### HEAT TRANSFER, REFRIGERATION AND AIR CONDITIONING TEST 4

### Number of Questions 35

*Directions for questions 1 to 35:* Select the correct alternative from the given choices.

- 1. Convective heat transfer coefficient '*h*' varies significantly with
  - (A) the type of fluid
  - (B) the temperature
  - (C) the thermal conductivity
  - (D) All of the above
- 2. In case of one dimensional heat conduction in a medium with constant properties, *T* is the temperature at posi- $\partial T$

tion x, at time t. Then  $\frac{\partial T}{\partial t}$  is proportional to

(A) 
$$\frac{T}{X}$$
 (B)  $\frac{\partial T}{\partial X}$ 

(C) 
$$\frac{\partial^2 T}{\partial X \partial T}$$
 (D)  $\frac{\partial^2 T}{\partial X^2}$ 

- 3. Biot number is the ratio of
  - (A) internal resistance to the surface resistance
  - (B) surface resistance to the internal resistance
  - (C) conductivity to the heat transfer co-efficient
  - (D) convective heat transfer to conductive heat transfer
- **4.** Which one of the following configurations has the highest fin effectiveness?
  - (A) Thin, closely spaced fins
  - (B) Thin, widely spaced fins
  - (C) Thick, widely spaced find
  - (D) Thick, closely spaced fins
- 5. Fouling factor in heat exchanger is estimated as

(A) 
$$U_{\text{foul}} = R_f + U_{\text{clean}}$$
 (B)  $U_{\text{foul}} + R_f = U_{\text{clean}}$   
(C)  $\frac{1}{U_{\text{foul}}} = R_f + \frac{1}{U_{\text{clean}}}$  (D)  $\frac{1}{U_{\text{foul}}} + R_f = \frac{1}{U_{\text{clean}}}$ 

- 6. Thermal conductivity is lower for
  - (A) wood (B) air
  - (C) water at  $100^{\circ}$ C (D) steam at 1 bar
- 7. In pool boiling, the highest heat transfer coefficient occurs in
  - (A) sub-cooled boiling zone
  - (B) nucleate boiling zone
  - (C) partial film boiling zone
  - (D) film boiling zone
- 8. Which of the following is closed to black body nature?(A) glass(B) water at 100°C
  - (C) ice (D) coal
- **9.** The number of transfer units in heat exchanges is equal to

Where A =Area

$$U =$$
 over all heat transfer co-efficient.

$$C_{min}$$
 = minimum heat capacity.

(A) 
$$\frac{AU}{C_{\min}}$$
 (B)  $\frac{C_{\min}}{AU}$   
(C)  $\frac{AU}{C_{\max}}$  (D)  $\frac{C_{\max}}{AU}$ 

10. In counter flow heat exchanger, if  $\theta_1 = \theta_2$  then the LMTD for the heat exchanger will be

(A) zero (B) 
$$\frac{\theta_1 - \theta_2}{\ln(\theta_1/\theta_2)}$$

- (C)  $\theta_1$  (or)  $\theta_2$  (D) undefined
- **11.** The refrigerant used for absorption refrigerators, working heat from solar collectors is mixture of water and
  - (A) carbon dioxide (B) sulphur dioxide
  - (C) lithium bromide (D) freon 12
- 12. During the adiabatic cooling of moist air
  - (A) DBT remains constant
  - (B) Specific humidity remains constant
  - (C) Relative humidity remains constant
  - (D) WBT remains constant
- **13.** For an air conditioning plant above 300 ton, which one of the following system would normally be preferred?
  - (A) Ammonia reciprocating compressor
  - (B) Centrifugal chiller
  - (C) Absorption refrigeration system
  - (D) Hermetic compressor
- 14. The maximum COP for the absorption cycle is given by ( $T_G$  = generator temperature,  $T_C$  = environment temperature,  $T_F$  = refrigerated space temperature)

(A) 
$$\frac{T_E \left(T_G - T_E\right)}{T_G \left(T_C - T_E\right)}$$
(B) 
$$\frac{T_G \left(T_C - T_E\right)}{T_E \left(T_G - T_E\right)}$$
(C) 
$$\frac{T_C \left(T_G - T_E\right)}{T_G \left(T_C - T_E\right)}$$
(D) 
$$\frac{T_G \left(T_C - T_E\right)}{T_C \left(T_G - T_E\right)}$$

**15.** One ton refrigeration is equivalent to (A) 3.5 kW (B) 50 kJ/s

(C) 1000 J/min (D) 1000 kJ/min

- **16.** Consider the development of laminar boundary layer for a moving non-reacting fluid in contact with a flat plate of length 'l' along the flow direction. The average value of heat transfer co-efficient can be obtained by multiplying the local heat transfer co-efficient at the trailing edge by the factor
  - (A) 0.75 (B) 1.0 (C) 1.5 (D) 2.0
- 17. A spherical aluminum shell of inside diameter 2.5 m is evacuated and used as radiation test chamber. If the

Time:60 min.

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inner surface is coated with carbon black and maintained at 600 K, the irradiation on a small test surface placed inside the chamber (Stefan-Boltzman constant  $\sigma = 5.67 \times 10^{-8} \text{ W/m}^2 \text{ K}^4$ ) in W/m<sup>2</sup> is

(A) 500.54 (B) 7348.32

(C) 8500 (D) 10000

**18.** Match List-I with List-II and select the correct answer using the codes given below.

	List - I		List - II			
Ρ	Fin	1	AU/C <sub>min</sub>			
Q	Heat exchanger	2	$X/2\sqrt{a\tau}$			
R	Transient conduction	3	$\sqrt{hp / kA}$			
S	Heisler chart	4	hL/k			
	P-3, Q-1, R-4, S-2 P-1, Q-2, R-3, S-4		(B) <i>P</i> -1, <i>Q</i> -4, <i>R</i> -3, <i>S</i> -2 (D) <i>P</i> -4, <i>Q</i> -3, <i>R</i> -2, <i>S</i> -1			

- 19. A 1m thick plane wall has its two surfaces kept at 400°C and 300°C. Thermal conductivity of the wall varies linearly with temperature and its values at 400°C and 300°C are 40 W/mK and 30 W/mK, respectively. The steady heat flux through the wall in kW/m<sup>2</sup> is
  (A) 5 (B) 4
  - (C) 3.5 (D) 3
- 20. The average Nusselt number in laminar natural convection from a vertical wall at 180°C with still air at 20°C is found to be 48. If the wall temperature becomes 30°C, all other parameters remaining same, the average Nusselt number will be

(A)	8	(B)	16
(C)	24	(D)	32

**21.** Match List I with List II and select the correct answer using the code given below the lists.

	List - I (Application)		List - II (Type of heat exchanger)			
P.	Gasto liquid	1.	Compact			
Q.	Space vehicle	2.	Shell and tube			
R.	Condenser	3.	Finned tube			
S.	Air pre-heater	4.	Regenerative			

- (A) P-2, Q-4, R-3, S-1
  (B) P-3, Q-1, R-2, S-4
  (C) P-2, Q-1, R-3, S-4
  (D) P-3, Q-4, R-2, S-1
- **22.** In a mass transfer process of diffusion of hot smoke in cold air in a power plant, the temperature profile and the concentration profile will become identical when
  - (A) Prandtl No. = 1
     (B) Nusselt No. = 1
     (C) Lewis No. = 1
     (D) Schmit No. = 1
- **23.** Heat is lost from a 100 mm diameter steam pipe placed horizontally in ambient at 30°C. If the Nusselt number is 25 and thermal conductivity of air is 0.03 W/mK, then the heat transfer co-efficient in W/m<sup>2</sup>K will be

- (A) 10 (B) 7.5 (D) 2.5
- (C) 5 (D) 2.5
- **24.** Match List-I with List-II and select the correct answer using the code given below the lists:

	List - I		List - II				
Р.	Grashof number	1.	Mass diffusion				
Q.	Schmid number	2.	Free convection				
R.	Weber number	3.	Surface tension				
S.	Fourier number	4.	Transient-heat conduction				
$(\Lambda)$	$P_{-2} O_{-1} R_{-3} S_{-4}$ (B) $P_{-1} O_{-2} R_{-3} S_{-4}$						

- (A) *P*-2, *Q*-1, *R*-3, *S*-4 (B) *P*-1, *Q*-2, *R*-3, *S*-4 (C) *P*-4, *Q*-3, *R*-2, *S*-1 (D) *P*-4, *Q*-3, *R*-1, *S*-2
- (-)
- **25.** The time constant of thermo couple is
  - (A) The time taken to attain 100% initial temperature difference.
  - (B) Time taken to attain 63.2% of initial temperature difference.
  - (C) Time taken to attain 50% of initial temperature difference.
  - (D) The minimum time taken to record a temperature reading.
- **26.** A large concrete slab of 1 m thick has one dimensional temperature distribution:

 $T = 4 - 10 x + 20 x^2 + 10 x^3,$ 

Where *T* is temperature and *x* is distance from one face towards other face of wall. If slab material has thermal diffusivity of  $2 \times 10^{-3}$  m<sup>2</sup>/h.

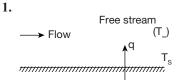
- The rate of change of temperature at the other face of the wall in °C/h is
- (A) 0.4 (B) 0.3 (C) 0.2 (D) 0.1
- 27. A hollow pipe of 1 cm outer diameter is to be insulated by thick cylindrical insulation having thermal conductivity 1 W/mK. The surface heat transfer co-efficient on the insulation surface is 5 W/m<sup>2</sup> K. The minimum effective thickness of insulation for causing the reduction in
  - heat leakage the insulated pipe is (D) = 0.5
  - (A) 10 cm (B) 0.5 cm (C) 10.5 cm
  - (C) 19.5 cm (D) 20 cm
- **28.** The geometric radius of heat transfer for a hollow sphere of inner and outer radii  $r_1$  and  $r_2$  is
  - (A)  $\sqrt{r_1 r_2}$  (B)  $r_2 r_1$ (C)  $\frac{r_1 + r_2}{2}$  (D)  $r_2/r_1$
- **29.** A vapour compression refrigerator has a COP of 4 and extracts 10 kJ of heat from the cold reservoir. If this machine is worked as a heat pump, how much heat will it deliver to the environment?
  - (A) 5 kJ (B) 10 kJ
  - (C) 12.5 kJ (D) 15 kJ

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<b>30.</b> During the sensible cooling process, specific humidity	<b>33.</b> Power input in kW is			
(A) remains constant (B) increases	(A) 0.98 (B) 1.02			
(C) decreases (D) undpredicable	(C) 1.05 (D) 1.13			
<b>31.</b> The wet bulb depression is zero, when relative humidity is equal to	<b>Statement for linked answer Questions 34 and 35:</b> In a certain counter flow heat exchanger, hot fluid enters at			
(A) 100% (B) 60%	450 °C and has mass flow rate of 1 kg/s. Cold fluid enters at			
(C) 40% (D) zero	25 °C and has mass flow rate of 4 kg/s. Effectiveness of heat			
<b>Common Data Questions 32 and 33:</b> In a 5 kW cooling capacity refrigeration system operating on simple VCRS. The refrigerant enters the evaporator with a enthalpy of 75 kJ/kg and leaves with enthalpy of 185 kJ/ kg. The enthalpy of the refrigerant after compression is 210	<ul> <li>exchanger is 75%. Specific heat of hot fluid is 4 kJ/kg K and that of cold fluid is 1 kJ/kg K.</li> <li>34. Exit temperature of cold fluid in °C is <ul> <li>(A) 343</li> <li>(B) 243</li> <li>(C) 143</li> <li>(D) 43</li> </ul> </li> </ul>			
kJ/kg.	<b>35.</b> The heat transfer rate in kW is			
<b>32.</b> The C.O.P will be	(A) 1175 (B) 1275			
(A) 3.4 (B) 4.4	(C) 2275 (D) 3175			
(C) 5 (D) 5.2				

Answer Keys										
1. D	<b>2.</b> D	<b>3.</b> A	<b>4.</b> A	<b>5.</b> C	<b>6.</b> B	<b>7.</b> C	8. C	<b>9.</b> A	<b>10.</b> C	
11. D	12. B	<b>13.</b> A	14. C	15. A	16. D	17. B	18. A	<b>19.</b> C	<b>20.</b> C	
<b>21.</b> B	<b>22.</b> A	<b>23.</b> B	<b>24.</b> A	<b>25.</b> B	<b>26.</b> C	<b>27.</b> C	<b>28.</b> A	<b>29.</b> C	<b>30.</b> A	
<b>31.</b> A	<b>32.</b> B	33. D	<b>34.</b> A	<b>35.</b> B						

# **HINTS AND EXPLANATIONS**



Velocity of fluid layer at the wall is zero (no slip condition) so the heat must be transferred only by conduction at the wall

$$\therefore \quad h(\Delta T) = -K \frac{\diamondsuit T}{\diamondsuit y}\Big|_{y=0}$$
$$\therefore \quad h = -\frac{K}{\mathsf{T}_{\mathrm{s}} - \mathsf{T}_{\infty}} \frac{\blacklozenge T}{\diamondsuit y}\Big|_{y=0}$$

Hence convective heat transfer co-efficient depends on thermal conductivity and temperature gradient at the wall.

And also heat transfer co-efficient h varies with the type of fluid and temperature. Choice (D)

2. One dimensional heat conduction equation is

$$\frac{\partial^2 T}{\partial X^2} + \frac{q_y}{k} = \frac{1}{a} \frac{\partial T}{\partial t}$$
  
$$\therefore \frac{\partial T}{\partial t} \propto \frac{\partial^2 T}{\partial X^2}$$
 Choice (D)

 $\left(\frac{L_c}{k}\right)_{-}$ 3. Biot number  $(Bi) = \frac{h L_c}{k}$ internal resistance surface resistance Choice (A)

- 4. Choice (A)
- 5. Fouling factor  $R_f = \frac{1}{U_{foul}} \frac{1}{U_{clean}}$ Choice (C)
- 6. Choice (B)
- 7. Choice (C)
- 8. For ice absorptivity  $\alpha \approx 0.98$ 
  - emissivity = 0.98*.*.. Hence ice is approximately closed to black body. Choice (C)

9. NTU = 
$$\frac{AU}{C_{\min}}$$
 C

 $\langle \alpha \rangle$ 

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- **11.** Choice (D)
- 12. Choice (B)
- 13. Choice (A) 14. Choice (C)

Choice (A)

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**17.** Irradiation 
$$q = \sigma T_1^4$$
  
= 5.67 × 10<sup>-8</sup> × 600<sup>4</sup>  
= 7348.32 W/m<sup>2</sup> Choice (B)

**18.** Choice (A)

19. Thickness of plane wall 
$$L = 1 \text{ m}$$
  
 $t_1 = 400^{\circ}\text{C} \ k_1 = 40 \text{ W/mK}$   
 $t_2 = 300^{\circ}\text{C} \ k_2 = 30 \text{ W/mK}$   
Heat flow rate  $d = \frac{km \ A(t_1 - t_2)}{L}$   
Where  $k_m = \frac{k_1 + k_2}{2} = \frac{40 + 30}{2} = \frac{70}{2}$   
 $= 35 \text{ W/mK}$   
 $Q = \frac{35 \times (400 - 300)}{1} = 3500 \text{ W/m}^2$   
 $= 3.5 \text{ kW/m}^2$ 

20. In laminar flow 
$$Nu = (Gr.Pr)^{1/4}$$
  
 $Gr = \frac{g\beta L^2(\Delta T)}{\vartheta^2}$   
 $Nu \ \mu \ (\Delta T)^{1/4}$   
 $\frac{Nu_1}{Nu_2} = \frac{(\Delta T_1)^{1/4}}{(\Delta T_2)^{1/4}} = \frac{(180 - 20)^{1/4}}{(30 - 20)^{1/4}} = 2$   
 $Nu_2 = \frac{48}{2} = 24$  Choice (C)

**21.** Choice (B)

22. 
$$\frac{\delta_h}{\delta_t} = (P_r)^{\frac{1}{3}}$$
  
 $\delta_h$  = thickness of hydrodynamic boundary layer  
 $\delta_t$  = thickness of thermal boundary layer.  
If  $P_r = 1$ ,  $\delta_h = \delta_t$  Choice (A)  
23.  $Nu = 25$ 

$$Nu = \frac{hD}{k}$$

$$h = \frac{Nu.k}{D} = \frac{25 \times 0.03}{100 \times 10^{-3}}$$

$$= 7.5 \text{ W/m}^2 \text{ K} \qquad \text{Choice (B)}$$

**24.** Choice (A)

**25.** Choice (B)

26. Given 
$$T = 4 - 10 x + 20 x^2 + 10 x^3$$
  
 $\alpha = 2 \times 10^{-3} \text{ m}^2/\text{hr}$   
 $\frac{\partial^2 T}{\partial x^2} = \frac{1}{a} \cdot \left(\frac{\partial T}{\partial t}\right)$   
 $\left(\frac{\partial T}{\partial t}\right)_{x=1} = a \cdot \left(\frac{\partial^2 T}{\partial x^2}\right)_{x=1}$   
 $\frac{\partial T}{\partial x} = -10 + 40 x + 30 x^2$ 

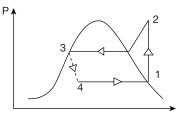
$$\frac{\partial^2 T}{\partial x^2} = 40 + 60x$$

$$\therefore \left(\frac{\partial T}{\partial t}\right)_{x=1} = 2 \times 10^{-3} (40 + 60 \times 1) = 0.2^{\circ}\text{C/hr}\text{ Choice (C)}$$
27.  $d_o = 1 \text{ cm}, r_o = 0.5 \text{ cm}$ 
 $k = 1 \text{ W/mK}$ 
 $h_o = 5 \text{ W/m}^2 \text{ K}$ 
 $r_c = \frac{k}{h_o} = \frac{1}{5} = 0.2 \text{ m} = 20 \text{ cm}$ 
The minimum effective thickness =  $r_c - r_o$ 
 $= 20 - 0.5 = 19.5 \text{ cm}$ 
Choice (C)
28. Choice (A)
29.
$$(\text{C.O.P})_R = 4$$
 $(\text{C.O.P})_{HP} = 1 + (\text{C.O.P})_R$ 
 $= 1 + 4 = 5$ 
 $(C.O.P)_{HP} = \frac{Q_1}{Q_1 - Q_2}$ 
 $5 = \frac{Q_1}{Q_1 - 10}$ 
 $5Q_1 - 50 = Q_1$ 
 $4Q_1 = 50$ 
 $Q_1 = \frac{50}{4} = 12.5 \text{ kJ}$ 
Choice (C)

- **30.** Choice (A)
- **31.** Wet bulb depression = DBT WBTFor saturated air ( $\phi = 100\%$ ) DBT = WBT Choice (A)

32.

Choice (C)



 $h_{1} = 185 \text{ kJ/kg}$   $h_{2} = 210 \text{ kJ/kg}$   $h_{4} = 75 \text{ kJ/kg}$ Refrigeration capacity = 5 kW i.e.,  $m(h_{1} - h_{4}) = 5 \text{ kW}$   $m = \frac{5}{(185 - 75)} = 0.04545 \text{ kg/s}$  3.152 | Heat Transfer, Refrigeration and Air Conditioning Test 4

C.O.P = 
$$\frac{h_1 - h_4}{h_2 - h_1} = \frac{185 - 75}{210 - 185}$$
  
= 4.4 Choice (B)  
= 0.04545(210 - 185)  
= 1.13 kW Choice (D)  
34.  
$$(t) \int_{cold fluid}^{450 \circ C} \int_{cold fluid}^{450 \circ C} \int_{cold fluid}^{hot fluid} \int_{cl}^{25 \circ C} \int_{cl}^{cl} \frac{1 \text{ kg/s}}{25 \circ C} \int_{c_2}^{25 \circ C} \int_{c_2$$

Choice (A)

Choice (B)