30$ days Kor duty, $\Delta_1 = \frac{8.64 \times B_1}{\Delta_1} = \frac{8.64 \times 30}{0.12} = 2160 \text{ ha/m}^3/\text{sec}$ (i) Corresponding discharge = $\frac{\text{Area}}{\text{Duty}} = \frac{100}{2160} = 0.046 \text{ m}^3/\text{sec}$ Overall duty, $\Delta_2 = \frac{8.64 \times B_2}{\Delta_2} = \frac{8.64 \times 120}{0.35} = 2962.28 \text{ ha/m}^3/\text{sec}$ (ii)

Corresponding discharge = $\frac{\text{Area}}{\text{Duty}} = \frac{100}{2962.28} = 0.034 \text{ m}^3/\text{sec}$ Minimum discharge required will be maximum of the above two. \therefore $Q_{\text{reg.}} = 0.046 \text{ m}^3/\text{sec}$

End of Solution

(NAT)

Q.34 The ordinates of a one-hour unit hydrograph for a catchment are given below:

t(hour)	0	1	2	3	4	5	6	7
$Q(m^3/s)$	0	9	21	18	12	5	2	0

Using the principle of superposition, a D-hour unit hydrograph for the catchment was derived from this one-hour unit hydrograph. The ordinates of the D-hour unit hydrograph were obtained as 3 m³/s at t = 1 hour and 10 m³/s at t = 2 hour. The value of D (in integer) is ______.

Ans. (3)(3 -3)

Time	1hr-UH	1hr UH lagged by 1 hr	1hr-UH lagged by 1 more hr	3 hr DRH	Ordinate of 3hr UH = $\frac{\text{Ordinate of 3hr DRH}}{3\text{cm}}$
(1)	(2)	(3)	(4)	(5)	(6)
0	0	-	-	0	0
1	9	0	-	9	3
2	21	9	0	30	10
3	18	21	9	48	16
4	12	18	21	51	17
5	5	12	18	35	11.67
6	2	5	12	19	6.33
7	0	2	5	7	2.33
		0	2	2	0.67
			0	0	0

- Firstly lag the UH by 1 hr. By lagging 1 hr. We obtained a 2 hr UH of ordinate 4.5 m³/sec. at 1 hr and 15 m³/sec at 2 hr.
- So, further lag the UH by 1 more hr we obtained a 3 hr, UH of ordinates 3 m³/sec at 1 hr and 10 m³/sec at 2 hr. Therefore D = 3 hr.

Q.35 For a horizontal curve, the radius of a circular curve is obtained as 300 m with the design speed as 15 m/s. If the allowable jerk is 0.75 m/s³, what is the minimum length (in m, in integer) of the transition curve?

(NAT)

Ans. (15)(15 – 15)

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Given:
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V = 15 m/sR = 300 mJerk, $C = 0.75 \text{ m}^3/\text{s}$

So, height of transition curve,

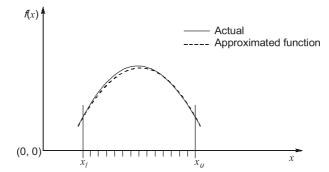
$$L_t = \frac{V^3}{RC} = \frac{15^3}{300 \times 0.75} = 15 \text{ m}$$

Note: We should also find out the length by formula given by IRC but terrain is not mentioned.

End of Solution

Q.36 - Q.65 carry TWO mark Each

Q.36 A function f(x), that is smooth and convex-shaped between interval (x_l, x_u) is shown in the figure. This function is observed at odd number of regularly spaced points. If the area under the function is computed numerically, then .

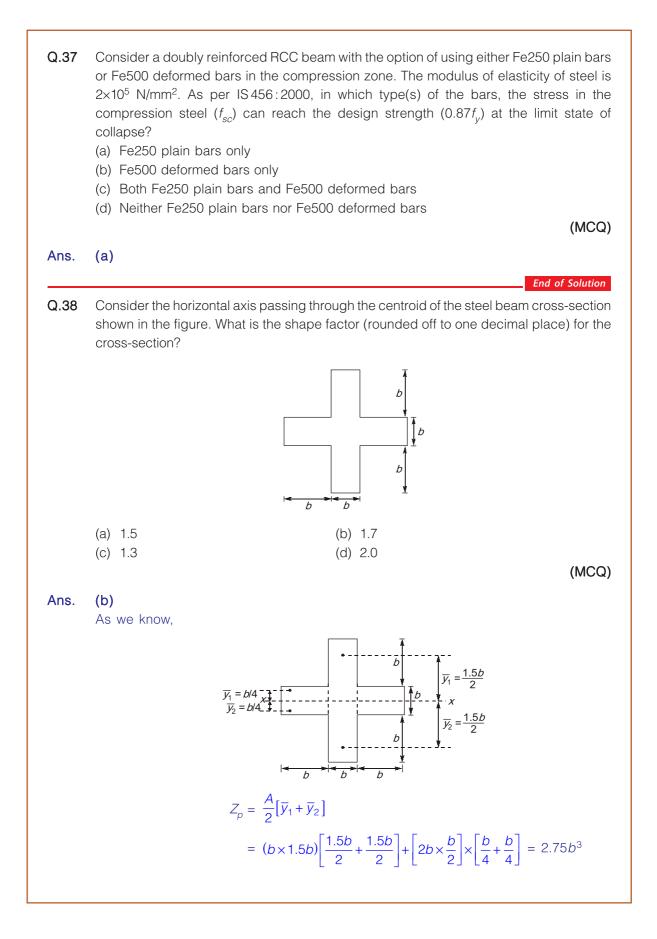


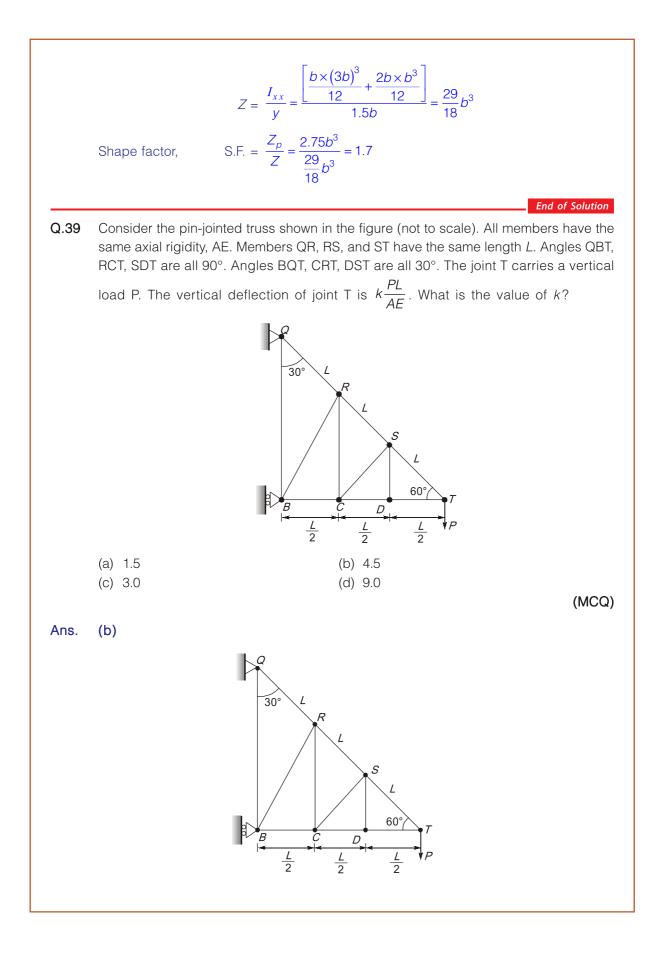
- (a) the numerical value of the area obtained using the trapezoidal rule will be less than the actual
- (b) the numerical value of the area obtained using the trapezoidal rule will be more than the actual
- (c) the numerical value of the area obtained using the trapezoidal rule will be exactly equal to the actual
- (d) with the given details, the numerical value of area cannot be obtained using trapezoidal rule

(MCQ)

Ans. (a)

Using the standard property of trapezoidal rule for converse shaped parabola, the numerical value of the area obtained using the trapezoidal rule will be less than the actual.





- Q.40 With reference to the compaction test conducted on soils, which of the following is INCORRECT?
 - (a) Peak point of the compaction curve gives the maximum dry unit weight and optimum moisture content
 - (b) With increase in the compaction effort, the maximum dry unit weight increases
 - (c) With increase in the compaction effort, the optimum moisture content decreases
 - (d) Compaction curve crosses the zero-air-voids curve

(MCQ)

Ans. (d)

Zero air void line do not cross compaction curve.

End of Solution

Q.41 Consider that a force P is acting on the surface of a half-space (Boussinesq's problem). The expression for the vertical stress (σ_z) at any point (*r*, *z*), within the half-space is given as,

$$\sigma_z = \frac{3P}{2\pi} \frac{z^3}{(r^2 + z^2)^{\frac{5}{2}}}$$

where, *r* is the radial distance, and *z* is the depth with downward direction taken as positive. At any given r, there is a variation of σ_z along *z*, and at a specific *z*, the value of σ_z will be maximum. What is the locus of the maximum σ_z ?

(a)
$$z^2 = \frac{3}{2}r^2$$

(b) $z^3 = \frac{3}{2}r^2$
(c) $z^5 = \frac{5}{2}r^2$
(d) $z^3 = \frac{5}{2}r^2$

(MCQ)

Ans. (a)

At given rFor maximum σ_z

$$\frac{d\sigma_z}{dz} = 0$$

$$\sigma_z = \frac{3P}{2\pi} \frac{z^3}{(r^2 + z^2)^{5/2}}$$

$$\Rightarrow \qquad \frac{d\sigma_z}{dz} = \frac{3P}{2\pi} \left[\frac{(r^2 + z^2)^{5/2} 3z^2 - z^3 \cdot \frac{5}{2} (r^2 + z^2)^{3/2} \cdot 2z}{(r^2 + z^2)^5} \right] =$$

$$\Rightarrow (r^2 + z^2)^{3/2} z^2 \left[3(r^2 + z^2) - 5z^2 \right] = 0$$

$$\Rightarrow \qquad 3r^2 + 3z^2 - 5z^2 = 0$$

$$\Rightarrow \qquad 3r^2 = 2z^2$$

$$\Rightarrow \qquad z^2 = \frac{3r^2}{2}$$

End of Solution

0

Q.42 A square footing of size 2.5 m \times 2.5 m is placed 1.0 m below the ground surface on a cohesionless homogeneous soil stratum. Considering that the groundwater table is located at the base of the footing, the unit weights of soil above and below the groundwater table are 18 kN/m³ and 20 kN/m³, respectively, and the bearing capacity factor N_q is 58, the net ultimate bearing capacity of the soil is estimated as 1706 kPa (unit weight of water = 10 kN/m³).

Earlier, a plate load test was carried out with a circular plate of 30 cm diameter in the same foundation pit during a dry season, when the water table was located beyond the plate influence zone. Using Terzaghi's bearing capacity formulation, what is the ultimate bearing capacity (in kPa) of the plate?

(a) 110.16(b) 61.20(c) 204.00(d) 163.20

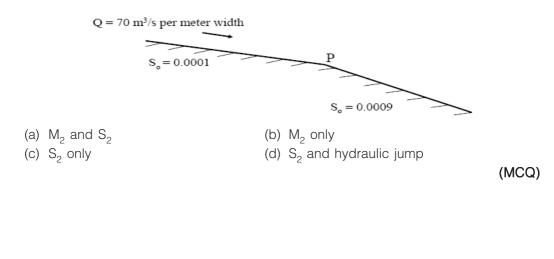
Ans. (a)

 $\begin{aligned} q_{\rm nu} &= q_u - \overline{\sigma} = q_u - \gamma D_f \\ 1706 &= \left\{ 1.3 C N_C + \gamma D_f N_q + 0.4 B \gamma N_\gamma \right\} - \gamma D_f \\ 1706 &= 18 \times 1 \times 58 + 0.4 \times 2.5 \times 10 \ N_\gamma - 18 \gamma_f \\ N_\gamma &= 68 \end{aligned}$ For Plate: [Surcharge at the plate level is zero] $\begin{aligned} q_u &= 1.3 C N_c + \gamma D_f N_q + 0.3 B \gamma N_\gamma \\ q_u &= 0 + 0.3 \times 0.3 \times 18 \times 68 \\ q_u &= 110.16 \end{aligned}$

End of Solution

(MCQ)

Q.43 A very wide rectangular channel carries a discharge (Q) of 70 m³/s per meter width. Its bed slope changes from 0.0001 to 0.0009 at a point P, as shown in the figure (not to scale). The Manning's roughness coefficient of the channel is 0.01. What water surface profile(s) exist(s) near the point P?



Ans. (a)

For a wide Rectangular channel

$$R = \frac{A}{P} = \frac{By}{B+2y} \approx \frac{By}{b} = y$$

Dischare per unit width, q is given by,

$$\Rightarrow$$

 $q = \frac{1}{n} y y^{2/3} S^{1/2}$

 \Rightarrow

 $q = \frac{1}{n} y^{5/3} S^{1/2}$

Calculation of S_{c} ,

$$y_{c} = \left(\frac{q^{2}}{g}\right)^{1/3}$$
$$q = \frac{1}{n}y_{c}^{5/3}S_{c}^{1/2}$$

 \Rightarrow

$$\Rightarrow$$

 \Rightarrow

 \Rightarrow

$$q = \frac{1}{n} \left(\frac{q^2}{g}\right)^{5/3} S_c^{1/2}$$
$$q = \frac{1}{n} \frac{q^{10/9}}{g^{5/3}} S_s^{1/2}$$

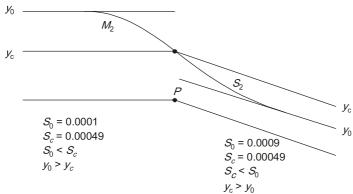
$$G^{=} n g^{5/3}$$
$$S_{c}^{1/2} = \frac{n q g^{5/9}}{q^{10/9}}$$

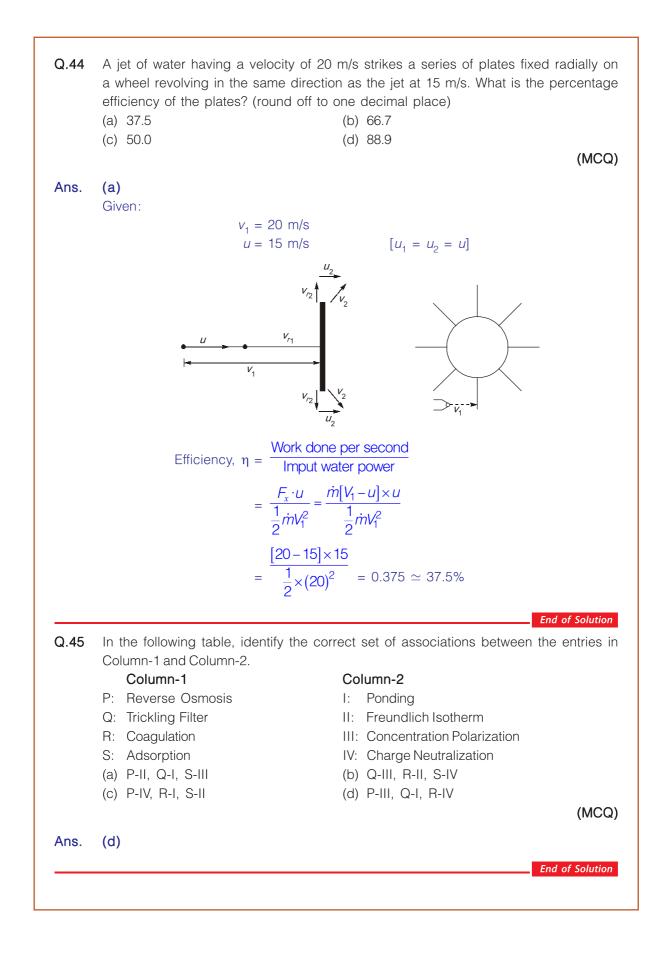
$$S_{c}^{1/2} = -$$

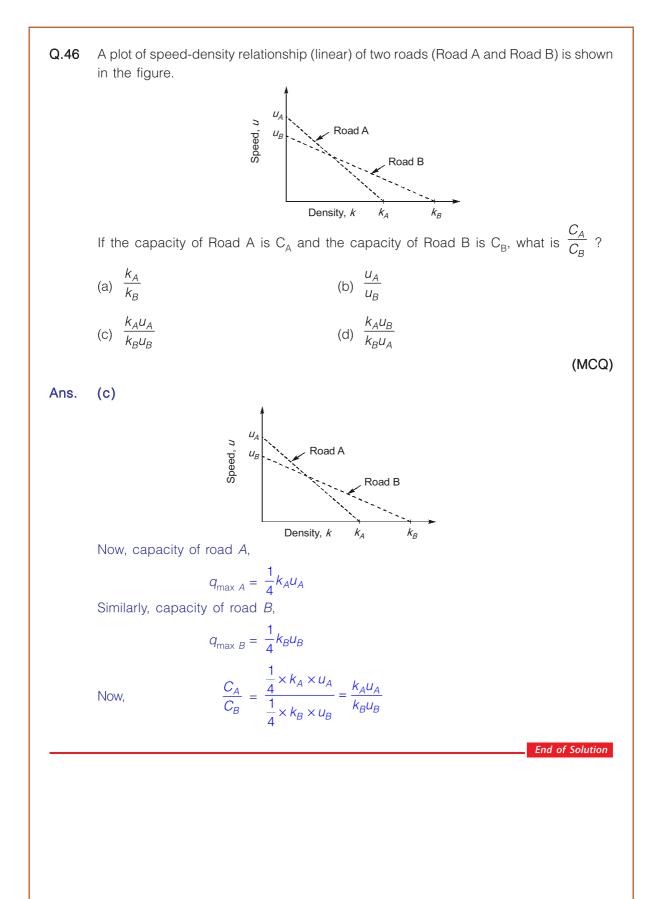
$$\Rightarrow$$

$$S_c = \left(\frac{ng^{5/9}}{q^{1/9}}\right)^2 = \left(\frac{0.01 \times 9.8^{5/9}}{70^{1/9}}\right)^2$$

= 0.00049 (> 0.0001 and < 0.0009)







Q.47 For the matrix

$$[A] = \begin{bmatrix} 1 & 2 & 3 \\ 3 & 2 & 1 \\ 3 & 1 & 2 \end{bmatrix}$$

Which of the following statements is/are TRUE?

- (a) The eigenvalues of $[A]^T$ are same as the eigenvalues of [A]
- (b) The eigenvalues of $[A]^{-1}$ are the reciprocals of the eigenvalues of [A]
- (c) The eigenvectors of $[A]^{T}$ are same as the eigenvectors of [A]
- (d) The eigenvectors of $[A]^{-1}$ are same as the eigenvectors of [A]

(MSQ)

Ans. (a, b, d)

Using standard properties of eigen values eigen vectors,

- Eigen values of A^T and A are same.
- Eigen values of A^{-1} is reciprocal of Eigen value of A.
- Eigen vectors of A⁻¹ are same as the eigenvectors of A.

Row space and column space for any matrix are not same. Thus option (c) is false.

End of Solution

Q.48 For the function $f(x)=.e^x |\sin x|_{x \in \mathbb{R}}$ which of the following statements is/are TRUE? (a) The function is continuous at all x

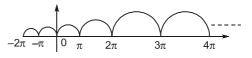
- (b) The function is differentiable at all x
- (c) The function is periodic
- (d) The function is bounded

(MSQ)

Ans. (a)

Given:

 $f(x) = e^x |\sin x|$



By observing graph we can easily say given function is neither periodic, nor bounded and nor differentiable, but is continuous at all x.

Q.49 Consider the beam shown in the figure (not to scale), on a hinge support at end A and a roller support at end B. The beam has a constant flexural rigidity, and is subjected to the external moments of magnitude M at one-third spans, as shown in the figure. Which of the following statements is/are TRUE? (a) Support reactions are zero (b) Shear force is zero everywhere (c) Bending moment is zero everywhere (d) Deflection is zero everywhere (MSQ) Ans. (a, b) $\Sigma F_v = 0$ $\Sigma F_{y} = 0$ $V_{A} + V_{B} = 0$ $\Sigma M_{A} = 0$ $V_{B} \times L - M + M = 0$ $V_{B} = 0$...(i) ... \Rightarrow $V_B = 0$ λ. from equation (i), we get $V_A = 0$:. shear force is zero everywhere in the beams, and reactions are also zero. Bending moment diagram is shown below $A \xrightarrow{| \bullet \ } M \qquad M$ So, bending moment is not zero everywhere. Also deflection is not zero everywhere. End of Solution

Q.50	 Which of the following statements is/are TRUE in relation to the Maximum Mixing Depth (or Height) 'D_{max}' in the atmosphere? (a) D_{max} is always equal to the height of the layer of unstable air (b) Ventilation coefficient depends on D_{max} (c) A smaller Dmax will have a smaller air pollution potential if other meteorological conditions remain same (d) Vertical dispersion of pollutants occurs up to D_{max} 			
Ans.	 (b, d) Maximum Mixing Depth (MMD) The dispersion of pollutants in the lower atmosphere is greatly aided by the convective and turbulent mixing that takes place. The vertical extent to which this mixing takes place depends on the environmental lapse rate which varies diurnally, from season to season and is also affected by topographical features. The depth of the convective mixing layer in which vertical movement of pollutants is possible, is called the maximum mixing depth (MMD). The ventilation coefficient is the product of mixing depth and the average wind speed. 			
Q.51	Which of the following options match the test reporting conventions with the given material tests in the table?Test reporting convention (P) Reported as ratio (Q) Reported as percentage (R) Reported in temperature (S) Reported in lengthMaterial test (I) Solubility of bitumen (III) Los Angeles abrasion test (IV) Flash point of bitumen (V) Ductility of bitumen (V) Specific gravity of bitumen (VI) Specific gravity of bitumen (VI) Thin film oven test(a) $(P) - (VI); (Q) - (I); (R) - (II); (S) - (VII)(b) (P) - (VI); (Q) - (II); (R) - (IV); (S) - (V)(c) (P) - (VI); (Q) - (II); (R) - (IV); (S) - (V)(d) (P) - (VI); (Q) - (III); (R) - (IV); (S) - (VII)$			
Ans.	 (b, c) Specific gravity of bitumen is the ratio of mass of given volume of substance to the mass of equal volume of water, the temperature of both being specified. (P) - (VI); (Q) - (I, III, VII); (R) - (II, IV); (S) - (V) End of Solution			

Q.52 The differential equation,

$$\frac{du}{dt} + 2tu^2 = 1,$$

is solved by employing a backward difference scheme within the finite difference framework. The value of u at the (n-1)th time-step, for some n, is 1.75. The corresponding time (t) is 3.14 s. Each time step is 0.01 s long. Then, the value of $(u_n - u_{n-1})$ is ______. (round off to three decimal places).

(NAT)

Ans. (-0.151) (-0.152 to -0.149)

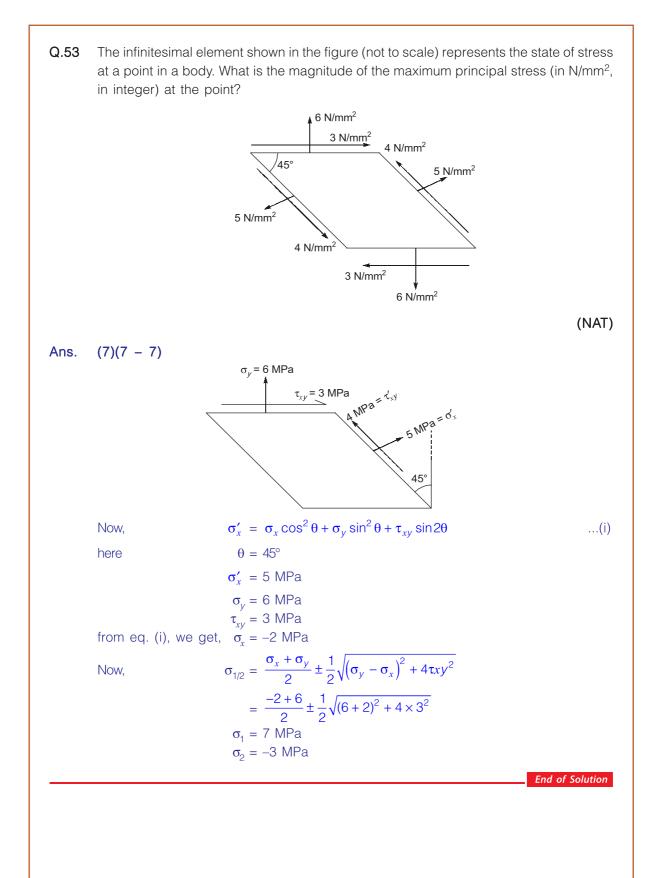
Given differential equation

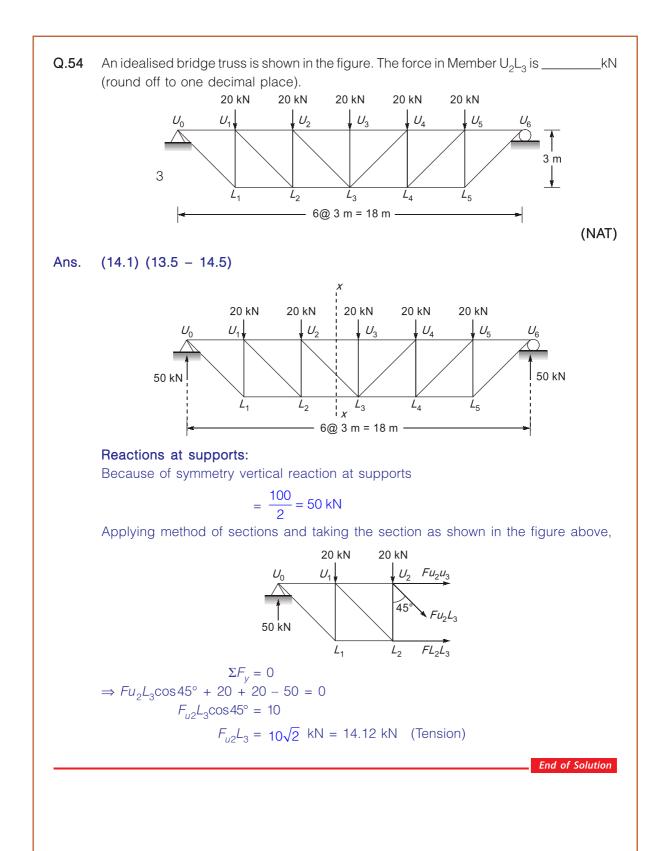
$$\frac{du}{dt} + 2tu^2 = 1$$

$$\frac{du}{dt} = f(t, u) = 1 - 2tu^2$$

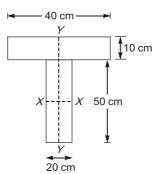
By backward Euler Iterative scheme,

	$u_n = u_{n-1} + hf(t_n, u_n)$	
	$u_n = u_{n-1} + h[1 - 2t_n u_n^2]$	(i)
Given,	$h = 0.01, \ u_{n-1} = 1.75, \ t_{n-1} = 3.14$	
So,	$t_n = t_{n-1} + h = 3.15$	
Putting thes	e values in (i)	
	$u_n = 1.75 + 0.01[1 - 2 \times 3.15 \times u_n^2]$	
	$u_n = 1.75 + 0.01 - 0.628 u_n^2$	
or $0.628u_n^2$	$u^2 + u_n - 1.75 = 0$	
$62.8u_n^2 +$	$100u_n + 175 = 0$	
\Rightarrow	$u_n = 1.599 - 17.472$	
So, for	$u_n = 1.599$ and $u_{n-1} = 1.75$	
We have,	$u_n - u_{n-1} = 1.599 - 1.75 = -0.151$	



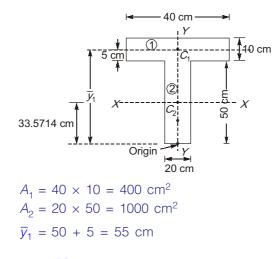


Q.55 The cross-section of a girder is shown in the figure (not to scale). The section is symmetric about a vertical axis (Y-Y). The moment of inertia of the section about the horizontal axis (X-X) passing through the centroid is _____ cm⁴. (round off to nearest integer).



(NAT)

Ans. (468810) (464000 - 472000)



 $\bar{y}_2 = \frac{50}{2} = 25 \text{ cm}$

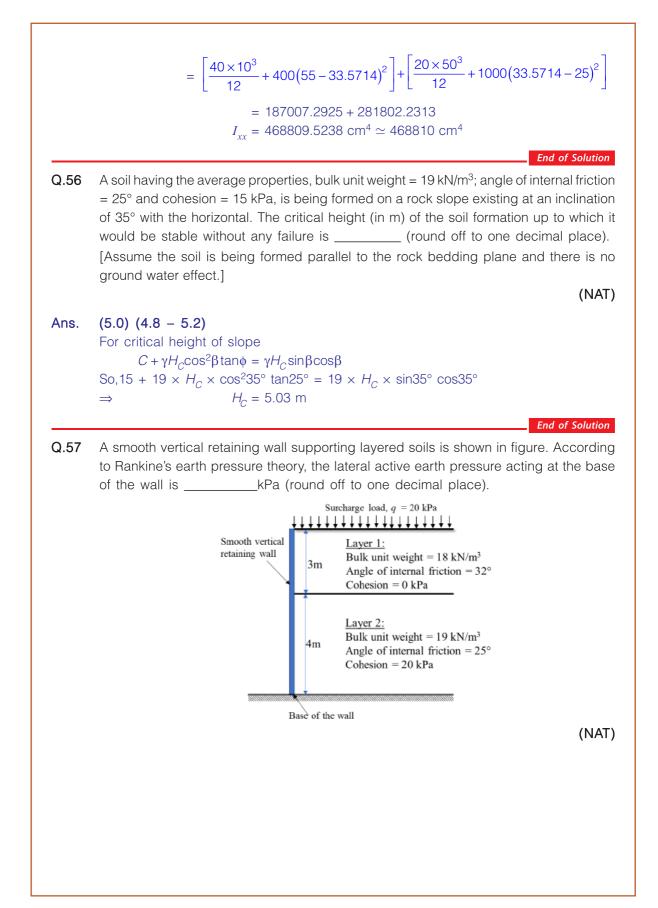
Centroid of composite shape, from bottom fibre,

$$\overline{y} = \frac{A_1 \overline{y}_1 + A_2 \overline{y}_2}{A_1 + A_2}$$

$$\overline{y} = \frac{(400 \times 55) + (1000 \times 25)}{400 + 1000}$$

$$\overline{y} = 33.5714 \text{ cm}$$

$$I_{xx} = \left[\frac{40 \times 10^3}{12} + 400(\overline{y}_1 - \overline{y})^2\right] + \left[\frac{20 \times 50^3}{12} + 1000(\overline{y} - \overline{y}_2)^2\right]$$



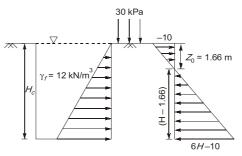
Ans. (35.4) (34.0 - 37.0)Active earth pressure at base, $\sigma = k_a (\gamma z + q) - 2C\sqrt{ka}$ $k_a = \frac{1 - \sin \phi}{1 + \sin \phi} = \frac{1 - \sin 25^\circ}{1 + \sin 25^\circ} = 0.406$ where, $q = 20 + 18 \times 3 = 74 \text{ kN/m}^2$ $\gamma z = 19 \times 4 = 76 \text{ kN/m}^2$ $C = 20 \text{ kN/m}^2$ [:: Given] $\sigma = 0.406 \times (76 + 74) - 2 \times 20 \times \sqrt{0.406}$ So, $= 35.413 \text{ kN/m}^2 \simeq 35.4 \text{ kN/m}^2$

End of Solution

Q.58 A vertical trench is excavated in a clayey soil deposit having a surcharge load of 30 kPa. A fluid of unit weight 12 kN/m³ is poured in the trench to prevent collapse as the excavation proceeds. Assume that the fluid is not seeping through the soil deposit. If the undrained cohesion of the clay deposit is 20 kPa and saturated unit weight is 18 kN/m³, what is the maximum depth of unsupported excavation (in m, rounded off to two decimal places)?

(NAT)

Ans. (3.33) (3.30 - 3.35)



Now, active pressure at depth z,

$$\sigma_z = k_a \gamma z - 2C \sqrt{k_a} - 12z + kq$$

At z = 0[:: k = 1 for $\phi = 0^{\circ}$, q = 30 kN/m²; C = 20 kN/m²] $\sigma_{z} = -2 \times C + q = 2 \times 20 + 30$ = -40 + 30 $= -10 \text{ kN/m}^2$ At z_0 , $\sigma_z = 0$ $18z_0 - 40 - 12z_0 + 30 = 0$ 6z - 10 = 0 $6z_0 - 10 = 0$ \Rightarrow $z_0 = 1.66 \text{ m}$ \Rightarrow At depth H, $\sigma_H = k_a \gamma H - 2C \sqrt{k_a} - 12H + k_a$

 $\sigma_{H} = 18H - 40 - 12H + 30$ = 6H - 10

For unsupported depth of excavation, total active thrust must be zero.

So,
$$\frac{1}{2} \times 10 \times 1.66 = \frac{1}{2} \times (H - 1.66) \times (6H - 10)$$

 $\Rightarrow \qquad H = \frac{10}{3} = 3.33 \text{ m}$

Alternatively:

So,

$$\sigma_{v} = q + \gamma z$$

= 30 + 18z
$$p_{a} = k_{a}\sigma_{v} - 2c\sqrt{k_{a}}$$

$$p_{a} = 30 + 18z - 2 \times 20 = 18z - 10$$

For critical depth, $p_{a} = 0$
 $18z_{c} - 10 = 0$
 $z_{c} = \frac{10}{18}m = 0.556 m$

For the maximum depth of unsupported excavation, the active earth pressure force at that depth should be zero.

$$P_{a} = \frac{1}{2} (18H_{c} - 10) (H_{c} - 0.56) - \frac{1}{2} 10 \times 0.56 - \frac{1}{2} \gamma_{f} H_{c}^{2}$$

$$0 = (9H_{c} - 5) (H_{c} - 0.56) - 5 \times 0.56 - 6H_{c}^{2}$$

$$0 = 3H_{c}^{2} - 10.04H_{c} + 5 \times 0.56 - 5 \times 0.56$$

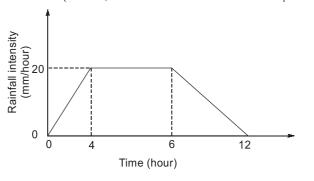
$$3H_{c}^{2} - 10.04H_{c} = 0$$

$$H_{c} = 0, 3.33 \text{ m}$$

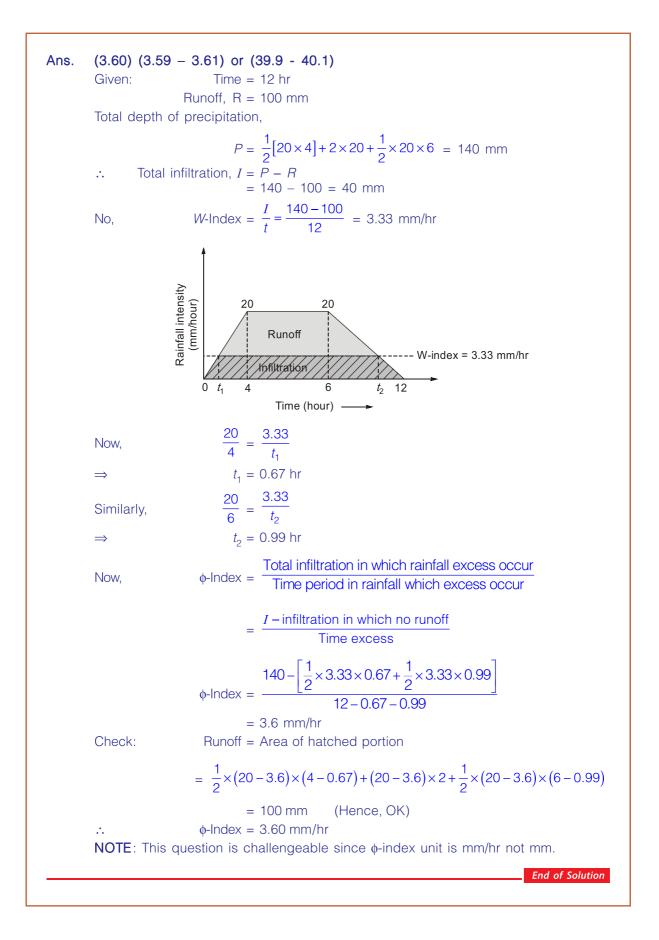
Therefore, the maximum depth of unsupported excavation is 3.33 m.

End of Solution

Q.59 A 12-hour storm occurs over a catchment and results in a direct runoff depth of 100 mm. The time-distribution of the rainfall intensity is shown in the figure (not to scale). The φ-index of the storm is (in mm, rounded off to two decimal places) _____.



(NAT)



Q.60 A hydraulic jump occurs in a 1.0 m wide horizontal, frictionless, rectangular channel, with a pre-jump depth of 0.2 m and a post-jump depth of 1.0 m. The value of g may be taken as 10 m/s². The values of the specific force at the pre-jump and post-jump sections are same and are equal to (in m³, rounded off to two decimal places) _____.

Ans. (0.62) (0.60 - 0.64)
Given,
$$y_1 = 0.2 \text{ m}, y_2 = 1 \text{ m}$$

As we know
 $\frac{2q^2}{g} = y_1 y_2 (y_1 + y_2)$
 $\Rightarrow \qquad \frac{2q^2}{10} = 0.2 \times 1(0.2 + 1)$
 $\Rightarrow \qquad q^2 = \frac{10}{2} \times 0.2 \times 1.2 = 1.2$
 $q = 1.095 \text{ m}^3/\text{s/m}$
Now, specific force $= \frac{Q^2}{Ag} + A\overline{y}$
 $= \frac{q^2 B^2}{By_1 g} + \frac{By_1 y_1}{2}$
 $= \left(\frac{1.095^2}{0.2 \times 102} + \frac{0.2^2}{2}\right) \times 1 = 0.6195 \text{ m}^3 \simeq 0.62 \text{ m}^3$
So,Specific force per unit width = 0.62 m³/m

Q.61 In Horton's equation fitted to the infiltration data for a soil, the initial infiltration capacity is 10 mm/h; final infiltration capacity is 5 mm/h; and the exponential decay constant is 0.5 /h. Assuming that the infiltration takes place at capacity rates, the total infiltration depth (in mm) from a uniform storm of duration 12 h is ______. (round off to one decimal place)

(NAT)

(NAT)

Ans. (70.0) (69.7 - 70.1)

Initial infiltration capacity, $f_0 = 10$ mm/h Final infiltration capacity, $f_c = 5$ mm/h Horton's Decay constant, $k_h = 0.5/h$

Now,

$$F_{P} = \int_{0}^{T} [f_{c} + [f_{0} - f_{c}]e^{-k_{\eta}t}]dt$$
$$= \int_{0}^{12} (5 + (10 - 5)e^{-0.5t})dt$$

$$= [5t]_{0}^{12} + \left[\frac{5e^{-0.5t}}{(-0.5)}\right]_{0}^{12}$$

= $[5 \times 12] + \left[-10e^{-0.5 \times 12} - \left[-10e^{-0.5 \times 0}\right]\right]$
= $60 + [9.975]$
= $69.97 \text{ mm} \simeq 70 \text{ mm}$

Alternatively:

For large value of 't' cumulative infiltration capacity is given by,

$$F_{P} = f_{c}t + \frac{(f_{0} - f_{c})}{k_{h}}$$
$$= (5 \times 12) + \frac{(10 - 5)}{0.5} = 70 \text{ mm}$$

End of Solution

Q.62 The composition and energy content of a representative solid waste sample are given in the table. If the moisture content of the waste is 26%, the energy content of the solid waste on dry-weight basis is MJ/kg (round off to one decimal place).

Components	% by Mass	Energy content as - discarded basis [MJ/kg]
Food waste	20	4.5
Paper	45	16
Card board	5	14
Plastic	10	32
Other	20	8.0

(NAT)

Ans. (18.4) (18 – 19)

Energy content (as discarded basis):

 $[0.2\times4.5+0.45\times16+0.05\times14+0.1\times32+0.2\times8]$ = 13.6 MJ/kg Energy content (on dry basis) for moisture content of 26%:

 $= \frac{13.6 \text{ MJ/kg} \times 100\%}{(100 - 26)\%} = 18.38 \text{MJ/kg} \simeq 18.4 \text{ MJ/kg}$

End of Solution

Q.63 A flocculator tank has a volume of 2800 m³. The temperature of water in the tank is 15°C, and the average velocity gradient maintained in the tank is 100/s. The temperature of water is reduced to 5°C, but all other operating conditions including the power input are maintained as the same. The decrease in the average velocity gradient (in %) due to the reduction in water temperature is (round off to nearest integer). [Consider dynamic viscosity of water at 15°C and 5°C as 1.139 × 10⁻³ N-s/m² and 1.518 ×10⁻³ N-s/m², respectively]

(NAT)

Ans. (13) (12 - 15)

$$G_{1} = \sqrt{\frac{P}{\mu_{1} \times V}} \qquad \dots (i)$$

$$G_{2} = \sqrt{\frac{P}{\mu_{2} \times V}} \qquad \dots (ii)$$

Divide (i) by (ii), we get

$$\frac{G_1^2}{G_2^2} = \frac{\mu_2}{\mu_1}$$

$$G_2^2 = \left[\frac{(100s^{-1})^2 \times 1.139 \times 10^{-3} \,\text{N-s/m}^2}{1.518 \times 10^{-3} \,\text{N-s/m}^2}\right]^{1/2} = 86.62 \,\text{S}^{-1}$$
% change in $G = \frac{G_1 - G_2}{G_1} \times 100 = \frac{100 - 86.62}{100} \times 100 = 13.38\%$

End of Solution

Q.64 The wastewater inflow to an activated sludge plant is 0.5 m³/s, and the plant is to be operated with a food to microorganism ratio of 0.2 mg/mg-d. The concentration of influent biodegradable organic matter of the wastewater to the plant (after primary settling) is 150 mg/L, and the mixed liquor volatile suspended solids concentration to be maintained in the plant is 2000 mg/L. Assuming that complete removal of biodegradable organic matter in the tank, the volume of aeration tank (in m³, in integer) required for the plant is _____.

(NAT)

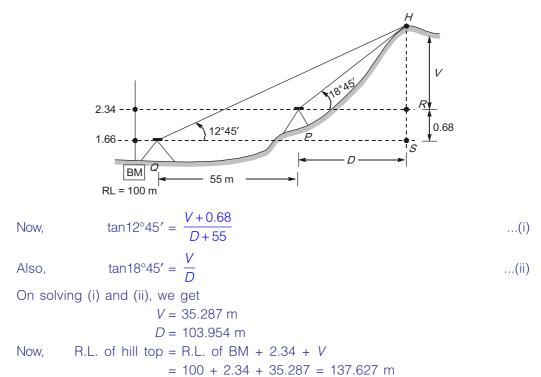
Ans. (16200) (16200 - 16200)
Given:
$$Q = 0.5 \text{ m}^3/\text{sec}$$

 $\frac{F}{M} = 0.2 \text{ mg/mg-d}$
 $S_0 = 150 \text{ mg/L}$
 $X = 2000 \text{ mg/L}$
 $K = 2000 \text{ mg/L}$
Now, $\frac{F}{M} = \frac{Q_0 S_0}{V \cdot X}$
 $0.2 d^{-1} = \frac{0.5 \frac{\text{m}^3}{\text{sec.}} \times 86400 \frac{\text{sec}}{d} \times 150 \frac{\text{mg}}{L}}{V \times 2000 \frac{\text{mg}}{L}}$
 $V = 16200 \text{ m}^3$
End of Solution

Q.65 Trigonometric levelling was carried out from two stations P and Q to find the reduced level (R. L.) of the top of hillock, as shown in the table. The distance between Stations P and Q is 55 m. Assume Stations P and Q, and the hillock are in the same vertical plane. The R. L. of the top of the hillock (in m) is ______ (round off to three decimal places).

Station	Vertical angle of top of hilllock	Staff reading on B.M	R.L of BM	
Р	18° 45′	2.340 m	100.000 m	
Q	12° 45′	1.660 m		

Ans. (137.627) (137.500 - 137.700)



End of Solution

(NAT)