

# Chapter 3

## DC-DC Converters (or) Choppers

### LEARNING OBJECTIVES

After reading this chapter, you will be able to understand:

- Principle of operation and control
- Time ratio control
- Current limit control
- Step up chopper
- Step down chopper
- Types of chopper circuits
- Second quadrant (type-B) chopper
- Voltage commutated chopper
- Current commutated chopper
- Peak commutating current
- Load commutated chopper
- Multiphase chopper

### PRINCIPLE OF OPERATION AND CONTROL

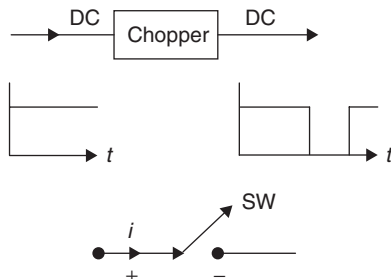
In industries, several applications need DC supply, it will be better if it is a variable DC voltage source.

- This conversion of fixed DC voltage to an adjustable DC output voltage by using semiconductor devices are called chopping examples of such DC systems are trolley buses, battery operated vehicles, subway cars, battery charging, etc.

### Principle of Chopper

Chopper is a static device that converts fixed DC input voltage to a variable DC output voltage directly.

- It is a high-speed on/off semiconductor switch (connects source to the load and disconnects the load from the source of a fast speed).
- The device used for a chopper circuit can be force commutated thyristor, power BJT, Power MOSFET, GTO or IGBT.



- It is a DC equivalent of an AC transformer.
- It can be used to step up and step down the fixed DC input voltage.
- Step-down DC chopper is most commonly used.

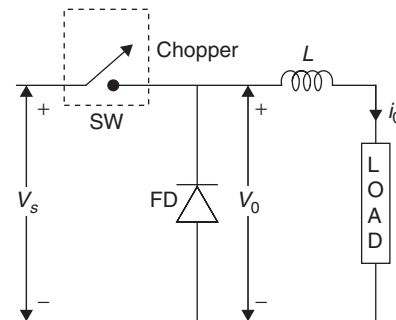
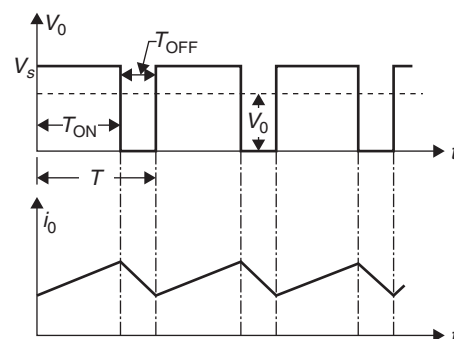


Figure 1 Basic chopper circuit



### Output voltage and current waveforms

When chopper is ON,  $T_{ON}$  load voltage is equal to source voltage  $V_s$  vs. during off period  $T_{OFF}$  load current flows through the free-wheeling diode FD. Load terminals are short-circuited by FD and  $V_0$  is zero.

The load power can be controlled by varying the ON and OFF times.

The ratio of  $T_{ON}$  to  $(T_{ON} + T_{OFF})$  is known as duty cycle.

There are three ways of obtaining the variable ON-time to OFF time for voltage control.

1.  $T_{ON}$  constant and  $T$  varying (Frequency modulation)
2.  $T$  constant and  $T_{ON}$  varying (Pulse width modulation)
3.  $T_{ON}$  and  $T$  are both varying and for all three

Average load voltage

$$V_0 = \frac{T_{ON}}{T_{ON} + T_{OFF}} \times V_s$$

$$= \left( \frac{T_{ON}}{T} \right) V_s$$

where  $T_{ON}$  = ON – time

$T_{OFF}$  = OFF – time

$T = T_{ON} + T_{OFF}$  = chopping period

and  $\alpha = \frac{T_{ON}}{T}$  = duty cycle

then  $V_0 = \alpha V_s$

$$V_0 = T_{ON} \cdot f \cdot V_s$$

$f = 1/T$  = chopping frequency

- Therefore, load voltage can be controlled by varying duty cycle  $\alpha$ .

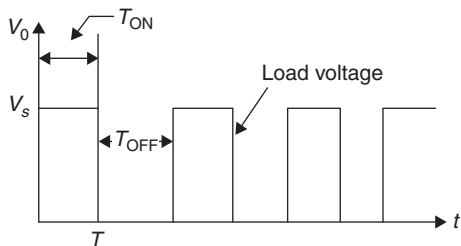
## Control Strategies

Average output voltage  $V_0$  can be varied through  $\alpha$  by opening and closing the semiconductor switch periodically. The various control strategies for varying duty cycle  $\alpha$  are as follows:

1. Time ratio control
2. Current limit control

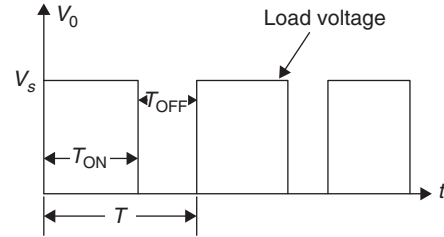
### Time Ratio Control

#### 1. Constant frequency system:



In this method,  $T_{ON}$  is varied but chopping frequency  $f(T)$  is kept constant. Also called as pulse-width modulation scheme.

#### 2. Variable frequency system



In this method, chopping frequency  $f$  is varied and either

- ON-time  $T_{ON}$  is kept constant
- OFF-time  $T_{OFF}$  is kept constant

This method is also called as frequency modulation scheme.

- Frequency modulation scheme has some disadvantages compared to pulse-width modulation scheme. Chopping frequency has to be varied over a wide range for the control of output voltage and so the design of filter is quite difficult.
- For the control of  $\alpha$ , frequency variation is wide. Due to which interference with signalling and telephone lines in frequency modulation.
- The large time  $T_{OFF}$  in frequency modulation make the load current discontinuous which is undesirable. Therefore pulse width modulation scheme is better than variable frequency scheme.
- The only limitation in PWM is  $T_{ON}$  cannot be reduced to near zero for most of the commutation circuits used in choppers. So, low range of a control is not possible in PWM.

### Current Limit Control

In this control strategy, the ON and OFF of chopper circuit is guided by the previous set value of load current. These two set values are maximum load current  $I_{max}$  and minimum load current  $I_{min}$ . When load current reaches the upper limit  $I_{max}$ , chopper is switched OFF. Now load current free wheels and begins to decay exponentially. When it falls to lower limit  $I_{min}$  chopper is switched on and load current begins to rise. So the load current fluctuates between  $I_{max}$  and  $I_{min}$ . Therefore it cannot be discontinuous. current limit control involves feedback loop, the trigger circuitry for the chopper is therefore more complex.

Chopper system offers smooth control, high efficiency, fast response and regeneration.

There are two types of choppers

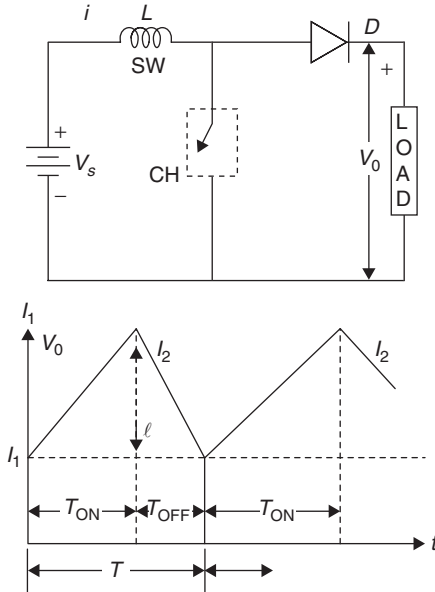
1. Step-down chopper
2. Step-up chopper

## STEP-UP CHOPPER

Average output voltage  $V_0$  is greater than input voltage.

$V_0 > V_s$  is called step-up chopper and  $V_0 < V_s$  is called step-down chopper.

### Working Principle



When the switch is ON, the current circulates in the loop and inductor stores energy.

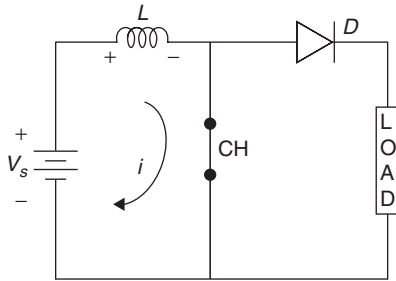
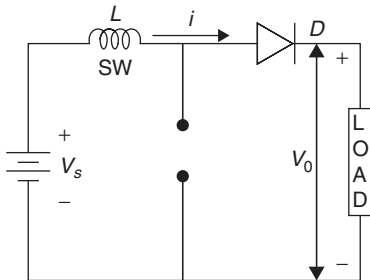


Figure 2 L' stores energy

When the switch is opened the total input voltage is now added up with  $L \frac{di}{dt}$ .



$L \frac{di}{dt}$  is added to  $V_s$

$$\therefore V_{IN} = V_s + L \frac{di}{dt}$$

Therefore, average output voltage  $V_0$  is greater than the input voltage  $V_s$ , assuming the output current is linear energy input to conductor from the source, during period  $T_{ON}$ ,  $W_{IN}$  = Avg. volt across  $L \times$  Avg. current the inductor  $\times$  time

$$W_{IN} = V_s \left[ \frac{I_1 + I_2}{2} \right] T_{ON}$$

Energy released by the inductor to the load during period  $T_{OFF}$ .

$$W_{OFF} = \text{Average voltage across} \times \text{Average Current} \times \text{Time.}$$

$$= (V_0 - V_s) \left( \frac{I_1 + I_2}{2} \right) \times T_{OFF}$$

For a lossless system

$$V_s \left[ \frac{I_1 + I_2}{2} \right] T_{ON} = (V_0 - V_s) \left[ \frac{I_1 + I_2}{2} \right] T_{OFF}$$

$$V_0 = V_s \left[ \frac{T}{T - T_{ON}} \right]$$

$$T = T_{ON} + T_{OFF}$$

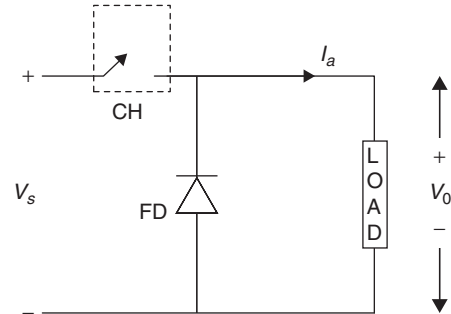
$$V_0 = \frac{V_s}{1 - \alpha}$$

$$\alpha = T_{ON} / T$$

where

From the above equation the average voltage across the load can be stepped up by varying the duty cycle.

### STEP-DOWN CHOPPER



If  $V_0 < V_s$ , it is called step-down chopper

$$V_0 = V_s \times \left( \frac{T_{ON}}{T} \right) = V_s \times f \times T_{ON}$$

$$V_0 = \alpha V_s$$

$\alpha$ -duty cycle of chopper. The average output voltage is less than the input voltage.

$$\text{RMS output voltage, } V_{RMS} = \left[ \frac{1}{T} \int_0^{T_{ON}} V_s^2 dt \right]^{1/2}$$

$$V_{RMS} = \sqrt{\alpha} V_s$$

### Effective Source Resistance ( $R_{eff}$ )

$$R_{eff} = \frac{(V_s)_{avg}}{(I_s)_{avg}} = \frac{V_s}{\alpha \cdot \frac{V_s}{R}} = \frac{R}{(\alpha)}$$

It can be used in static rotor resistance control of an induction motor.

### Solved Examples

**Example 1:** If  $V_{OUT}$  and  $V_{IN}$  are the magnitudes of output voltage and DC input voltages, respectively, for a step-down chopper. If the chopper is operated in a steady state with a constant duty ratio  $\alpha$  and continuous conduction mode, then the ratio  $\frac{V_{OUT}}{V_{IN}}$  is given by

- (A)  $\left(\frac{\alpha}{1-\alpha}\right)$  (B)  $\left(\frac{1}{1-\alpha}\right)$  (C)  $\alpha$  (D)  $\left(\frac{\alpha-1}{\alpha}\right)$

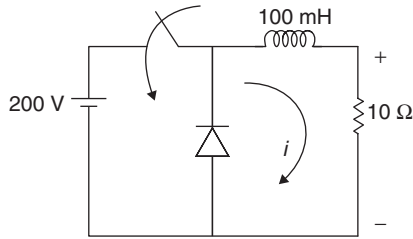
**Solution:** (C)

For a step-down chopper

$$V_{OUT} = \alpha V_{IN} \quad \frac{V_{OUT}}{V_{IN}} = \alpha$$

**Example 2:** The peak-to-peak ripple in load current in a step-down chopper (as shown below) switched at 2 kHz with a duty ratio of 0.75 is close to

- (A) 0.125 A (B) 0.25 A (C) 0.5 A (D) 1 A



**Solution:** (B)

Maximum ripple current

$$\Delta I_{\max} = \frac{V_s}{4fL} = \frac{200}{4 \times 2000 \times 0.1} = 0.25 \text{ A}$$

**Example 3:** If the desired output voltage of a step DC–DC chopper with an input DC voltage of 230 V is 280 V. The conducting time for the thyristor chopper operating at a  $T_{OFF}$  of 50  $\mu\text{s}$  would be

- (A) 33.33  $\mu\text{s}$  (B) 66.66  $\mu\text{s}$   
(C) 50  $\mu\text{s}$  (D) 100  $\mu\text{s}$

**Solution:** (A)

$$V_0 = \frac{V_s}{1-\alpha}$$

$$380 = 230 \left( \frac{1}{1-\alpha} \right)$$

$$(1-\alpha) = 0.6$$

$$\alpha = 0.4 = \frac{T_{ON}}{T_{ON} + T_{OFF}}$$

$$1 + \frac{T_{OFF}}{T_{ON}} = \frac{1}{0.6} = 2.5$$

$$T_{ON} = \frac{50}{(2.5 - 1)} = 33.33 \mu\text{s}$$

**Example 4:** The duty cycle of a boost regulator which has an input voltage of 4 V and an average output voltage of 8 V is

- (A) 1/2 (B) 3/2 (C) 2/3 (D) 5/2

**Solution:** (A)

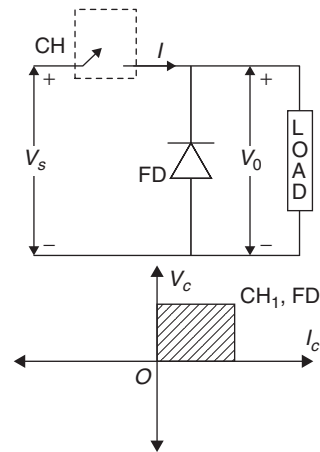
For a boost regulator

$$V_0 = \frac{V_s}{1-\alpha} \Rightarrow 1-\alpha = \frac{4}{8} = \frac{1}{2}$$

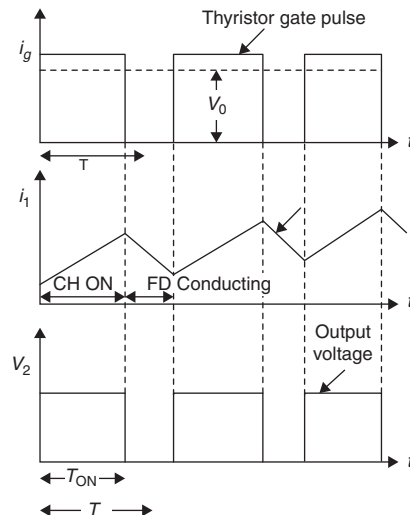
$$\alpha = (1 - 1/2) = (1/2)$$

### TYPES OF CHOPPER CIRCUITS

#### First-quadrant (Type-A) Chopper

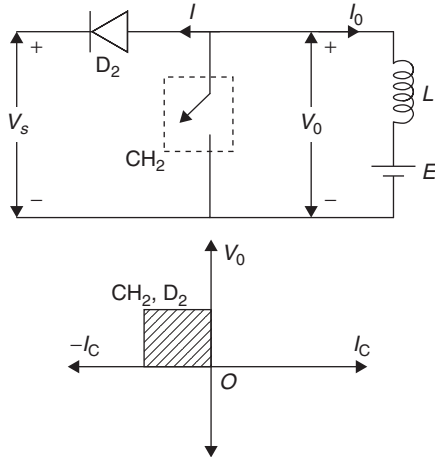


- When chopper  $CH_1$  is ON,  $V_0 = V_s$  and current  $i_0$  flows in the direction as shown.
- When  $CH_1$  is OFF  $V_0 = 0$  but  $i_0$  in the load continues flowing in the same direction through FD (free-wheeling diode).
- Hence average values of both load voltages and currents, i.e.  $V_0$  and  $I_0$  are always positive as shown by the shaded area in the I quadrant.
- The average output voltage  $V_0$  is always less than input DC voltage  $V_s$  and hence it is also known as step-down chopper.
- The power flow in Type-A chopper is always from source to load.

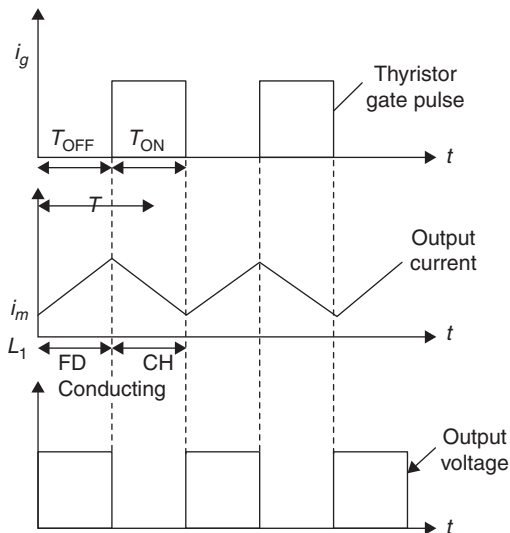


It is a step-down chopper in which the average value of output voltage and current is always positive. A free-wheeling diode is connected across the load to prevent the output current being negative. Its region of operation is in the first quadrant only, so it is also called first-quadrant chopper.

### Second-quadrant (Type-B) Chopper

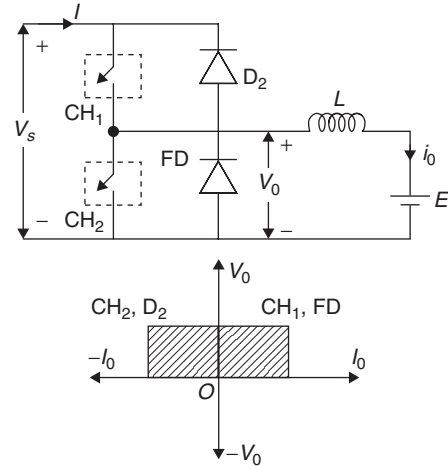


- When  $CH_2$  is ON,  $V_0 = 0$  but load voltage  $E$  drives current through  $L$  and  $CH_2$ . Inductance stores energy during  $T_{ON}$  of  $CH_2$ .
- When  $CH_2$  is OFF  $V_0 = \left(E + L \frac{di}{dt}\right)$  exceeds source voltage  $V_s$ ; then  $D_2$  becomes forward biased and begins conduction thus allowing power to flow to the source.
- $CH_2$  may be ON or OFF, current  $i_0$  flows out of the load, current  $i_0$  is therefore treated as negative. Since  $V_0$  is always positive and  $i_0$  is negative, power flow is always from load to source.
- As load voltage  $V_0 = \left(E + L \frac{di}{dt}\right)$  is more than source voltage  $V_s$ , type-B chopper is also called step-up chopper.

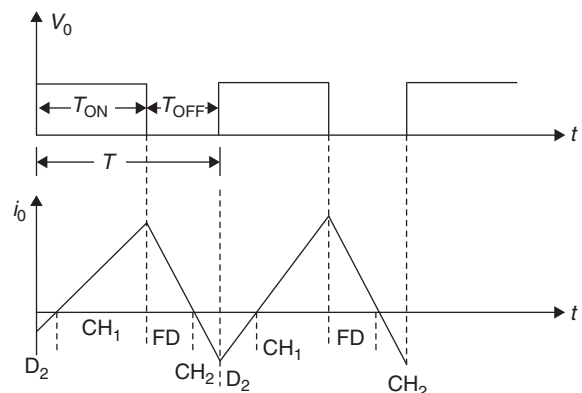


In this type the average output voltage is positive but the average output current is negative. Therefore the class B chopper operates in the second quadrant. Power flows from the load to the source. It is a step-up chopper. It is widely used for regenerative braking of DC Motor.

### Two-quadrant Type-A (Type-C) Chopper



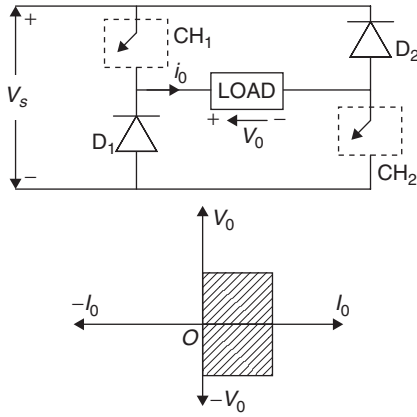
- This chopper is obtained by connecting type-A and type-B choppers in parallel.
- $V_0$  is always positive due to the presence of FD across the load.
- When  $CH_2$  is ON (or) FD conducts  $V_0 = 0$ , and in case  $CH_1$  is ON or diode  $D_2$  conducts and  $V_0 = V_s$ .
- Load current  $i_0$  can however reverse its direction.  $i_0$  is positive when  $CH_1$  is ON and FD conducts.  $i_0$  is negative when  $CH_2$  is ON or  $D_2$  conducts.
- $CH_1$  and FD operate together as type-A chopper in the I quadrant  $CH_2$  and  $D_2$  operate together as type-B in the second quadrant.
- Average load voltage is always positive but average load current may be positive or negative. Hence the power flow may be from source to load (I quadrant operation) or from load to source (II quadrant operation).
- Choppers  $CH_1$  and  $CH_2$  should not be ON at the same time as this would lead to a direct short circuit of supply lines.
- Such choppers are used for motoring and regenerative braking of DC motors.



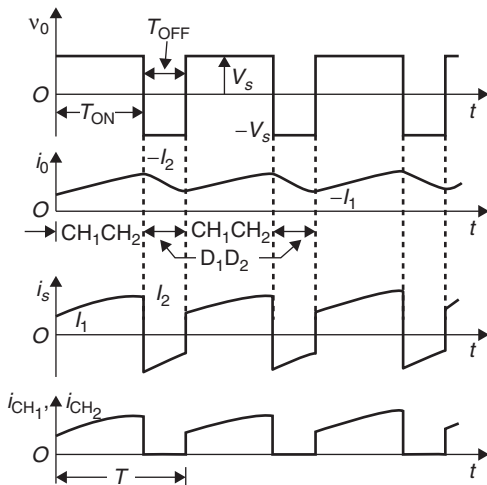
Class C chopper is a combination of class A and class B choppers. For first-quadrant operation,  $CH_1$  is ON or  $D_1$  conducts. For second quadrant,  $CH_2$  is ON or  $D_1$  conducts. When  $CH_1$  is ON, the load current is positive. The output voltage is equal to ' $V$ ' and the load receives power from the source.

When  $CH_1$  is turned OFF, energy stored in inductance,  $L$  forces current to flow through the diode  $D_2$  and the output voltage in zero. Current continues to flow in positive direction.  $\Rightarrow$  When  $CH_2$  is triggered, the voltage  $E$  forces current to flow in opposite direction through  $L$  and  $CH_2$ . The output voltage is zero turning OFF  $CH_2$ , the energy stored in the inductance drives current through diode  $D_1$  and the supply output voltage is  $V_1$  the input current becomes negative and power flows from load to source.

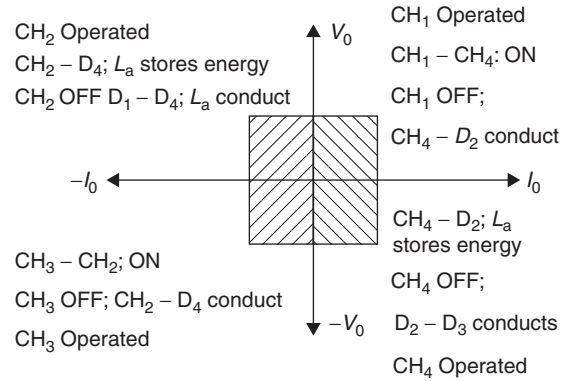
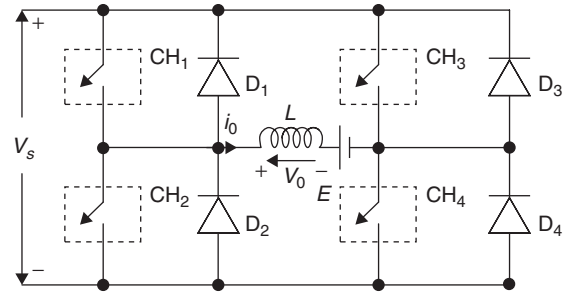
### Two-quadrant Type-B (Type-D) Chopper



- Type-D chopper is obtained by connecting Type-A and Type-B chopper in differential mode, i.e., load is connected in between them.
- When both  $CH_1$  and  $CH_2$  are ON  $V_0 = V_s$ .
- When both choppers are off  $D_1$  and  $D_2$  conducts  $V_0 = -V_s$ .
- Average output voltage  $V_0$  is positive when their  $T_{ON} < T_{OFF}$  and  $V_0$  is negative when their  $T_{ON} > T_{OFF}$ .
- The direction of load current is always positive because choppers and diodes can conduct current only in the direction of arrows. As  $V_0$  is reversible, power flow is reversible.



### Four-quadrant Type-E Chopper



#### First Quadrant

- $CH_4$  is kept ON,  $CH_3$  is kept OFF and  $CH_1$  is operated. With  $CH_1, CH_4$  ON  $V_0 = V_s$  and  $i_0$  begins to flow. Here both  $V_0$  and  $i_0$  are positive resulting first quadrant operation. When  $CH_1$  is turned OFF positive current freewheels through  $CH_4$  and  $D_2$ .

#### Second Quadrant

- $CH_2$  is operated and  $CH_1, CH_3, CH_4$  are kept OFF. With  $CH_2$  ON, reverse (negative) current flows through  $L, CH_2, D$  and  $E$ . Inductance  $L$  stores energy during the time  $CH_2$  is ON. When  $CH_2$  is turned OFF, current is fed back to source through diodes  $D_1, D_4$ . Here,  $E + L \frac{di}{dt}$  is more than the source voltage  $V_s$ .
- As  $V_0$  is positive and  $I_0$  is negative, it is second-quadrant operation of chopper.
- Power is fed back from load to source.

#### Third Quadrant

$CH_1$  is kept off,  $CH_2$  is kept ON and  $CH_3$  is operated. Polarity of load emf  $E$  must be reversed for this quadrant working when  $CH_3$  ON, load gets connected to  $V_s$  so that both  $V_0$  and  $I_0$  are negative leading to third-quadrant operation.

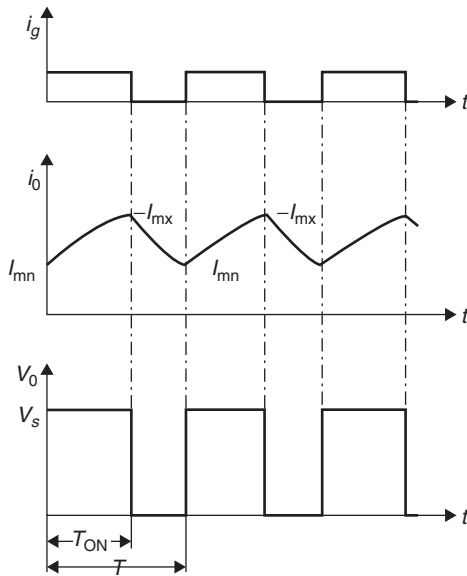
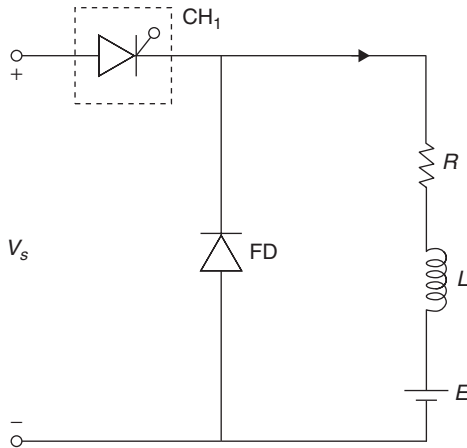
- When  $CH_3$  is turned off, negative current freewheels through  $CH_2, D_4$ . In this manner,  $V_0$  and  $i_0$  can be controlled in the third quadrant.
- Here, the chopper operates as step-down chopper.

### Fourth Quadrant

CH<sub>4</sub> is operated and other devices are kept OFF. Load emf  $E$  must have its polarity reversed, for operation in IV Quadrant. With CH<sub>4</sub> ON positive current flows through CH<sub>4</sub>, D<sub>2</sub>,  $L$  and  $E$ .

- $L$  stores energy during the time CH<sub>4</sub> is ON. When CH<sub>4</sub> is turned OFF current is fed back to the source through diodes D<sub>2</sub>, D<sub>3</sub>. Here, load voltage is negative, but load current is positive leading to the chopper operation in IV quadrant.
- Power is fed back from load to source. Chopper here operates as step-up chopper.

### Steady-state Analysis of Type-A Chopper



For type A-chopper with RLE load, for  $0 < t < T_{ON}$

$$V_s = Ri + \frac{Ldi}{dt} + E$$

$$V_0 = V_s$$

$$RI(s) + L[SI(s) - I_{mn}] = \frac{V_s - E}{s}$$

$$I(s) + \frac{V_s - E}{R} \left[ \frac{1}{s} - \frac{1}{(s + R/L)} \right] + \frac{I_{mn}}{s + (R/L)}$$

$$I(t) = \frac{V_s - E}{R} \left[ 1 - e^{-(R/L)t} \right] + I_{mn} e^{-R/Lt}$$

$$I(t) = \left[ \frac{V_s - E}{R} \right] \left[ 1 - e^{-(R/L)t} \right] + I_{mn} e^{-R/Lt}$$

When  $t = T_{ON}$ , then  $i(t) = I_{mx}$

$$t = T; i(t) = I_{mn}$$

Let  $\frac{L}{R} = T_a$  (Time constant)

$$I_{mx} = \frac{V_s}{R} \left[ \frac{1 - e^{-T_{ON}/T_a}}{1 - e^{-T/T_a}} \right] - \frac{E}{R}$$

$$I_{mn} = \frac{V_s}{R} \left[ \frac{e^{T_{ON}/T_a} - 1}{e^{T/T_a} - 1} \right] - \frac{E}{R}$$

Steady-state ripple current

$$\Delta I = I_{mx} - I_{mn}$$

$$\Delta I = \frac{V_s}{R} \left[ \frac{(1 - e^{T_{ON}/T_a})(1 - e^{-(T - T_{ON})/T_a})}{1 - e^{-T/T_a}} \right]$$

$\Rightarrow$  The ripple current given by the equation is independent of load converter emf  $E$  with  $T_{ON} = \alpha T$  and  $(T - T_{ON}) = (1 - \alpha)T$  and duty cycle  $\delta = \frac{T_{ON}}{T}$ .

$$\Delta I = \frac{V_s}{R} \left[ \frac{(1 - e^{\delta x})(1 - e^{-(1-\delta)x})}{1 - e^{-x}} \right]$$

For maximum value of ripple current,

$$\delta = 0.5 = 1/2$$

From which we can get

$$\Delta I_{max} = \frac{V_s}{4fL} \text{ at } \alpha = 0.5$$

### Fourier Analysis of Output Voltage

$$V_0 = V_0 + \sum_{n=1}^{\infty} V_n$$

where  $V_n$  = value of  $n^{\text{th}}$  harmonic voltage

$$= \frac{2V_s}{n\pi} \sin(n\pi\alpha) \sin(n\omega t + \theta_n)$$

$$V_0 = \alpha V_s; \alpha = T_{ON}/T$$

$$\theta_n = \tan^{-1} \left[ \frac{\sin(2\pi n\alpha)}{1 - \cos(2\pi n\alpha)} \right]$$



$$\text{Ripple Factor} = \frac{\text{AC ripple voltage}}{\text{DC voltage}}$$

$$\begin{aligned} \text{R.F.} &= \sqrt{\frac{\alpha V_s^2 - \alpha^2 V_s^2}{\alpha V_s^2}} \\ &= \frac{V_s \times \sqrt{\alpha - \alpha^2}}{\alpha V_s} \end{aligned}$$

$$\text{R.F.} = \sqrt{(1/\alpha) - 1}$$

RMS value of output voltage

$$\begin{aligned} &= \sqrt{\frac{1}{T} \int_0^{T_{\text{ON}}} V_s^2 dt} \\ &= \sqrt{1/T V_s^2 \cdot T_{\text{ON}}} \end{aligned}$$

$$(V_0)_{\text{RMS}} = \sqrt{\alpha} V_s$$

**Example 5:** The duty ratio of a chopper, operating at a fixed frequency and feeding an RL load is increases from 0.3 to 0.7. The ripple in the load current

- (A) Increases with duty ratio
- (B) Does not change
- (C) Would decrease, reach minimum at 50% duty ratio and then increase
- (D) Would increase, reach maximum at 50% ratio and then decrease

**Solution:** (D)

**Example 6:** A transistor chopper operates at 0.5 duty cycle and at a frequency of 2 kHz. The chopper is supplied from a fixed voltage DC source and feeds a fixed RL load and a freewheeling diode. If it is desired to reduce the ripple content of load current, without changing the value of average DC current through the load. The chopper should be operated

- (A) With constant duty cycle and increased frequency
- (B) By decreasing only duty cycle
- (C) By increasing the value of frequency and duty cycle  $\alpha$  in equal proportion
- (D) By decreasing only chopper frequency

**Solution:** (A)

Average DC current through the load  $I_0 = \frac{V_0}{R}$  and  $V_0 = \alpha V_s$ . If  $\alpha$  changes, average value of  $I_0$  changes which has to be kept constant.

Hence,  $\alpha$  has to be constant.

$$\text{Ripple } \Delta I = \frac{V_s}{4fL}$$

Ripple can be reduced by increasing the chopper frequency that is constant average DC load current and reduced ripple content can be obtained by constant  $\alpha$  and increasing chopper frequency.

**Example 7:** A DC motor armature with a back emf  $E$ , is fed from a step-down chopper which is connected to supply of  $V$ . When the average output DC current of the chopper was observed in a CRO the following were noted in every chopping cycle.

- (A) The current increases for the time  $t_1$ .
- (B) The current falls to zero over  $t_2$ .
- (C) The current remains zero for time  $t_3$ .
- (D) The average DC voltage across the freewheeling diode is

$$(A) \frac{V_s t_r}{(t_r + t_f + t_0)}$$

$$(B) \frac{V_s t_r + E_b t_f}{(t_r + t_f + t_0)}$$

$$(C) \frac{V_s t_r + E_b t_0}{(t_r + t_f + t_0)}$$

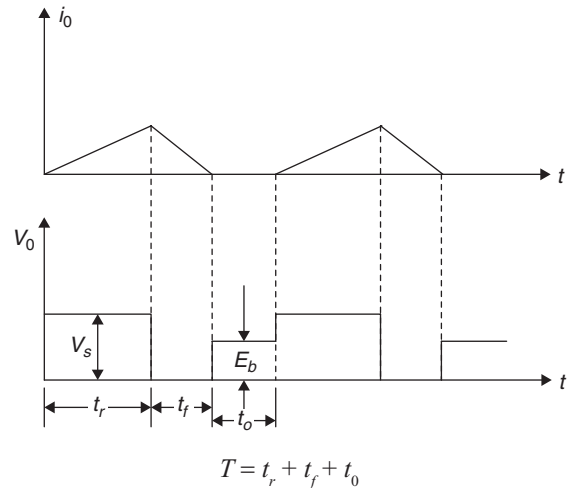
$$(D) \frac{V_s t_r + E_b (t_f + t_0)}{(t_r + t_f + t_0)}$$

**Solution:** (C)

For step-down chopper for  $R_L$  load

$$V_t = V_0 = \alpha V_s = \frac{T_{\text{ON}}}{T} V_s$$

For RLE load, the output waveform is



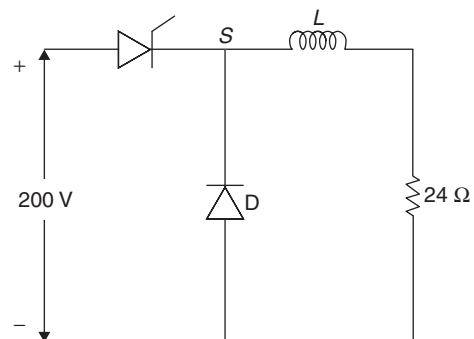
The terminal voltage

Exist only for the periods  $t_r$  and  $t_0$  remaining time zero

$\therefore$  The average voltage

$$= \frac{V_s t_r + E_b t_0}{t}$$

**Example 8:** A chopper connected to a supply of 200 V DC input feeding an RL load is shown below.





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The duty cycle of the main switch is 0.6 and the load inductance is sufficient enough to maintain a constant, ripple-free load current. The average steady-state diode current would be

- (A) 1.6 A (B) 2 A (C) 2.6 A (D) 8 A

**Solution:** (B)

During chopper operation switch (s) conducts during  $T_{ON}$  and diode D conducts during  $T_{OFF}$ . Average diode current

$$I_D = I_D \times \frac{T_{OFF}}{T} = I_0 \times \frac{(1-\alpha)T}{T}$$

$$I_D = I_D(1 - \alpha)$$

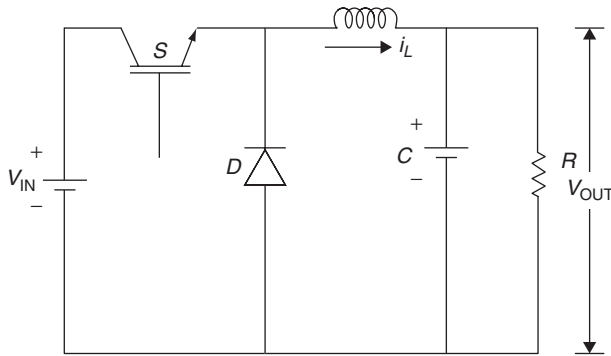
$$I_0 = \frac{V_0}{R}$$

$$V_0 = \alpha V_s = 0.6 \times 200 = 120 \text{ V}$$

$$I_0 = \frac{120}{24} = 5 \text{ A}$$

$$I_D = 5 \times (1 - 0.6) = 2 \text{ A}$$

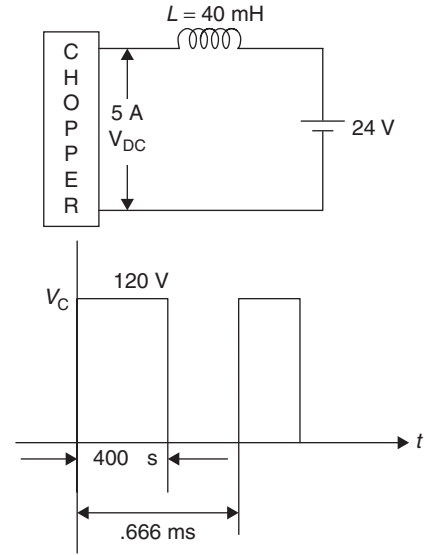
**Example 9:** The chopper shown below is operated with a constant input source voltage  $V_{IN}$  and ripple free output voltage  $V_{OUT}$ . The value of duty ratio D at the boundary of continuous and discontinuous conduction of the inductor current  $I_L$  would be (assume that the switch S is operated with a switching time period T)



- (A)  $D = 2L/RT$   
 (B)  $D = RT/L$   
 (C)  $D = 1 - \frac{V_s}{V_o}$   
 (D)  $D = 1 - 2L/RT$

**Solution:** (D)

**Example 10:** A battery charger employs a DC-DC which is operating at a duty ratio of 0.6 and supplying a charging current of 7.5 A is shown in Fig I. The chopper output voltage is as seen in Fig II. The peak-to-peak ripple current in the charging current is



- (A) 0.48 A (B) 1.2 A (C) 1 A (D) 2.4 A

**Solution:** (C)

$$T_{ON} = 400 \mu s \quad T = 0.666 \text{ ms}$$

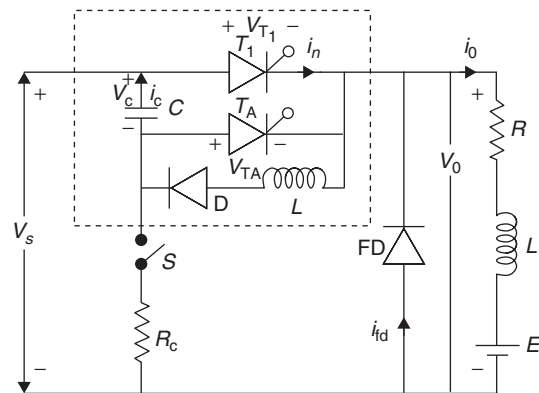
Charging current peak to peak

$$I_P = \left[ \frac{V - E}{L} \right] T_{ON} = \left[ \frac{120 - 24}{40 \times 10^{-3}} \right] \times 400 \times 10^{-6} = 0.96 \text{ A} \approx 1 \text{ A}$$

### Thyristor Chopper Circuits

The process of turning off a conducting thyristor is called commutation. In a DC chopper, it is essential to provide a separate commutation circuitry to commutate the main power SCR.

### VOLTAGE COMMUTATED CHOPPER



### Operating Modes

Chopper operation is divided into 4 modes.

**Mode 1:** For  $0 < t < t_1$

$T_1$  and  $D_1$  are ON  $T_2$  and FD are kept OFF. The output voltage  $V_0 = V_s$  and simultaneously the capacitor gets charged to a voltage  $V_c = V_s$ .

The direction of output current remains the same.

**Mode 2:** For  $t_1 \leq t \leq t_2$

Only  $T_1$  is kept ON and all other devices are turned OFF.

- The source voltage  $V_s$  appears across the output and  $i_0$  flows through  $T_1$  and then to the load.

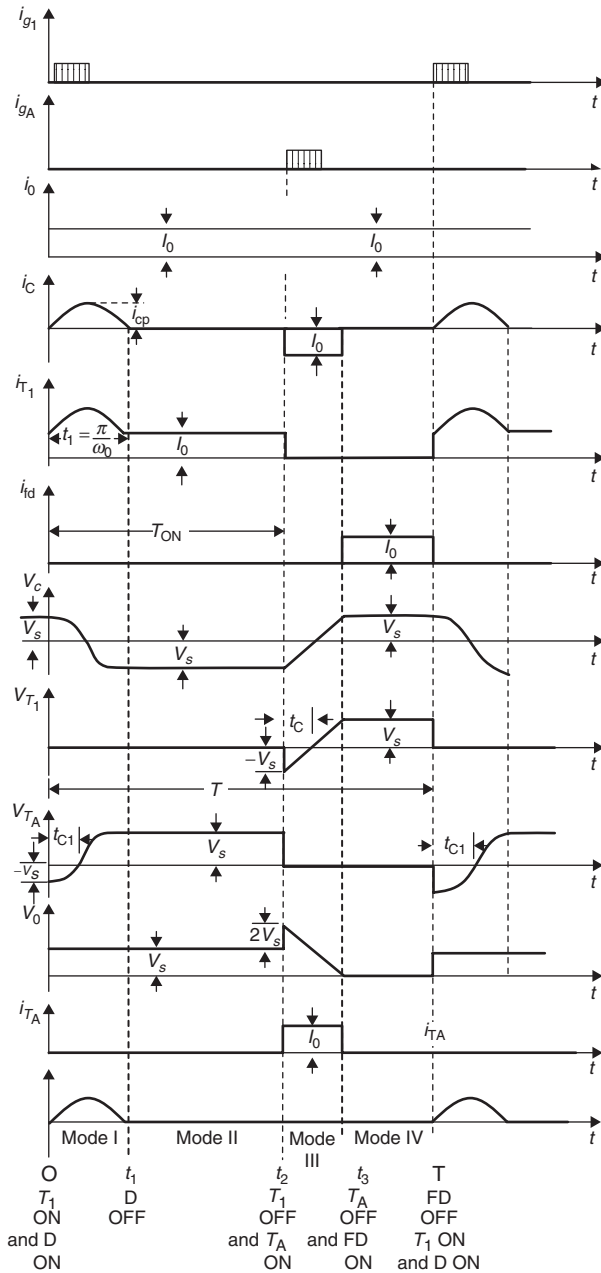
**Mode 3:** For  $t_2 \leq t \leq t_3$

- Now  $T_A$  is operated and all other devices are turned off.
- Now  $V_s$  is in series with  $V_c$ ; hence the total input voltage is  $(V_s + V_c)$ , which appears across load.  $V_0 = V_s + V_c$ .
- Load current  $i_0$  flows through  $T_2$  and then flows through load.

**Mode 4:** For  $t_3 \leq t \leq T$

The capacitor is now fully discharged and all other devices except FD are switched OFF.

- Though there is no current flow from source to load since  $V_0 = i_0$  in the load continues flowing in the same direction through free-wheeling diode.



For a constant load current  $I_0$  commutating capacitor

$$C = \frac{t_c I_0}{V_s}$$

$T_c$  = Commutation circuit turn off time  $t_c$  must be greater than  $t_q$ .

$T_q$  = S.C.R. turn off time

$$T_c = t_q + \Delta t$$

$$C = \frac{(t_q + \Delta t) I_0}{V_s}$$

$$\text{Commutating inductor } L \geq \left( \frac{V_s}{I_0} \right)^2 C$$

$$\text{Turn-off time } t_{c1} = \frac{t_1}{2\omega_0} = \frac{\pi\sqrt{LC}}{2}$$

$$\omega_0 = \frac{1}{\sqrt{LC}}$$

$$L = \left( \frac{2t_{c1}}{\pi} \right)^2 \cdot \frac{1}{C}$$

Peak current through  $T_1$  is

$$I_{T1P} = I_0 + V_s \sqrt{\frac{C}{L}}$$

Peak diode current  $I_{DP} = V_s \sqrt{\frac{C}{L}}$  = Peak capacitor current.

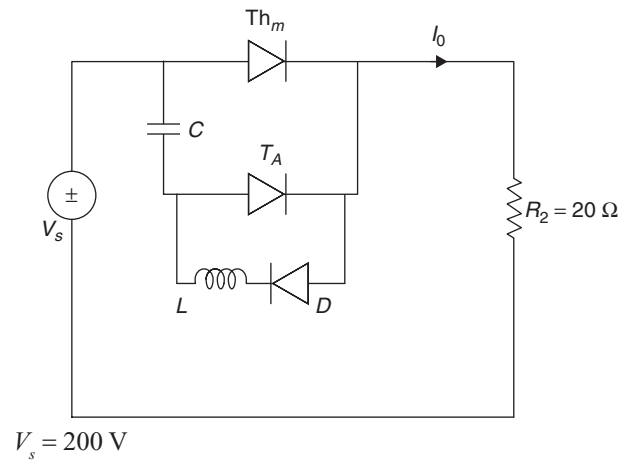
$$\text{Effective on period } T'_{ON} = T_{ON} + \frac{2V_s}{I_0} C$$

Commutating capacitor

$$I_0 = C \frac{(V_s - (-V_s))}{2t_c}$$

$$C = \frac{I_0 t_c}{V_s}$$

**Example 11:** For the current shown below if the circuit turn off time and peak value of capacitor current are 55  $\mu$ s and 15 A, respectively. Then the values of 'L' and 'C', respectively, are



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- (A) 1.2 mH, 24  $\mu$ F      (B) 2.4 mH, 44  $\mu$ F  
(C) 1.1 mH, 24  $\mu$ F      (D) 1.1 mH, 2.75  $\mu$ F

**Solution:** (D)

$$i_0 = \frac{V_s}{R} = \frac{200}{20} = 10 \text{ A}$$

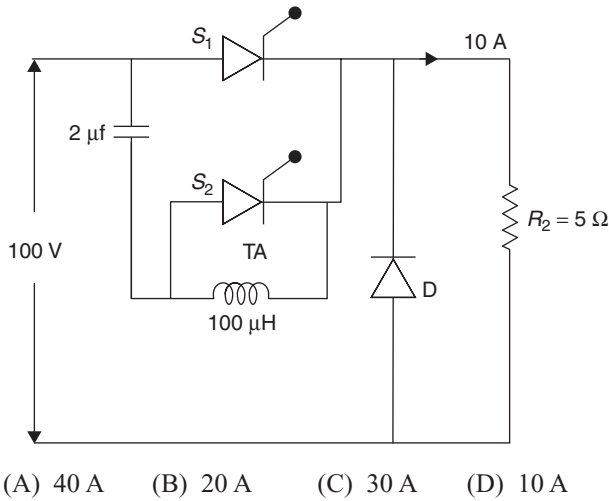
$$(t_c)_{\text{OFF}} = \frac{C V_s}{I_0} \quad C = \frac{(t_c)_{\text{OFF}} \times I_0}{V_s}$$

$$C = \frac{55 \times 10^{-6} \times 10}{200} = 2.75 \mu\text{F}$$

$$L = \left[ \frac{V_s}{I_0} \right]^2 \times C = \left[ \frac{200}{10} \right]^2 \times 2.75 \times 10^{-6}$$

$$L = 1.1 \text{ mH}$$

**Example 12:** The figure shown below is that of a chopper with  $S_M$  being the main switch rated for 200 V, 30 A and  $S_S$  being the auxiliary commutation device rated for 200 V, 20 A. The main device operates at a duty ratio of 75% and the load current is 10 A. The peak current through  $S_M$  is



**Solution:** (B)

When  $S_M$  is triggered  $L$ ,  $C$  and  $S_M$  forms a tank circuit. The current through circuit is given by

$$I_C = \frac{V_s}{\omega_0 L} \sin \omega_0 t \quad \left[ \text{where } \omega_0 = \frac{11}{\sqrt{LC}} \right]$$

Peak capacitor current

$$(I_C)_p = \frac{V_s}{\omega_0 L} = V_s \times \sqrt{\frac{C}{L}}$$

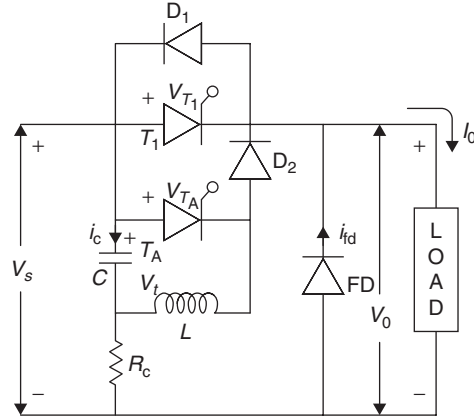
Peak current through  $S_1$  is

$$I = (I_C)_p + I_0$$

$$= V_s \sqrt{\frac{C}{L}} + I_0 = 100 \times \sqrt{\frac{1 \times 10^{-6}}{100 \times 10^{-6}}} + 10$$

$$= 100 \times (0.1) + 10 = 20 \text{ A}$$

## CURRENT COMMUTATED CHOPPER



### Operating Modes

The chopper operates in five modes

**Mode 1:** For  $t_1 < t < t_2$

- Initially devices  $T_1$ ,  $T_A$  are switched ON and  $D_1$ ,  $D_2$ , F.D. are turned OFF.
- This charge the capacitor  $V_c = V_s$  (through  $T_A$ ) and simultaneously source voltage appears across the load (through  $T_1$ ) and current  $I_0$  flows. When capacitor is fully charged  $T_A$  is turned off.

**Mode 2:** For  $t_2 < t < t_3$

- When capacitor is fully charged  $D_2$  is forward biased and is conducting. This circulates a current in the loop formed by  $C$ - $L$ - $D_1$ - $T_1$  and the current through  $T_1$  opposes the flow of load current.

$$I_{T1} = I_0 - i_c$$

**Mode 3:** For  $t_3 < t < t_4$

$D_1$  and  $D_2$  are forward-biased and starts conducting.  $T_1$  is turned OFF and  $T_A$  remains OFF as before.

- The source current splits up into diode  $D_1$  and capacitor where

$$I_{D1} = I_0 - I_c$$

- After this mode capacitor voltage is fully discharged and  $D_1$  is turned off.

**Mode 4:** For  $t_4 < t < t_5$

- During this mode,  $D_1$ ,  $T_1$ ,  $T_A$  and FD are turned OFF.
- The supply current flows through capacitor, charges the capacitor, and then reaches the load through  $D_2$ .
- Load current  $I_0 = I$ .

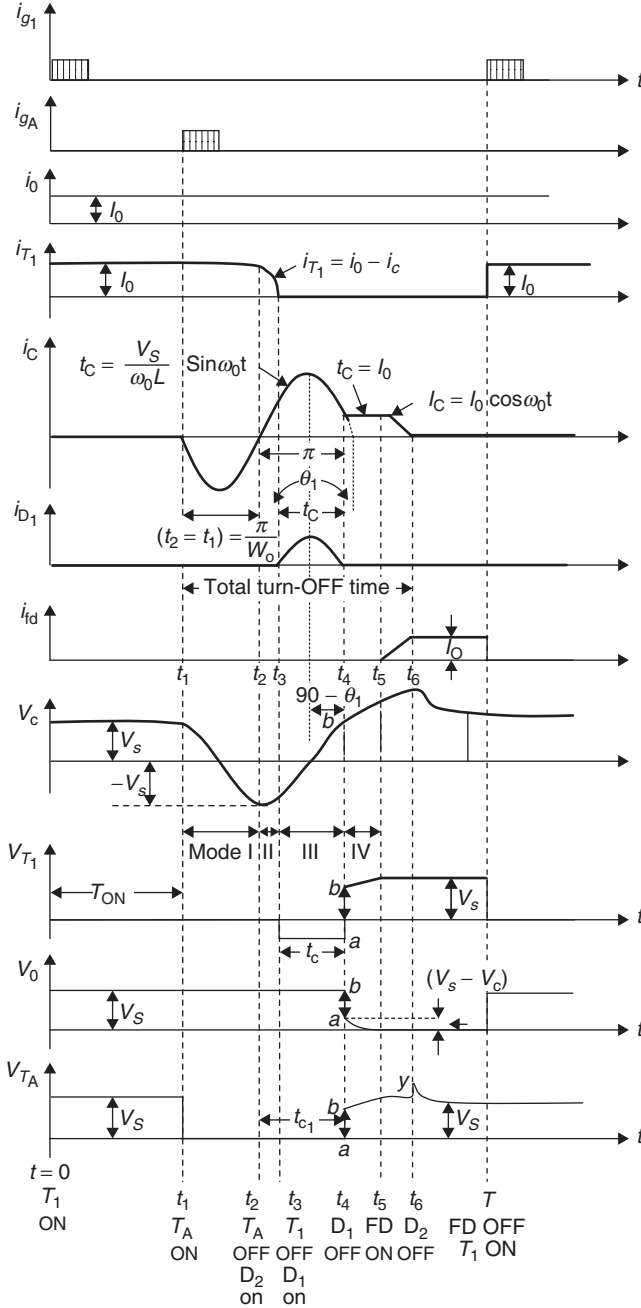
**Mode 5:** For  $t_4 < t < t_6$

Once the capacitor is fully charged while mode 4 FD starts conducting and the load current keeps circulating in the same direction.

- $D_2$  and FD are the only conducting devices.
- The output current flowing through the load  $I_0 = i_c + i_{fd}$ .
- At  $t_6$ ,  $D_2$  is turned off as well and the load current circulates in the loop FD-LOAD.

**Note:**

1. In all modes of operations, the output voltage always remains positive.
2. The direction of current will always be from source to load and it is never fed back.


**Peak Commutating Current ( $I_{cp}$ )**

$$I_{cp} = V_s \sqrt{\frac{C}{L}} > I_0$$

$$I_{cp} = V_s \sqrt{\frac{C}{L}} = XI_0$$

where  $x = \frac{I_{cp}}{I_0}$  is greater than 1.

**Circuit Turn-off time**

$$t_c = \frac{1}{\omega_0} \left[ \pi - 2 \sin^{-1} \left[ \frac{I_0}{I_{cp}} \right] \right]$$

**Commutating Inductor**

$$L = \frac{V_s t_c}{XI_0 \left[ \pi - 2 \sin^{-1} (1/x) \right]}$$

**Commutating Capacitor**

$$C = \frac{X I_0 t_c}{V_s \left[ \pi - 2 \sin^{-1} (1/x) \right]}$$

**Turn-off Times**

For main SCR,  $t_4 - t_3 = t_c = \left[ \pi - 2 \sin^{-1} \left( \frac{1}{x} \right) \right] \cdot \sqrt{LC}$

For auxiliary SCR

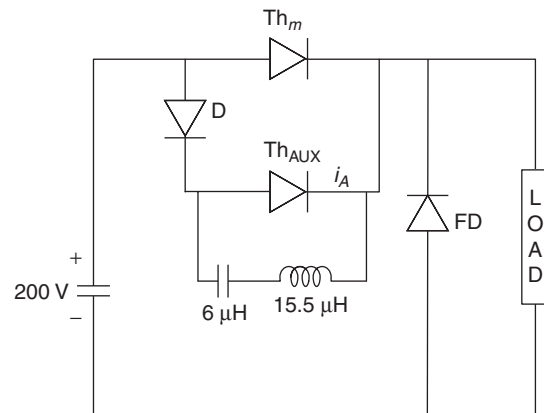
$$t_4 - t_2 = t_{c1} = \left[ \pi - 2 \sin^{-1} \left( \frac{1}{x} \right) \right] \cdot \sqrt{LC}$$

**Example 13:** Among the following which would yield best performance in a thyristor DC chopper?

- (A) Source commutation
- (B) Voltage commutation
- (C) Load commutation
- (D) Current commutation

**Solution:** (D)

**Example 14:** Given below is a current commutated DC-DC chopper where  $(Th)_M$  and  $(Th)_A$  are main and auxiliary thyristors, respectively.



If the auxiliary S.C.R. is triggered at  $t = 0$ , when  $Th_M$  is conducting and a constant load current of 12 A is flowing through the load. The main thyristor is turned OFF between

- (A)  $30 \mu s < t \leq 40 \mu s$
- (B)  $20 \mu s < t \leq 30 \mu s$
- (C)  $10 \mu s < t \leq 20 \mu s$
- (D)  $0 \mu s \leq t \leq 10 \mu s$

### 3.706 | Power Electronics and Drives

**Solution:** (A)

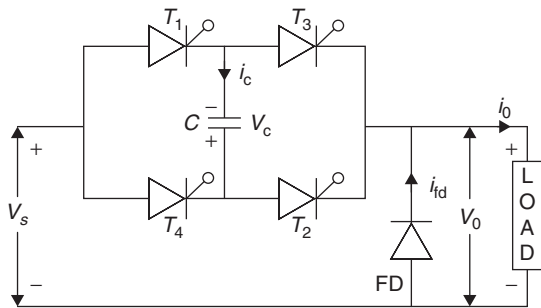
When  $(Th)_A$  is triggered, a tank circuit is formed and conducts for  $\pi\sqrt{LC}$  seconds

$$\pi\sqrt{LC} = \pi\sqrt{15.5 \times 10^{-6} \times 6 \times 10^{-6}} \\ = 3.03 \times 10^{-5} = 30 \mu s$$

After 30  $\mu s$  an opposite current pulse will be injected and  $Th_M$  gets off. It is possible when capacitor current equals load current

$(Th)_M$  gets OFF when  $30 < t \leq 40 \mu s$

### Load-commutated Chopper



#### Operating Modes

**Mode 1:** For  $0 < t < t_1$

- $T_1$  and  $T_2$  are turned ON and the current flows through  $T_1 - C - T_2 - \text{LOAD}$
- $T_3$  and  $T_4$  are OFF
- The output voltage across the load  $V_o = V_s$  and simultaneously the capacitor gets charged.

**Mode 2:** For  $t_1 < t < t_2$

- All  $T_1, T_2, T_3, T_4$  are turned off.

- The capacitor is fully charged and the polarity of the plates reversed when compared to initial condition.
- Free-wheeling diode  $D_1$  starts conducting and the current through the load circulates in the loop.

**Mode 3:** For  $t_2 < t < t_3$

- $T_4$  and  $T_3$  conduct output voltage that appears across the load

$$V_o = V_s + V_c$$

- $T_1$  and  $T_2$  are turned off.
- Since the load voltage is more than source voltage this chopper also is known as step-up chopper.

### Multiphase Chopper

A multiphase chopper is one that consists of two or more choppers connected in parallel at the same frequency but with a proper phase shift. This type of operation enables the load and power supply to be subjected to an effective frequency which is a multiple of the chopping frequency.

- As a result, the supply harmonic current is reduced and the ripple amplitude decreases.

A multiphase chopper may be operated in two modes:

- In phase operation mode
- Phase-shifted operation mode

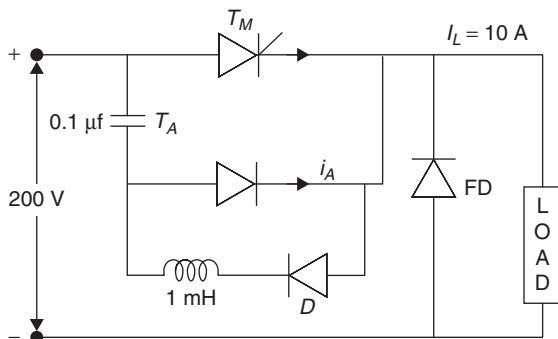
- In the in phase operation mode, all parallel connected choppers are on and off at the same instant.
- In the phase shifted operation mode, different choppers are on and off at different instant of time.
- The inductance  $L$  in series with each chopper is sufficiently large so that each chopper operates independent of each other.

## EXERCISES

### Practice Problems I

**Directions for questions 1 to 15:** Select the correct alternative from the given choices.

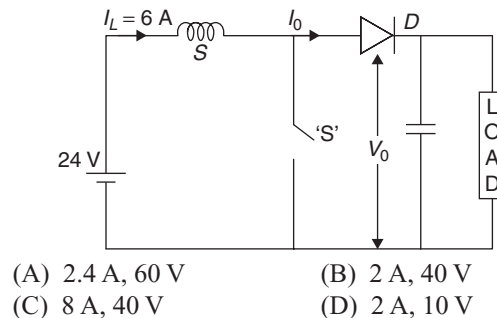
- A voltage-commutated chopper circuit operated at 50 Hz as shown below.



For a load current of 5 A, the ratio of magnitudes of  $I_M$  to  $I_A$  (as indicated in the figure) would be

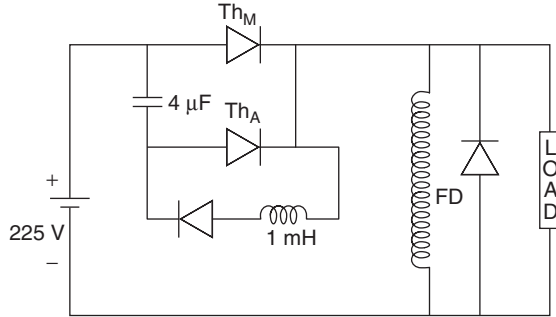
- (A) 0.65 (B) 0.833 (C) 1 (D) 1.2

- A step-up chopper shown below is operated at a duty cycle of 0.6. If a large capacitor is connected across the load and for a constant value of inductor current, then the average values of diode current and load voltage, respectively, are



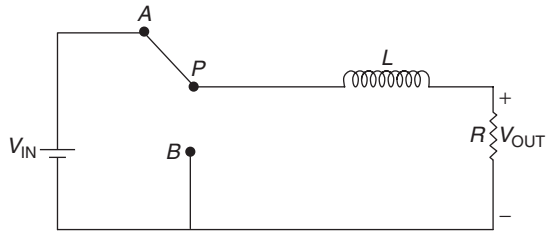
- (A) 2.4 A, 60 V (B) 2 A, 40 V  
(C) 8 A, 40 V (D) 2 A, 10 V

3. The figure shown below is a voltage commutated chopper operating with a duty ratio of 0.4 and at a frequency of 0.5 kHz. The load current is almost ripple free and remains constant at 15 A. The turn off time available to the thyristor  $Th_M$  is (assume the devices to be ideal)



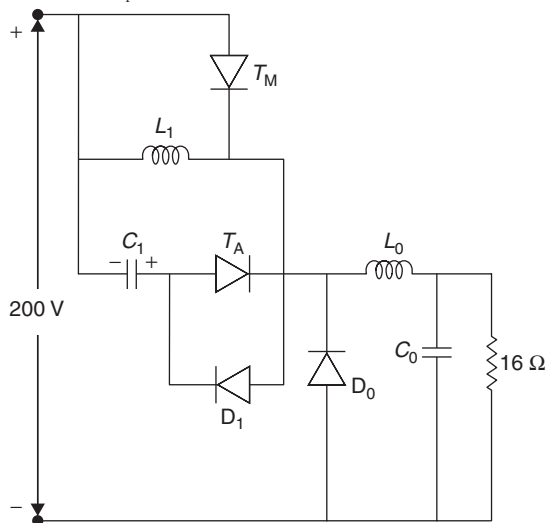
- (A) 30  $\mu$ s (B) 60  $\mu$ s  
(C) 20  $\mu$ s (D) 40  $\mu$ s

4. If the pole P of a single pole double throw switch is connected alternately to throws A and B as shown in the figure below. Which among the following converter does the figure given, represent?



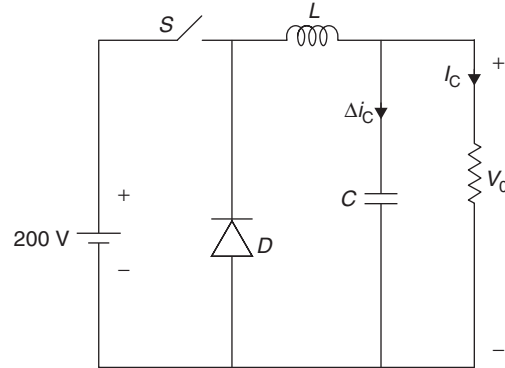
- (A) Half-wave rectifier  
(B) Step-up chopper [Boost converter]  
(C) Step-down converter [Buck converter]  
(D) None of the above

5. A chopper circuit shown in the figure below  $T_M$  is operated at 50% duty ratio. The maximum allowable reapplied  $\frac{dV}{dt}$  on  $T_M$  is 10 V/ $\mu$ s. Assuming the ripple current through  $L_o$  to be negligible, the theoretical minimum values of  $C_1$  should be



- (A) 0.0625  $\mu$ F  
(B) 0.625 F  
(C) 0.625  $\mu$ F  
(D) 0.625 mF

6. The ideal  $S$  in the circuit shown below is operated at 120 kHz at a duty ratio of 0.8. If  $I_o$  is 10 A and  $(\Delta i_c)_{c/p-p}$  is 1.6 A, the peak current in the switch  $S$  is



- (A) 11.6 A  
(B) 12.4 A  
(C) 10.3 A  
(D) 9.3 A

7. A 30 V battery charger feeds an ideal chopper which is operating at 400 Hz. It is supplying power to a resistive load of 1.5  $\Omega$ , assuming the load is shunted by a perfect commutating diode and a loss less battery. The mean load current at an ON/OFF ratio of 1/1 would be

- (A) 15 A  
(B) 10 A  
(C) 20 A  
(D) 25 A

8. A voltage-commutated chopper has following parameters:

$$V_s = 230 \text{ V}$$

Load circuit parameter 5  $\Omega$ , 10 mH, 25 V

Commutation circuit parameters  $L = 5 \mu$ H,  $C = 10 \mu$ F

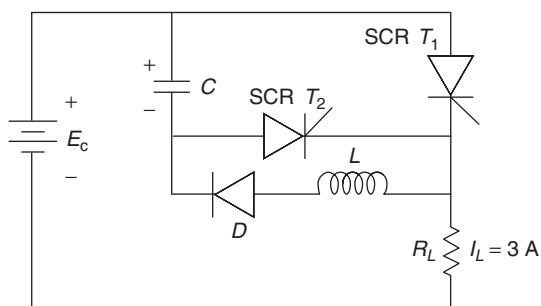
For a constant load current at 115 A, the effective ON period and peak current through the main thyristor are, respectively,

- (A) 100  $\mu$ S, 200 A  
(B) 22.2  $\mu$ S, 440 A  
(C) 700  $\mu$ S, 282.2 A  
(D) 1000  $\mu$ S, 440 A

9. In a type-A-chopper, source voltage is 110 V DC, ON period = 200  $\mu$ S, OFF period = 150  $\mu$ S and load RLE consists of  $R = 4 \Omega$ ,  $L = 10$  mH,  $E = 20$  V.

For continuous conduction, average output voltage and average output current for this chopper are, respectively,

- (A) 40 V, 5 A  
(B) 66.6 V, 28.3 A  
(C) 62.8 V, 10.7 A  
(D) 40 V, 20 A

**Common Data for Questions 10 and 11:**

For the above class D commutation circuit  $E_{DC} = 50$  V,  $I_{cc(max)} = 50$  A,  $T_{OFF}$  of  $SCR_1 = 30$   $\mu$ S chopping frequency  $f = 500$  Hz load variation required is 10% to 100%  $t_{DC} = 2$  S.

10. The value of capacitor  $C$  is  
 (A) 27  $\mu$ F (B) 45  $\mu$ F  
 (C) 52  $\mu$ F (D) 57  $\mu$ F
11. The commutating inductor for allowing large voltage variation at the load is  
 (A) 90  $\mu$ H (B) 67.5  $\mu$ H  
 (C) 45  $\mu$ H (D) 72  $\mu$ H

**Common Data for Questions 12 and 13:**

A voltage commutated chopper has following parameters:  $V_s = 200$  V, load parameters:  $1 \Omega$ ,  $2$  mH,  $5$  V, commutation circuit parameters  $L = 25$   $\mu$ H and  $C = 50$   $\mu$ F

12. For a constant load current of 200 A, the effective ON period is  
 (A) 350  $\mu$ S (B) 100  $\mu$ S  
 (C) 700  $\mu$ S (D) 1400  $\mu$ S
13. The peak current through main thyristor is  
 (A) 200 A (B) 482.8 A  
 (C) 382.8 A (D) 282.8 A

**Common Data for Questions 14 and 15:**

A simple DC chopper is operating at a frequency of 2 kHz from 96 V DC source to supply a load of  $8 \Omega$ . The load time constant is 6ms. The average load voltage is 57.6 V.

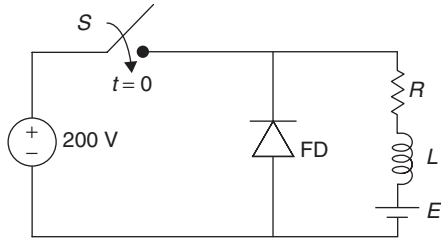
14. The ON period of the chopper is  
 (A) 0.3 ms (B) 0.4 ms  
 (C) 0.6 ms (D) 0.5 ms
15. Average load current is  
 (A) 7.2 A (B) 14.4 A  
 (C) 28.8 A (D) 3.6 A

**Practice Problems 2**

**Directions for questions 1 to 15:** Select the correct alternative from the given choices.

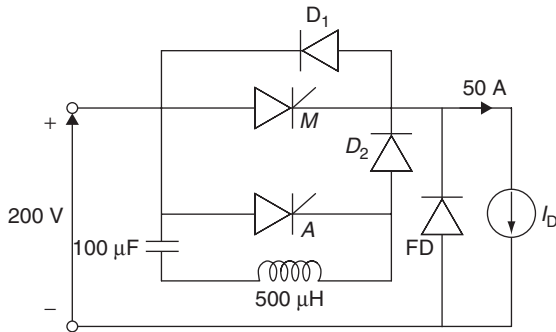
1. The features of chopper drives are  
 (A) Smooth control but slow response  
 (B) Smooth control, fast response but less efficient  
 (C) Smooth control, and fast response  
 (D) None of the above
2. Choppers can be used in future electric automobiles  
 (A) For speed control only  
 (B) For braking only  
 (C) For both speed control and braking  
 (D) None of these
3. Given a step-down chopper of supply voltage 80 V and average output voltage 40 V. Assuming continuous conduction mode and an ON period of 20  $\mu$ s, the chopping frequency will be  
 (A) 10 kHz  
 (B) 20 kHz  
 (C) 50 kHz  
 (D) 25 kHz
4. The per unit ripple in a step-down chopper would have its maximum value at a duty cycle of  
 (A) 20% (B) 40%  
 (C) 50% (D) 75%
5. A type-A chopper is connected to a 200 V DC source and is feeding an RLE load consisting of  $R = 4 \Omega$ ;  $L = 10$  mH;  $E = 20$  V. If the on and off periods are 200  $\mu$ s and 300  $\mu$ s, respectively, then the average output voltage and average output current for continuous conduction are, respectively,  
 (A) 40 V, 15 A (B) 60 V, 25 A  
 (C) 80 V, 15 A (D) 66.66 V, 28.33 A
6. If a step-down DC chopper is connected to a 230 V supply and a resistive load of  $R = 20 \Omega$ ; if the voltage drop across the converter switch is  $V_{ch} = 2$  V. Then the chopper efficiency at  $\alpha = 0.5$  would be  
 (A) 93% (B) 95%  
 (C) 97% (D) 99%
7. Which among the following is a correct match for DC chopper?  
 (A) Input Voltage—Continuous  
 Output Voltage—Continuous  
 (B) Input Voltage—Continuous  
 Output Voltage—Discontinuous  
 (C) Input voltage—Discontinuous  
 Output voltage—Continuous  
 (D) None of the above
8. For the chopper shown in the figure below if minimum instantaneous load current is  $I_1 = 32.75$  A and peak instantaneous load current is  $I_2 = 26.05$  A. The value of RMS value of load current at  $\alpha = 0.5$  would be  
 (A) 36.17 A (B) 22.13 A  
 (C) 63.71 A (D) 43.65 A





9. For the above problem, effective value of input resistance would be  
 (A)  $20 \Omega$  (B)  $13.6 \Omega$   
 (C)  $10 \Omega$  (D)  $18.36 \Omega$

10. The figure shows a current commutated chopper feeding a load such that a constant current of 50 A is maintained at the load. The peak commutating current in the circuit is



- (A) 40 A (B) 60 A  
 (C) 20 A (D) 89 A

11. In a current-commutated chopper,  
 (A) Peak commutating current should be less than maximum load current  
 (B) Peak commutating current should be equal to maximum load current  
 (C) Peak commutating current should be greater than maximum load current  
 (D) There is no relation between peak commutating current and maximum load current
12. A 3- $\phi$  wound rotor induction motor is controlled by a chopper controlled resistance in its rotor circuit. A resistance of  $2 \Omega$  connected in the rotor circuit and a resistance of  $4 \Omega$  is additionally connected during OFF periods of the chopper. The OFF period of the chopper

is 4 ms. The average resistance in the rotor circuit for the chopper frequency of 200 Hz is

- (A)  $\frac{26}{5} \Omega$  (B)  $\frac{24}{5} \Omega$   
 (C)  $\frac{18}{5} \Omega$  (D)  $\frac{16}{5} \Omega$

13. A voltage commutated chopper has the following parameters:

$V_s = 200 \text{ V}$ , load circuit parameter  $1 \Omega$ ,  $2 \text{ mH}$ ,  $5 \text{ V}$ .

Commutation circuit parameter:  $L = 25 \mu\text{H}$ ,  $C = 50 \mu\text{F}$ .

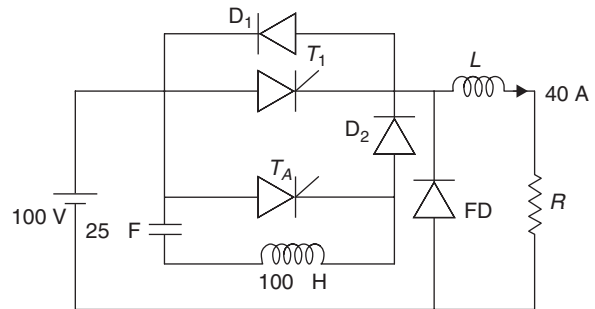
For constant load current at 100 A, the effective on period and peak current through the main thyristor are, respectively,

- (A)  $1000 \mu\text{s}$ ,  $200 \text{ A}$   
 (B)  $700 \mu\text{s}$ ,  $382.8 \text{ A}$   
 (C)  $500 \mu\text{s}$ ,  $282.8 \text{ A}$   
 (D)  $1000 \mu\text{s}$ ,  $382.8 \text{ A}$

14. A DC–DC transistor chopper is supplied from a fixed voltage DC source feeds an RLE load and a free-wheeling diode. The chopper operates at 1 kHz and 50% duty cycle. Keeping the average DC value of current and duty cycle unchanged and by increasing chopper frequency; the ripple content of load current would

- (A) Increase  
 (B) Reduce  
 (C) Remain the same  
 (D) Cannot be determined

15. The figure shows a DC–DC chopper feeding on RL load such that the load current is 40 A. If the thyristor TA is fired at  $t = 0$

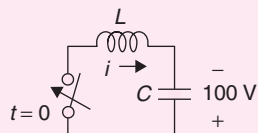


- (A)  $64 \mu\text{s}$  (B)  $128 \mu\text{s}$   
 (C)  $100 \mu\text{s}$  (D)  $200 \mu\text{s}$

## PREVIOUS YEARS' QUESTIONS

**Common Data for Questions 1 and 2:**

The  $L$ - $C$  circuit shown in the figure has an inductance  $L = 1$  mH and a capacitance  $C = 10$   $\mu$ F.



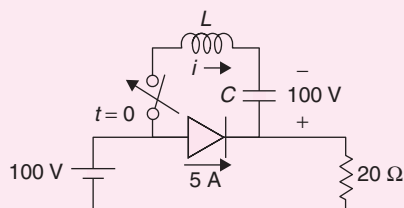
1. The initial current through the inductor is zero, while the initial capacitor voltage is 100 V. The switch is closed at  $t = 0$ . The current  $i$  through the circuit is:

[2010]

- (A)  $5\cos(5 \times 10^3 t)$  A      (B)  $5\sin(10^4 t)$  A  
(C)  $10\cos(5 \times 10^3 t)$  A      (D)  $10\sin(10^4 t)$  A

2. The  $L$ - $C$  circuit of above question is used to commutate a thyristor, which is initially carrying a current of 5 A as shown in the figure below. The values and initial conditions of  $L$  and  $C$  are the same as in above question. The switch is closed at  $t = 0$ . If the forward drop is negligible, the time taken for the device to turn off is

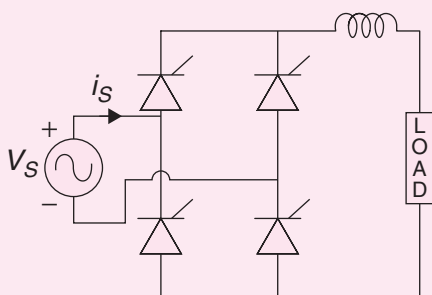
[2010]



- (A) 52  $\mu$ s      (B) 156  $\mu$ s  
(C) 312  $\mu$ s      (D) 26  $\mu$ s

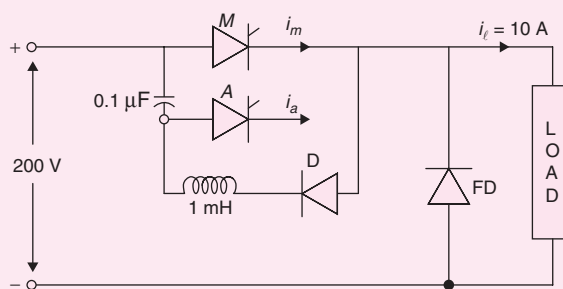
3. A fully controlled converter bridge feeds a highly inductive load with ripple-free load current. The input supply ( $v_s$ ) to the bridge is a sinusoidal source. Triggering angle of the bridge converter is  $\alpha = 30^\circ$ . The input power factor of the bridge is \_\_\_\_\_

[2010]



4. A voltage-commutated chopper circuit, operated at 500 Hz, is shown below.

[2011]

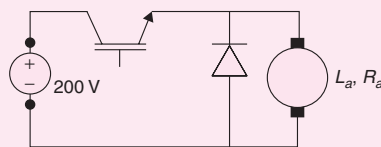


If the maximum value of load current is 10 A, then the maximum current through the main ( $M$ ) and auxiliary ( $A$ ) thyristors will be

- (A)  $i_{M_{\max}} = 12$  A and  $i_{A_{\max}} = 10$  A  
(B)  $i_{M_{\max}} = 12$  A and  $i_{A_{\max}} = 2$  A  
(C)  $i_{M_{\max}} = 10$  A and  $i_{A_{\max}} = 12$  A  
(D)  $i_{M_{\max}} = 10$  A and  $i_{A_{\max}} = 8$  A

5. The separately excited DC motor in the figure below has a rated armature current of 20 A and a rated armature voltage of 150 V. An ideal chopper switching at 5 kHz is used to control the armature voltage. If  $L_a = 0.1$  mH,  $R_a = 1$   $\Omega$ , neglecting armature reaction, the duty ratio of the chopper to obtain 50% of the rated torque at the rated speed and the rated field current is

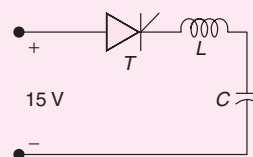
[2013]



- (A) 0.4      (B) 0.5      (C) 0.6      (D) 0.7

6. Thyristor  $T$  in the figure below is initially off and is triggered with a single pulse of width 10  $\mu$ s. It is given that  $L = \left(\frac{100}{\pi}\right)$   $\mu$ H and  $C = \left(\frac{100}{\pi}\right)$   $\mu$ F. Assuming latching and holding current of the thyristor are both zero and the initial charge on  $C$  is zero,  $T$  conducts for

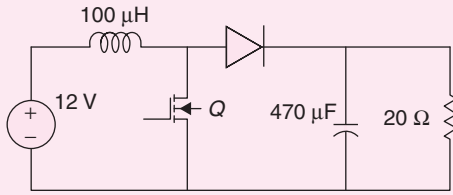
[2013]



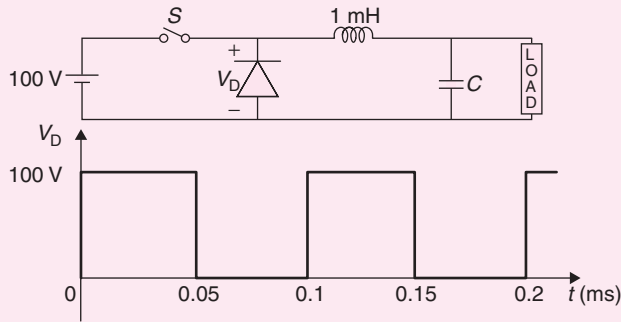
- (A) 10  $\mu$ s      (B) 50  $\mu$ s  
(C) 100  $\mu$ s      (D) 200  $\mu$ s

**Common Data for Questions 7 and 8:**

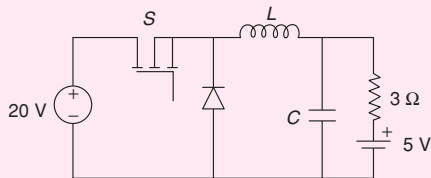
In the figure shown below, the chopper feeds a resistive load from a battery source. MOSFET  $Q$  is switched at 250 kHz, with a duty ratio of 0.4. All elements of the circuit are assumed to be ideal.



7. The average source current in ampere in steady state is [2013]  
 (A)  $3/2$  (B)  $5/3$  (C)  $5/2$  (D)  $5/4$
8. The PEAK-TO-PEAK source current ripple in ampere is [2013]  
 (A) 0.96 (B) 0.144  
 (C) 0.192 (D) 0.288
9. Figure (i) shows the circuit diagram of a chopper. The switch  $S$  in the circuit in figure (i) is switched such that the voltage  $v_D$  across the diode has the wave shape as shown in figure (ii). The capacitance  $C$  is large so that the voltage across it is constant. If switch  $S$  and the diode are ideal, the peak to peak ripple (in A) in the inductor current is [2014]

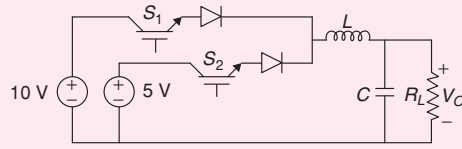


10. A step-up chopper is used to feed a load at 400 V DC from a 250 V DC source. The inductor current is continuous. If the 'off' time of the switch is 20  $\mu$ s, the switching frequency of the chopper in kHz is [2014]
11. In the following chopper, the duty ratio of switch is 0.4. If the inductor and capacitor are sufficiently large to ensure continuous inductor current and ripple free capacitor voltage, the charging current (in Ampere) of the 5 V battery, under steady-state is [2015]

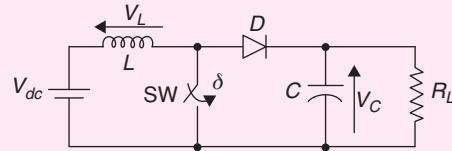


12. The circuit shown is meant to supply a resistive load  $R_L$  from two separate DC voltage sources. The switches  $S_1$  and  $S_2$  are controlled so that only one of them is ON at any instant.  $S_1$  is turned on for 0.2 ms and  $S_2$  is turned on for 0.3 ms in a 0.5 ms switching cycle time period. Assuming continuous conduction of the

inductor current and negligible ripple on the capacitor voltage, the output voltage  $V_o$  (in Volt) across  $R_L$  is [2015]

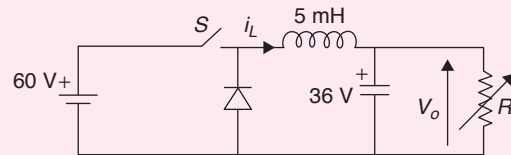


13. A self commutating switch SW, operated at duty cycle  $\delta$  is used to control the load voltage as shown in the figure

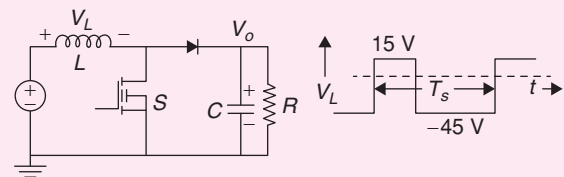


Under steady state operating conditions, the average voltage across the inductor and the capacitor respectively, are [2015]

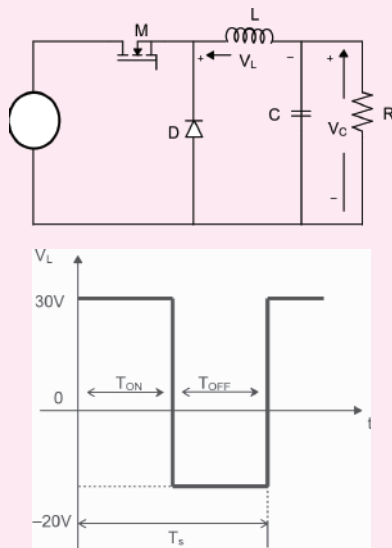
- (A)  $V_L = 0$  and  $V_C = \frac{1}{1-\delta} V_{dc}$   
 (B)  $V_L = \frac{\delta}{2} V_{dc}$  and  $V_C = \frac{1}{1-\delta} V_{dc}$   
 (C)  $V_L = 0$  and  $V_C = \frac{\delta}{1-\delta} V_{dc}$   
 (D)  $V_L = \frac{\delta}{2} V_{dc}$  and  $V_C = \frac{\delta}{1-\delta} V_{dc}$
14. A buck converter feeding a variable resistive load is shown in the figure. The switching frequency of the switch  $S$  is 100 kHz and the duty ratio is 0.6. The output voltage  $V_o$  is 36 V. Assume that all the components are ideal, and that the output voltage is ripple-free. The value of  $R$  (in Ohm) that will make the inductor current ( $i_L$ ) just continuous is [2015]



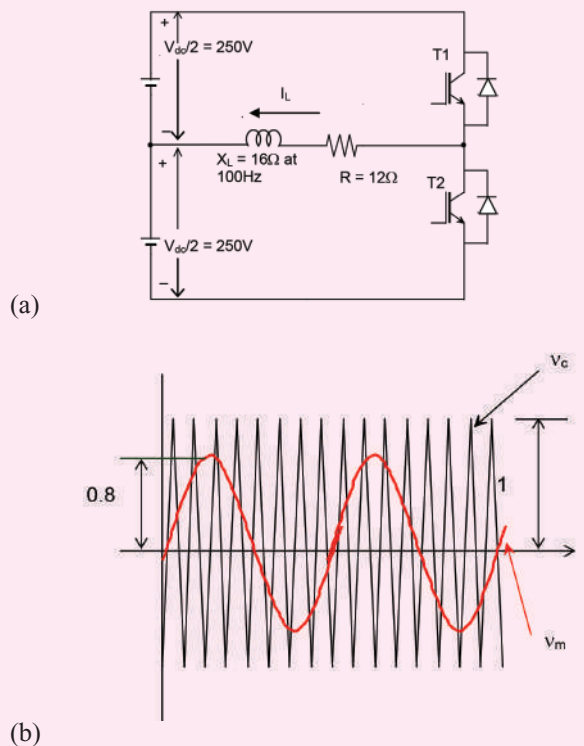
15. For the switching converter shown in the following figure, assume steady-state operation. Also assume that the components are ideal, the inductor current is always positive and continuous and switching period is  $T_s$ . If the voltage  $V_L$  is as shown, the duty cycle of the switch  $S$  is [2015]



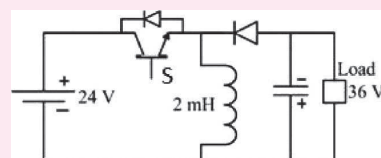
16. A buck converter, as shown in Figure (a) below, is working in steady state. The output voltage and the inductor current can be assumed to be ripple free. Figure (b) shows the inductor voltage  $V_L$  during a complete switching interval. Assuming all devices are ideal, the duty cycle of the buck converter is \_\_\_\_\_.



17. The switches T1 and T2 in Figure (a) are switched in a complementary fashion with sinusoidal pulse width modulation technique. The modulating voltage  $\nu_m(t) = 0.8 \sin(200\pi t)$  V and the triangular carrier voltage ( $\nu_c$ ) are as shown in Figure (b). The carrier frequency is 5 kHz. The peak value of the 100 Hz component of the load current ( $i_L$ ), in ampere, is \_\_\_\_\_.



18. A buck-boost DC – DC converter, shown in the figure below, is used to convert 24V battery voltage to 36V DC voltage to feed a load of 72W. It is operated at 20kHz with an inductor of 2mH and output capacitor of 1000μF. All devices are considered to be ideal. The peak voltage across the Solid-state switch (S), in volt is \_\_\_\_\_.



19. A DC - DC boost converter, as shown in the figure below, is used to boost 360V to 400V, at a power of 4kW. All devices are ideal. Considering continuous inductor current, the rms current in the Solid state switch (S), in ampere is \_\_\_\_\_.

## ANSWER KEYS

### EXERCISES

#### Practice Problems 1

- |       |       |       |       |       |      |      |      |      |       |
|-------|-------|-------|-------|-------|------|------|------|------|-------|
| 1. D  | 2. A  | 3. B  | 4. C  | 5. C  | 6. A | 7. B | 8. B | 9. C | 10. B |
| 11. C | 12. C | 13. B | 14. A | 15. A |      |      |      |      |       |

#### Practice Problems 2

- |       |       |       |       |       |      |      |      |      |       |
|-------|-------|-------|-------|-------|------|------|------|------|-------|
| 1. C  | 2. C  | 3. D  | 4. C  | 5. C  | 6. D | 7. B | 8. A | 9. B | 10. D |
| 11. C | 12. D | 13. B | 14. B | 15. A |      |      |      |      |       |

#### Previous Years' Questions

- |       |       |         |                  |      |          |         |        |           |           |
|-------|-------|---------|------------------|------|----------|---------|--------|-----------|-----------|
| 1. D  | 2. A  | 3. 0.78 | 4. A             | 5. D | 6. C     | 7. B    | 8. C   | 9. 2.5    | 10. 31.25 |
| 11. 1 | 12. 7 | 13. A   | 14. 2480 to 2520 |      | 15. 0.75 | 16. 0.4 | 17. 10 | 18. 60.03 | 19. 3.51  |