

Short Notes for FLUID MECHANICS

Pressure (P):

- If F be the normal force acting on a surface of area A in contact with liquid, then pressure exerted by liquid on this surface is: $P = F/A$
- **Units :** N/m^2 or Pascal (S.I.) and Dyne/cm² (C.G.S.)
- **Dimension :** $[P] = \frac{[F]}{[A]} = \frac{[MLT^{-2}]}{[L^2]} = [ML^{-1}T^{-2}]$
- **Atmospheric pressure:** Its value on the surface of the earth at sea level is nearly $1.013 \times 10^5 N/m^2$ or Pascal in S.I. other practical units of pressure are atmosphere, bar and torr (mm of Hg)
- $1 \text{ atm} = 1.01 \times 10^5 \text{ Pa} = 1.01 \text{ bar} = 760 \text{ torr}$
- **Fluid Pressure at a Point:** $\rho = \frac{dF}{dA}$

Density (ρ):

- In a fluid, at a point, density ρ is defined as: $\rho = \lim_{\Delta V \rightarrow 0} \frac{\Delta m}{\Delta V} = \frac{dm}{dV}$
- In case of homogenous isotropic substance, it has no directional properties, so is a scalar.
- It has dimensions $[ML^{-3}]$ and S.I. unit kg/m^3 while C.G.S. unit g/cc with $1 g/cc = 10^3 kg/m^3$
- Density of body = Density of substance
- Relative density or specific gravity which is defined as : $RD = \frac{\text{Density of body}}{\text{Density of water}}$
- If m_1 mass of liquid of density ρ_1 and m_2 mass of density ρ_2 are mixed, then as

$$m = m_1 + m_2 \text{ and } V = (m_1 / \rho_1) + (m_2 / \rho_2) \quad [\text{As } V = m / \rho]$$

$$\rho = \frac{m}{V} = \frac{m_1 + m_2}{(m_1 / \rho_1) + (m_2 / \rho_2)} = \frac{\sum m_i}{\sum (m_i / \rho_i)}$$

If $m_1 = m_2$, $\rho = \frac{2\rho_1\rho_2}{\rho_1 + \rho_2} = \text{Harmonic mean}$
- If V_1 volume of liquid of density ρ_1 and V_2 volume of liquid of density ρ_2 are mixed, then as: $m = \rho_1 V_1 + \rho_2 V_2$ and $V = V_1 + V_2$ [As $\rho = m / V$]

If $V_1 = V_2 = V$ $\rho = (\rho_1 + \rho_2)/2 = \text{Arithmetic Mean}$

- With rise in temperature due to thermal expansion of a given body, volume will increase while mass will remain unchanged, so density will decrease, i.e.,

$$\frac{\rho}{\rho_0} = \frac{(m/V)}{(m/V_0)} = \frac{V_0}{V} = \frac{V_0}{V_0(1+\gamma\Delta\theta)} \quad [\text{As } V = V_0(1+\gamma\Delta\theta)]$$

or

$$\rho = \frac{\rho_0}{(1+\gamma\Delta\theta)} \approx \rho_0(1-\gamma\Delta\theta)$$

- With increase in pressure due to decrease in volume, density will increase, i.e.,

$$\frac{\rho}{\rho_0} = \frac{(m/V)}{(m/V_0)} = \frac{V_0}{V} \quad [\text{As } \rho = \frac{m}{V}]$$

- By definition of **bulk-modulus**: $B = -V_0 \frac{\Delta p}{\Delta V}$ i.e., $V = V_0 \left[1 - \frac{\Delta p}{B} \right]$

$$\rho = \rho_0 \left(1 - \frac{\Delta p}{B} \right)^{-1} \approx \rho_0 \left(1 + \frac{\Delta p}{B} \right)$$

Specific Weight (γ):

- It is defined as the weight per unit volume.
- Specific weight = $\frac{\text{Weight}}{\text{Volume}} = \frac{m \cdot g}{\text{Volume}} = \rho \cdot g$

Specific Gravity or Relative Density (s):

- It is the ratio of specific weight of fluid to the specific weight of a standard fluid. Standard fluid is water in case of liquid and H_2 or air in case of gas.

$$s = \frac{\gamma}{\gamma_w} = \frac{\rho \cdot g}{\rho_w \cdot g} = \frac{\rho}{\rho_w}$$

Where, γ_w = Specific weight of water, and ρ_w = Density of water specific.

Specific Volume (v):

- Specific volume of liquid is defined as volume per unit mass. It is also defined as the reciprocal of specific density.
- Specific volume = $\frac{V}{m} = \frac{1}{\rho}$

$$\text{Inertial force per unit area} = \frac{dp/dt}{A} = \frac{v(dm/dt)}{A} = \frac{v \cdot A \cdot \rho}{A} = v^2 \rho$$

The other energy term, $mV^2/2$, is the kinetic energy.

- $Storage = \frac{\partial \Phi}{\partial t} = \frac{\partial(m\phi)}{\partial t} = \frac{\partial(\rho \Delta x \Delta y \Delta z \phi)}{\partial t} = \frac{\partial(\rho \phi)}{\partial t} \Delta x \Delta y \Delta z$
- $Inflow = \rho u \phi|_x \Delta y \Delta z + \rho v \phi|_y \Delta x \Delta z + \rho w \phi|_z \Delta y \Delta x$
- $Outflow = \rho u \phi|_{x+\Delta x} \Delta y \Delta z + \rho v \phi|_{y+\Delta y} \Delta x \Delta z + \rho w \phi|_{z+\Delta z} \Delta y \Delta x$
- $Source = S_\phi \Delta x \Delta y \Delta z$
- $\frac{\partial \rho \phi}{\partial t} + \frac{\rho u \phi|_{x+\Delta x} - \rho u \phi|_x}{\Delta x} + \frac{\rho v \phi|_{y+\Delta y} - \rho v \phi|_y}{\Delta y} + \frac{\rho w \phi|_{z+\Delta z} - \rho w \phi|_z}{\Delta z} = S_\phi$
- $\frac{\partial \rho \phi}{\partial t} + \frac{\partial \rho u \phi}{\partial x} + \frac{\partial \rho v \phi}{\partial y} + \frac{\partial \rho w \phi}{\partial z} = S_\phi^*$
- $S_\phi^* = \lim_{\Delta x \Delta y \Delta z \rightarrow 0} S_\phi$

The Mass Balance Equations:

- $\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_i}{\partial x_i} = 0$
- $\frac{\partial \rho}{\partial t} + \frac{\partial \rho u}{\partial x} + \frac{\partial \rho v}{\partial y} + \frac{\partial \rho w}{\partial z} = 0$
- $\frac{\partial \rho}{\partial t} + u_i \frac{\partial \rho}{\partial x_i} + \rho \frac{\partial u_i}{\partial x_i} = 0$
- $\frac{\partial \rho}{\partial t} + \rho \left[\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right] + u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y} + w \frac{\partial \rho}{\partial z} = 0$
- $\frac{D\rho}{Dt} = \frac{\partial \rho}{\partial t} + u \frac{\partial \rho}{\partial x} + v \frac{\partial \rho}{\partial y} + w \frac{\partial \rho}{\partial z} \quad \text{or} \quad \frac{D\rho}{Dt} = \frac{\partial \rho}{\partial t} + u_i \frac{\partial \rho}{\partial x_i}$
- $\frac{D\rho}{Dt} + \rho \left[\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} \right] = 0 \quad \frac{D\rho}{Dt} + \rho \frac{\partial u_i}{\partial x_i} = 0 \quad \frac{D\rho}{Dt} + \rho \Delta = 0$
- $\Delta \equiv \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = 0 \quad \text{or} \quad \Delta \equiv \frac{\partial u_i}{\partial x_i} = 0$

- $\rho \frac{\partial \phi}{\partial t} + \phi \left[\frac{\partial \rho}{\partial t} + \frac{\partial \rho u_i}{\partial x_i} \right] + \rho u_i \frac{\partial \phi}{\partial x_i} = S_\phi$
- $\rho \frac{\partial \phi}{\partial t} + \rho u_i \frac{\partial \phi}{\partial x_i} = S_\phi$

Momentum Balance Equation:

- Net j -direction source term = $\frac{\partial \sigma_{1j}}{\partial x_1} + \frac{\partial \sigma_{2j}}{\partial x_2} + \frac{\partial \sigma_{3j}}{\partial x_3} + \rho B_j = \frac{\partial \sigma_{ij}}{\partial x_i} + \rho B_j$
- $\frac{\partial \rho u_j}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_i} = \frac{\partial \sigma_{ij}}{\partial x_i} + \rho B_j \quad j = 1, \dots, 3$
- For a Newtonian fluid, the stress, σ_{ij} , is given by the following equation:

$$\sigma_{ij} = -P\delta_{ij} + \mu \left[\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right] + \left(\kappa - \frac{2}{3}\mu \right) \Delta \delta_{ij}$$

- $\frac{\partial \rho u_j}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_i} = \frac{\partial}{\partial x_i} \left[-P\delta_{ij} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) + \left(\kappa - \frac{2}{3}\mu \right) \Delta \delta_{ij} \right] + \rho B_j \quad j = 1, \dots, 3$
- $\frac{\partial \rho u_j}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_i} = -\frac{\partial P}{\partial x_j} + \frac{\partial}{\partial x_i} \left[\mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \right] + \frac{\partial}{\partial x_j} \left[\left(\kappa - \frac{2}{3}\mu \right) \Delta \right] + \rho B_j \quad j = 1, \dots, 3$
- $\frac{\partial \rho u}{\partial t} + \frac{\partial \rho u u}{\partial x} + \frac{\partial \rho v u}{\partial y} + \frac{\partial \rho w u}{\partial z} = \rho B_x$
- $-\frac{\partial P}{\partial x} + 2\frac{\partial}{\partial x} \mu \left(\frac{\partial u}{\partial x} \right) + \frac{\partial}{\partial y} \left[\mu \left(\frac{\partial v}{\partial x} + \frac{\partial u}{\partial y} \right) \right] + \frac{\partial}{\partial z} \left[\mu \left(\frac{\partial w}{\partial x} + \frac{\partial u}{\partial z} \right) \right] + \frac{\partial}{\partial x} \left[\left(\kappa - \frac{2}{3}\mu \right) \Delta \right]$

Energy Balance Equation:

- This directional heat flux is given the symbol q_i : $q_i = -k \frac{\partial T}{\partial x_i}$
- $\frac{\text{Net } x\text{Direction heat}}{\text{Unit Volume}} = -\frac{q_x|_{x+\Delta x} - q_x|_x}{\Delta x \Delta y \Delta z} \Delta y \Delta z = -\frac{q_x|_{x+\Delta x} - q_x|_x}{\Delta x}$
- $\lim_{\Delta x \rightarrow 0} \frac{\text{Net } x\text{Direction heat source}}{\text{Unit Volume}} = -\frac{\partial q_x}{\partial x}$

- $Heat\ Rate = -\frac{\partial q_x}{\partial x} - \frac{\partial q_y}{\partial y} - \frac{\partial q_z}{\partial z} = -\frac{\partial q_i}{\partial x_i}$
- $Body\text{-}force\ work\ rate = \rho(uB_x + vB_y + wB_z) = \rho u_i B_i$

- The work term on each face is given by the following equation:

$$y\text{-face surface force work} = (u\sigma_{yx} + v\sigma_{yy} + w\sigma_{yz})\Delta x \Delta z = u_i\sigma_{iy} \Delta x \Delta z$$

- $Net\ y\text{Face Surface Force Work} = \frac{\partial(u\sigma_{yx} + v\sigma_{yy} + w\sigma_{yz})}{\partial y} = \frac{\partial u_i\sigma_{ji}}{\partial y}$
- $Net\ Surface\ Force\ Work = \frac{\partial u_i\sigma_{xi}}{\partial x} + \frac{\partial u_i\sigma_{yi}}{\partial y} + \frac{\partial u_i\sigma_{zi}}{\partial z} = \frac{\partial u_i\sigma_{ji}}{\partial x_j}$
- Energy balance equation:

$$\frac{\partial \rho(e + \mathbf{V}^2/2)}{\partial t} + \frac{\partial \rho u_i(e + \mathbf{V}^2/2)}{\partial x_i} = -\frac{\partial q_i}{\partial x_i} + \frac{\partial u_i\sigma_{ji}}{\partial x_j} + \rho u_i B_i$$

Substitutions for Stresses and Heat Flux:

Using only the Fourier Law heat transfer, the source term involving the heat flux in the energy balance equation:

- $-\frac{\partial q_i}{\partial x_i} = -\frac{\partial}{\partial x_i} \left(-k \frac{\partial T}{\partial x_i} \right) = \frac{\partial}{\partial x_i} k \frac{\partial T}{\partial x_i} = \frac{\partial}{\partial x} k \frac{\partial T}{\partial x} + \frac{\partial}{\partial y} k \frac{\partial T}{\partial y} + \frac{\partial}{\partial z} k \frac{\partial T}{\partial z}$
- $\frac{\partial \rho e}{\partial t} + \frac{\partial \rho u_i e}{\partial x_i} = \frac{\partial}{\partial x_i} k \frac{\partial T}{\partial x_i} + \left[-P\delta_{ij} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) + \left(\kappa - \frac{2}{3}\mu \right) \Delta \delta_{ij} \right] \frac{\partial u_i}{\partial x_j}$
- $\delta_{ij} \frac{\partial u_i}{\partial x_j} = \frac{\partial u_j}{\partial x_j} = \Delta$
- $\frac{\partial \rho e}{\partial t} + \frac{\partial \rho u_i e}{\partial x_i} = \frac{\partial}{\partial x_i} k \frac{\partial T}{\partial x_i} - P\Delta + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \frac{\partial u_i}{\partial x_j} + \left(\kappa - \frac{2}{3}\mu \right) \Delta^2$

Dissipation to avoid confusion with the general quantity in a balance equation:

- $\Phi_D = \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) \frac{\partial u_i}{\partial x_j} + \left(\kappa - \frac{2}{3}\mu \right) \Delta^2$

- $\frac{\partial \rho e}{\partial t} + \frac{\partial \rho u_i e}{\partial x_i} = \frac{\partial}{\partial x_i} k \frac{\partial T}{\partial x_i} - P \Delta + \Phi_D$

The temperature gradient in the Fourier law conduction term may also be written as a gradient of enthalpy or internal energy:

- $\frac{\partial T}{\partial x_i} = \frac{1}{c_v} \frac{\partial e}{\partial x_i} + \frac{1}{c_v} \left[\frac{T \beta_p}{\kappa_T} - P \right] \frac{1}{\rho^2} \frac{\partial \rho}{\partial x_i}$

- $\frac{\partial T}{\partial x_i} = \frac{1}{c_p} \frac{\partial h}{\partial x_i} - \frac{1 - T \beta_p}{\rho c_p} \frac{\partial P}{\partial x_i}$

- $\frac{\partial \rho e}{\partial t} + \frac{\partial \rho u_i e}{\partial x_i} = \frac{\partial}{\partial x_i} k \frac{\partial e}{\partial x_i} - P \Delta + \Phi_D + \frac{\partial}{\partial x_i} \frac{1}{c_v} \left[\frac{T \beta_p}{\kappa_T} - P \right] \frac{1}{\rho^2} \frac{\partial \rho}{\partial x_i}$

- $\frac{\partial \rho h}{\partial t} + \frac{\partial \rho u_i h}{\partial x_i} = \frac{\partial}{\partial x_i} k \frac{\partial h}{\partial x_i} + \Phi_D + \frac{\partial}{\partial x_i} \left[\frac{1 - T \beta_p}{\rho c_p} \right] \frac{\partial P}{\partial x_i} + \frac{DP}{Dt}$

- $c_p \left[\frac{\partial \rho T}{\partial t} + \frac{\partial \rho u_i T}{\partial x_i} \right] = \frac{\partial}{\partial x_i} k \frac{\partial T}{\partial x_i} + \Phi_D + \beta_p T \frac{DP}{Dt}$

General Balance Equations			
ϕ	c	$\Gamma^{(\phi)}$	$S^{(\phi)}$
1	1	0	0
$u = u_x = u_1$	1	μ	$-\frac{\partial P}{\partial x} + \frac{\partial}{\partial x} \mu \frac{\partial u}{\partial x} + \frac{\partial}{\partial y} \mu \frac{\partial v}{\partial x} + \frac{\partial}{\partial z} \mu \frac{\partial w}{\partial x} + \frac{\partial}{\partial x} \left[\left(\kappa - \frac{2}{3} \mu \right) \Delta \right] + \rho B_x$
$v = u_y = u_2$	1	μ	$-\frac{\partial P}{\partial y} + \frac{\partial}{\partial x} \mu \frac{\partial u}{\partial y} + \frac{\partial}{\partial y} \mu \frac{\partial v}{\partial y} + \frac{\partial}{\partial z} \mu \frac{\partial w}{\partial y} + \frac{\partial}{\partial y} \left[\left(\kappa - \frac{2}{3} \mu \right) \Delta \right] + \rho B_y$
$w = u_z = u_3$	1	μ	$-\frac{\partial P}{\partial z} + \frac{\partial}{\partial x} \mu \frac{\partial u}{\partial z} + \frac{\partial}{\partial y} \mu \frac{\partial v}{\partial z} + \frac{\partial}{\partial z} \mu \frac{\partial w}{\partial z} + \frac{\partial}{\partial z} \left[\left(\kappa - \frac{2}{3} \mu \right) \Delta \right] + \rho B_z$
e	1	k/c_v	$-P\Delta + \Phi_D + \frac{\partial}{\partial x_i} \frac{1}{c_v} \left[\frac{T\beta_p}{\kappa_T} - P \right] \frac{1}{\rho^2} \frac{\partial \rho}{\partial x_i}$
h	1	k/c_p	$\Phi_D + \frac{\partial}{\partial x_i} \left[\frac{1 - T\beta_p}{\rho c_p} \right] \frac{\partial P}{\partial x_i} + \frac{DP}{Dt}$
T	c_p	k	$\Phi_D + \beta_p T \frac{DP}{Dt}$
T	c_v	k	$\Phi_D + \frac{T\beta_p}{\kappa_T} \Delta$
$W^{(K)}$	1	$\rho D_{K,Mix}$	$\Gamma^{(K)}$

Momentum equation:

$$\bullet \quad \frac{\partial \rho u_j}{\partial t} + \frac{\partial \rho u_i u_j}{\partial x_i} = \frac{\partial}{\partial x_i} \mu \frac{\partial u_j}{\partial x_i} + S^{(j)} = -\frac{\partial P}{\partial x_i} + \frac{\partial}{\partial x_i} \mu \frac{\partial u_j}{\partial x_i} + S^{*(j)}$$

General Momentum Equations			
ϕ	c	$\Gamma^{(\phi)}$	$S^{*(\phi)}$
1	1	0	0
$u = u_x = u_1$	1	μ	$\frac{\partial}{\partial x} \mu \frac{\partial u}{\partial x} + \frac{\partial}{\partial y} \mu \frac{\partial v}{\partial x} + \frac{\partial}{\partial z} \mu \frac{\partial w}{\partial x} + \frac{\partial}{\partial x} \left[\left(\kappa - \frac{2}{3} \mu \right) \Delta \right] + \rho B_x$
$v = u_y = u_2$	1	μ	$+\frac{\partial}{\partial x} \mu \frac{\partial u}{\partial y} + \frac{\partial}{\partial y} \mu \frac{\partial v}{\partial y} + \frac{\partial}{\partial z} \mu \frac{\partial w}{\partial y} + \frac{\partial}{\partial y} \left[\left(\kappa - \frac{2}{3} \mu \right) \Delta \right] + \rho B_y$
$w = u_z = u_3$	1	μ	$\frac{\partial}{\partial x} \mu \frac{\partial u}{\partial z} + \frac{\partial}{\partial y} \mu \frac{\partial v}{\partial z} + \frac{\partial}{\partial z} \mu \frac{\partial w}{\partial z} + \frac{\partial}{\partial z} \left[\left(\kappa - \frac{2}{3} \mu \right) \Delta \right] + \rho B_z$

Bernoulli's Equation:

This equation has four variables: velocity (v), elevation (z), pressure (p), and density (ρ). It also has a constant (g), which is the acceleration due to gravity. Here is Bernoulli's equation:

- $\frac{v^2}{2} + gz + \frac{p}{\rho} = \text{constant}$
- $P + \rho gh + \frac{1}{2} \rho v^2 = \text{constant}$
- $\frac{P}{\rho g} + h + \frac{v^2}{2g} = \text{constant}$; $\frac{P}{\rho g}$ is called pressure head, h is called gravitational head and $\frac{v^2}{2g}$ is called velocity head.

Factors that influence head loss due to friction are:

- Length of the pipe (l)
- Effective diameter of the pipe (D_h)
- Velocity of the water in the pipe (v)
- Acceleration of gravity (g)
- Friction from the surface roughness of the pipe (λ)
- The head loss due to the pipe is estimated by the following equation:

$$h_{f,major} = \lambda \frac{lv^2}{2D_h g}$$

- To estimate the total head loss in a piping system, one adds the head loss from the fittings and the pipe:

$$h_{f,total} = \sum h_{f,minor} + \sum h_{f,major}$$

- Note that the summation symbol (\sum) means to add up the losses from all the different sources. A less compact-way to write this equation is:

$$h_{f,total} = h_{f,minor1} + h_{f,minor2} + h_{f,minor3} + \dots \\ h_{f,major1} + h_{f,major2} + h_{f,major3} + \dots$$

Combining Bernoulli's Equation With Head Loss:

$$\frac{p_1}{\gamma} + \frac{v_1^2}{2g} + z_1 = \frac{p_2}{\gamma} + \frac{v_2^2}{2g} + z_2 + h_{f,total}$$

Relation between coefficient of viscosity and temperature:

$$\text{Andrade formula } \eta = \frac{A e^{C\rho/T}}{\rho^{-1/3}}$$

Stoke's Law: $F = 6\pi\eta rv$

Terminal Velocity:

- Weight of the body (W) = $mg = (\text{volume} \times \text{density}) \times g = \frac{4}{3}\pi r^3 \rho g$
- Upward thrust (T) = weight of the fluid displaced
$$= (\text{volume} \times \text{density}) \text{ of the fluid} \times g = \frac{4}{3}\pi r^3 \sigma g$$
- Viscous force (F) = $6\pi\eta rv$
- When the body attains terminal velocity the net force acting on the body is zero.
- $W - T - F = 0$ or $F = W - T$
- $$6\pi\eta rv = \frac{4}{3}\pi r^3 \rho g - \frac{4}{3}\pi r^3 \sigma g = \frac{4}{3}\pi r^3 (\rho - \sigma) g$$
- Terminal velocity $v = \frac{2}{9} \frac{r^2 (\rho - \sigma) g}{\eta}$
- Terminal velocity depend on the radius of the sphere so if radius is made n - fold, terminal velocity will become n^2 times.
- Greater the density of solid greater will be the terminal velocity
- Greater the density and viscosity of the fluid lesser will be the terminal velocity.
- If $\rho > \sigma$ then terminal velocity will be positive and hence the spherical body will attain constant velocity in downward direction.
- If $\rho < \sigma$ then terminal velocity will be negative and hence the spherical body will attain constant velocity in upward direction.

Poiseuille's Formula:

- $V \propto \frac{P r^4}{\eta l}$ or $V = \frac{K P r^4}{\eta l}$
- $V = \frac{\pi P r^4}{8 \eta l}$; where $K = \frac{\pi}{8}$ is the constant of proportionality.

Buoyant Force:

- Buoyant force = Weight of fluid displaced by body

- Buoyant force on cylinder = Weight of fluid displaced by cylinder
- V_{sub} = Value of immersed part of solid
- $F_B = p_{water} \times g \times \text{Volume of fluid displaced}$
- $F_B = p_{water} \times g \times \text{Volume of cylinder immersed inside the water}$
- $F_B = mg$
- $F_B = p_w g \frac{\pi}{4} d^2$ ($\because w = mg = pVg$)
- $V_{sub} p_l g = V_s p_s g$
- $p_w g \frac{\pi}{4} d^2 x = p_{cylinder} g \frac{\pi}{4} d^2 h$
- $p_w x = p_{cylinder} h$

Relation between B, G and M:

- $GM = \frac{I}{V} - BG$; where I = Least moment of inertia of plane of body at water surface, G = Centre of gravity, B = Centre of buoyancy, and M = Metacentre.
- $I = \min(I_{xx}, I_{yy})$, $I_{xx} = \frac{bd^3}{12}$, $I_{yy} = \frac{bd^3}{12}$
- $V = bdx$

Energy Equations:

- $F_{net} = F_g + F_p + F_v + F_c + F_t$; where Gravity force F_g , Pressure force F_p , Viscous force F_v , Compressibility force F_c , and Turbulent force F_t
- If fluid is incompressible, then $F_c = 0$
 $\therefore F_{net} = F_g + F_p + F_v + F_t$; This is known as **Reynolds equation** of motion.
- If fluid is incompressible and turbulence is negligible, then
 $F_c = 0, F_t = 0 \therefore F_{net} = F_g + F_p + F_v$; This equation is called as **Navier-Stokes equation**.
- If fluid flow is considered ideal then, viscous effect will also be negligible. Then
 $F_{net} = F_g + F_p$; This equation is known as **Euler's equation**.
- Euler's equation can be written as: $\frac{dp}{\rho} + g dz + v dv = 0$

Dimensional analysis:

Quantity	Symbol	Dimensions
Mass	m	M
Length	l	L
Time	t	T
Temperature	T	θ
Velocity	u	LT^{-1}
Acceleration	a	LT^{-2}
Momentum/Impulse	mv	MLT^{-1}
Force	F	MLT^{-2}
Energy - Work	W	ML^2T^{-2}
Power	P	ML^2T^{-3}
Moment of Force	M	ML^2T^{-2}
Angular momentum	-	ML^2T^{-1}
Angle	η	$M^0L^0T^0$
Angular Velocity	ω	T^{-1}
Angular acceleration	α	T^{-2}
Area	A	L^2
Volume	V	L^3
First Moment of Area	Ar	L^3
Second Moment of Area	I	L^4
Density	ρ	ML^{-3}
Specific heat- Constant Pressure	C_p	$L^2T^{-2}\theta^{-1}$
Elastic Modulus	E	$ML^{-1}T^{-2}$
Flexural Rigidity	EI	ML^3T^{-2}
Shear Modulus	G	$ML^{-1}T^{-2}$
Torsional rigidity	GJ	ML^3T^{-2}
Stiffness	k	MT^{-2}

Angular stiffness	T/η	$ML^{-2}T^{-2}$
Flexibility	$1/k$	$M^{-1}T^2$
Vorticity	-	T^{-1}
Circulation	-	L^2T^{-1}
Viscosity	μ	$ML^{-1}T^{-1}$
Kinematic Viscosity	τ	L^2T^{-1}
Diffusivity	-	L^2T^{-1}
Friction coefficient	f/μ	$M^0L^0T^0$
Restitution coefficient		$M^0L^0T^0$
Specific heat- Constant volume	C_v	$L^2T^{-2}\theta^{-1}$

Boundary layer:

- **Reynolds number** $= \frac{\rho v \cdot x}{\mu} (Re)_x = \frac{v \cdot x}{\nu}$
- **Displacement Thickness** (δ^*): $\delta^* = \int_0^\delta \left(1 - \frac{u}{U}\right) dy$
- **Momentum Thickness** (θ): $\theta = \int_0^\delta \frac{u}{U} \left(1 - \frac{u}{U}\right) dy$
- **Energy Thickness** (δ^{**}): $\delta^{**} = \int_0^\delta \frac{u}{U} \left(1 - \frac{u^2}{U^2}\right) dy$
- **Boundary Conditions for the Velocity Profile:** Boundary conditions are as
 - (a) At $y=0, u=0, \frac{du}{dy} \neq 0$; (b) At $y=\delta, u=U, \frac{du}{dy} = 0$

Turbulent flow:

- **Shear stress in turbulent flow:** $\tau = \tau_v + \tau_t = \mu \frac{d\bar{u}}{dy} + \eta \frac{d\bar{u}}{dy}$
- **Turbulent shear stress by Reynold:** $\tau = \rho u'v'$
- **Shear stress in turbulent flow due to Prndtle :** $\tau = \rho l^2 \left(\frac{du}{dy}\right)^2$