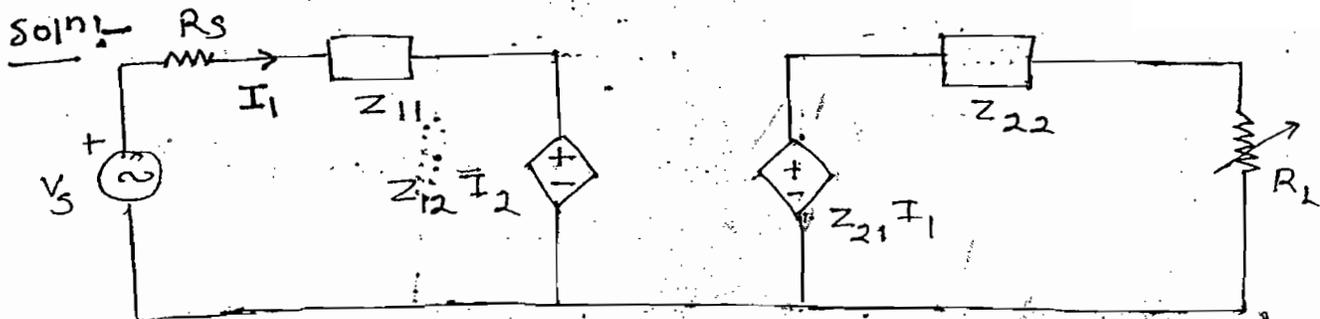
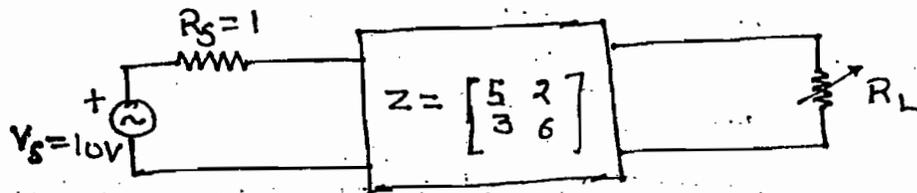


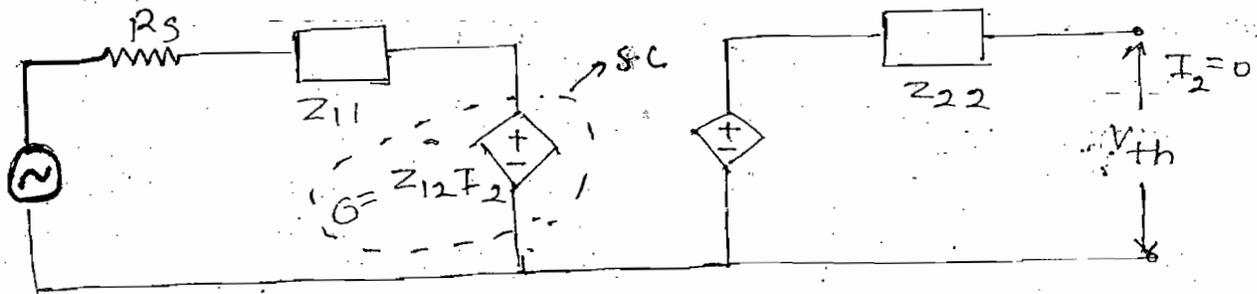
## Lecture - 12

ques:- Find max. power dissipation in load resistor



Case-(1):-  $V_{th}$

Disconnect load resistor



$$I_1 = \frac{V_s}{R_s + Z_{11}} \quad \text{--- (i)}$$

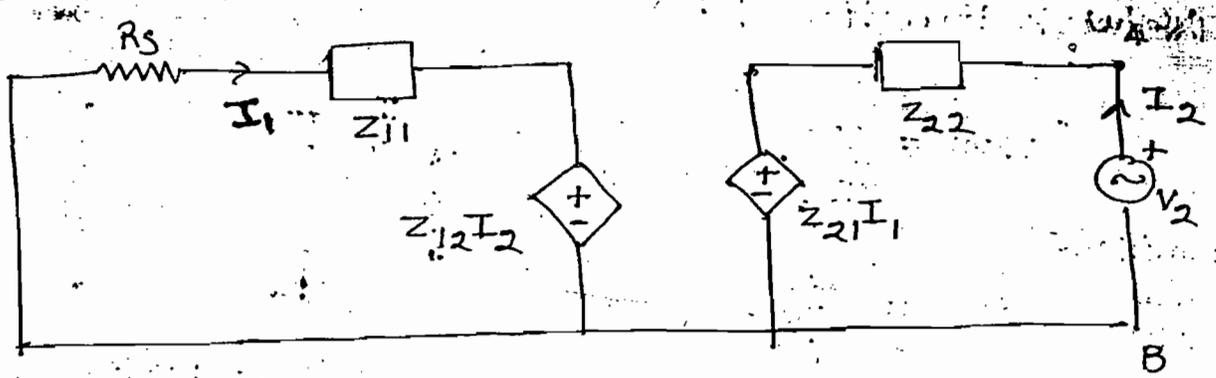
$$V_{th} = z_{21} I_1 \quad \text{--- (ii)}$$

Substitute eq-(i) in eq-(ii)

$$V_{th} = z_{21} \frac{V_s}{R_s + Z_{11}}$$

$$V_{th} = \frac{3 \times 10}{1 + 5} = 5$$

Case-(ii) ( $R_{th}$ ): —



$$Z_{th} = \frac{V_2}{I_2}$$

$$I_2 = \frac{V_2 - Z_{21}I_1}{Z_{22}}$$

$$I_1 = -\frac{Z_{12}I_2}{R_s + Z_{11}} \quad \text{--- (i)}$$

$$I_2 Z_{22} = V_2 - Z_{21}I_1$$

$$V_2 = I_2 Z_{22} + Z_{21}I_1 \quad \text{--- (ii)}$$

Substitute eq-(i) in eq-(ii).

$$V_2 = I_2 Z_{22} - \frac{Z_{12} Z_{21} I_2}{R_s + Z_{11}}$$

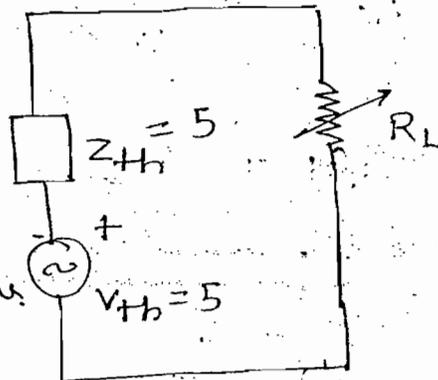
$$Z_{th} = \frac{V_2}{I_2} = Z_{22} - \frac{Z_{12} Z_{21}}{R_s + Z_{11}}$$

$$= 6 - \frac{2 \times 3}{1 + 5} \Rightarrow Z_{th} = 5$$

$$R_f = R_{th} = 5 \Omega$$

$$P_{max} = \frac{V_{th}^2}{4R_L}$$

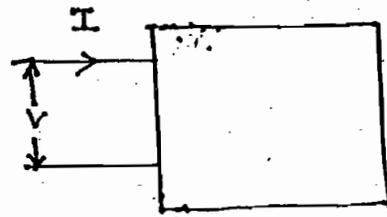
$$= \frac{25}{4 \times 5} = 1.25 \text{ W, Ans.}$$



# Network Functions :-

Immittance  
Common Name

$$\begin{cases} Z(s) = \frac{V(s)}{I(s)} \\ Y(s) = \frac{I(s)}{V(s)} \end{cases}$$



Single Port

## Two Port :-



Driving Point I/p impedance

(I)  $Z_{11}(s) = \frac{V_1(s)}{I_1(s)}$        $Z_{22}(s) = \frac{V_2(s)}{I_2(s)}$

(II)  $Y_{11}(s) = \frac{I_1(s)}{V_1(s)}$        $Y_{22}(s) = \frac{I_2(s)}{V_2(s)}$  → Driving pt admittance function

(III)  $Z_{12}(s) = \frac{V_1(s)}{I_2(s)}$        $Z_{21}(s) = \frac{V_2(s)}{I_1(s)}$  → Transfer impedance ratio

(IV)  $Y_{12}(s) = \frac{I_1(s)}{V_2(s)}$        $Y_{21}(s) = \frac{I_2(s)}{V_1(s)}$  → Transfer admittance ratio

(V)  $G_{12} = \frac{V_1(s)}{V_2(s)}$        $G_{21} = \frac{V_2(s)}{V_1(s)}$  → Transfer voltage ratio

(VI)  $\alpha_{12} = \frac{I_1(s)}{I_2(s)}$        $\alpha_{21} = \frac{I_2(s)}{I_1(s)}$  → Transfer current ratio

→ N/w parameter is calculated at pre-defined condition (either o.c or s.c)

eg:-  $Z_{11} = \frac{V_1}{I_1} \Big|_{I_2=0 \rightarrow \text{o.c.}}$        $Y_{11} = \frac{I_1}{V_1} \Big|_{V_2=0 \rightarrow \text{s.c.}}$

→ To find the N/w function, no pre-defined condition is required

→ To represent the N/w simultaneously four parameters are required

eg:- To develop T-N/w  $Z_{11}, Z_{12}, Z_{21}$  &  $Z_{22}$  are required.

→ By using only one N/w function it is possible to represent the N/w.

### Network Synthesis:-

→ In the N/w analysis for a given N/w it is possible to find either voltage response or current response or impedance function or admittance function

→ In a N/w synthesis, for a given function N/w is designed (It is reverse procedure of N/w analysis)

→ In a N/w synthesis it is possible to design the N/w for the following functions

(I) Single port →  $\left. \begin{array}{l} 1. Z(s) \\ 2. Y(s) \end{array} \right\} \rightarrow \text{Driving Point Impedance}$

(II) Two port →  $\left. \begin{array}{l} 1. Z_{11}(s), Z_{22}(s), Y_{11}(s), Y_{22}(s) \\ 2. Z_{12}(s), Z_{21}(s), Y_{12}(s), Y_{21}(s), G_{12}, G_{21}, \alpha_{12}, \alpha_{21} \end{array} \right\} \rightarrow \text{Transfer function}$

→ In the N/w synthesis for given function it is possible to design the following N/w

(I) Series                      (II) Parallel                      (III) Ladder

(I) Series  $\rightarrow$  Foster - I form

Partial fraction  
of expansion

(II) Parallel  $\rightarrow$  Foster - II form

(III) Ladder

Cauer - I form

Cauer - II form

Continued fraction  
of expansion

### Necessary Condition to design a N/W:-

(I)  $F(s)$  should be <sup>positive</sup> ~~primary~~ real function (PRF)

$$R \geq 0$$

$$L \geq 0$$

$$C \geq 0$$

Positive Real

(II) If  $F(s)$  is PRF then  $\frac{1}{F(s)}$  also PRF

(III) If  $F_1(s)$  and  $F_2(s)$  are PRF then

$$F(s) = F_1(s) + F_2(s) \text{ are always PRF}$$

(IV) All the poles of the function should be present in the left half of the plane

(V) Imaginary poles and zeroes should be conjugate pairs

(VI) In the partial fraction of expansion residue should be positive real

(VII) Numerator and denominator polynomials should satisfy Hurwitz.

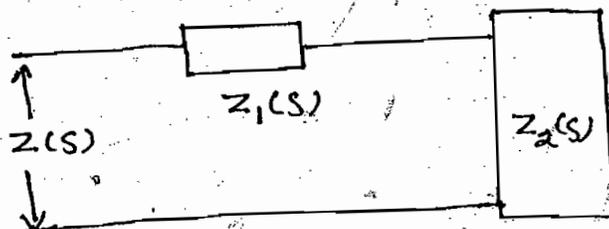
(VIII) The highest power of Numerator and denominator of polynomial should be differ at <sup>at most</sup> by unity. This condition prohibits multiple pole and zero at infinity.

9 → The lowest power of Numerator and Denominator should be differ<sup>by</sup> at most unity. This conditions prohibits multiple poles and zeroes at origin.

10 → Total No. of poles of a function should be equal to total no. of zeroes.

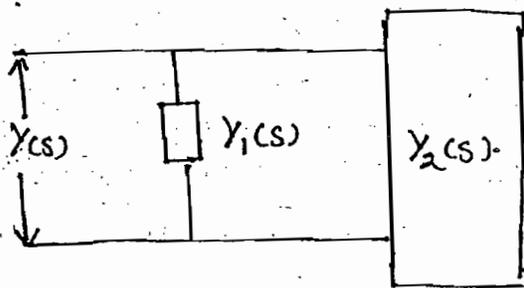
$$Z(s) = Z_1(s) + Z_2(s)$$

$$\Rightarrow Z_2(s) = Z(s) - Z_1(s)$$



$$Y(s) = Y_1(s) + Y_2(s)$$

$$\Rightarrow Y_2(s) = Y(s) - Y_1(s)$$



Removal of Pole at  $\infty$  :-

$$Z(s) = \frac{b_{n+1}s^{n+1} + b_n s^n + \dots + b_0}{a_n s^n + a_{n-1} s^{n-1} + \dots + a_0}$$

$$\cdot \frac{a_n s^n + a_{n-1} s^{n-1} + \dots + a_0}{a_n s^n + a_{n-1} s^{n-1} + \dots + a_0}$$

Numerator Power > Denominator power

→ pole exist at  $\infty$ .

By long division

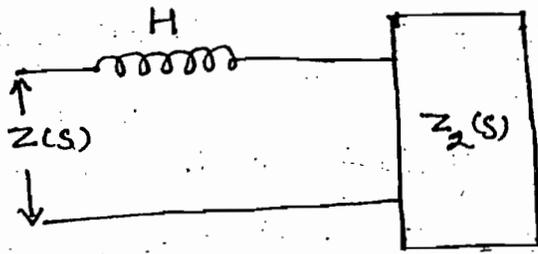
$$Z(s) = \frac{b_{n+1} s^{n+1}}{a_n s^n} + Z_2(s)$$

$$\left( H = \frac{b_{n+1}}{a_n} \right)$$

$$Z(s) = Hs + Z_2(s)$$

$$X_L = Ls$$

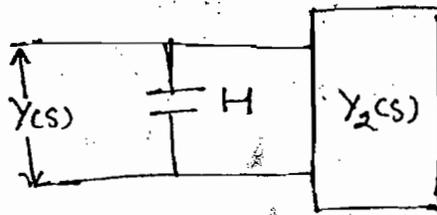
$$Z_2(s) = Z(s) - Hs$$



$$Y(s) = \frac{Hs}{s} + Y_2(s)$$

$$B_C = SC$$

$$Y_2(s) = Y(s) - \frac{Hs}{s}$$



Removal of pole at origin:-

$$Z(s) = \frac{b_0 + \dots + b_{n-1}s^{n-1} + b_n s^n}{s(a_0 + \dots + a_{n-1}s^{n-1} + a_n s^n)}$$

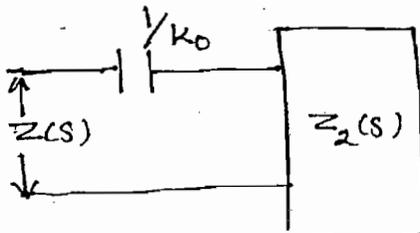
By long division

$$Z(s) = \frac{b_0}{s a_0} + Z_2(s) \quad \left( k_0 = \frac{b_0}{a_0} \right)$$

$$Z(s) = \frac{k_0}{s} + Z_2(s)$$

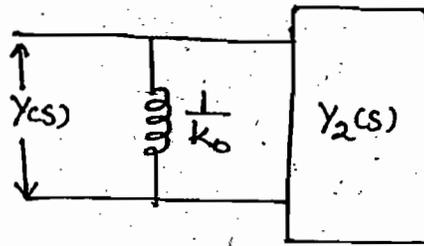
$$\Rightarrow Z_2(s) = Z(s) - \frac{k_0}{s}$$

$$X_C = \frac{1}{Cs}$$



$$Y(s) = \frac{k_0}{s} + Y_2(s)$$

$$Y_2(s) = Y(s) - \frac{k_0}{s}$$



Removal of conjugate Pair of Poles: —

$$Z(s) = Z_1(s) + Z_2(s)$$

$$Z_2(s) = Z(s) - Z_1(s)$$

$$Z_1(s) \rightarrow \text{Poles} \Rightarrow \pm j\omega$$

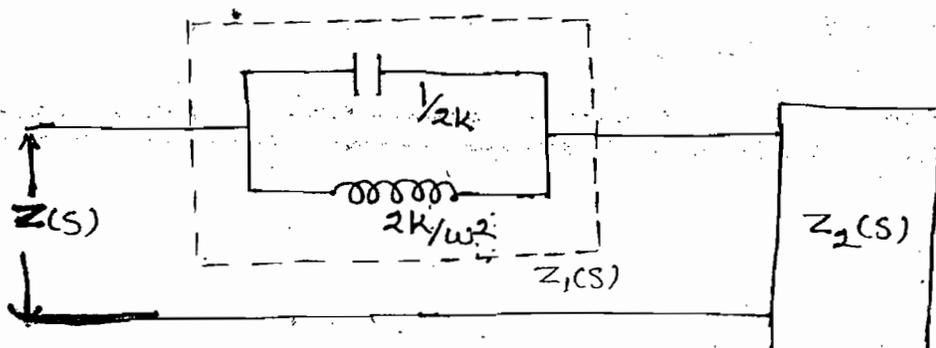
$$Z_1(s) = \frac{k_1}{s+j\omega} + \frac{k_2}{s-j\omega} \quad (k_1 = k_2 = k)$$

$$Z_1(s) = \frac{k}{s+j\omega} + \frac{k}{s-j\omega}$$

$$Z_1(s) = \frac{2ks}{s^2 + \omega^2}$$

$$Z_1(s) = \frac{1}{\frac{s^2}{2ks} + \frac{\omega^2}{2ks}} = \frac{1}{Y_a + Y_b}$$

$B_c = sC$        $B_h = \frac{1}{Ls}$

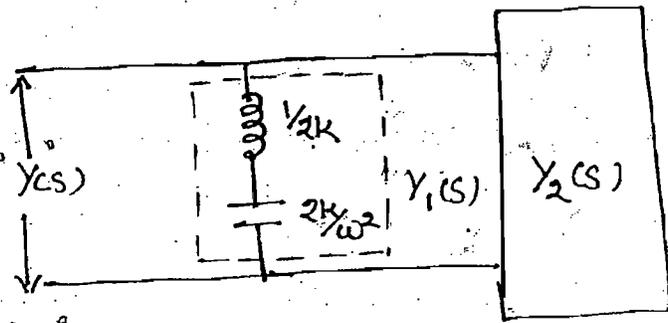


$$Y(s) = Y_1(s) + Y_2(s)$$

$$Y_2(s) = Y(s) - Y_1(s)$$

$$Y_1(s) = \frac{1}{\frac{s}{2k} + \frac{\omega^2}{2ks}} = \frac{1}{z_a + z_b}$$

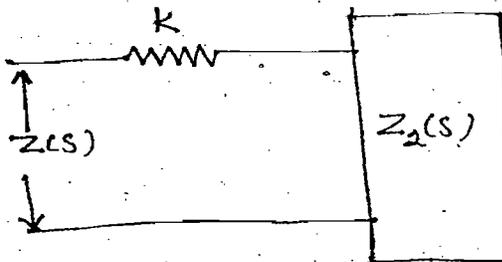
$X_L = s$        $X_C = \frac{1}{cs}$



Removal of constant:

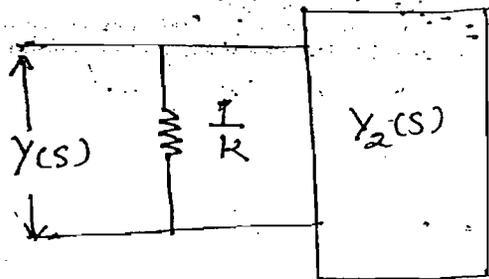
$$Z(s) = k + Z_2(s)$$

$$Z_2(s) = Z(s) - k$$



$$Y(s) = k + \frac{1}{Z}(s)$$

$$Y_2(s) = Y(s) - k$$



LC N/ω Foster - I form :- (Series)

$$Z(s) = \frac{k_0}{s} + \sum_{i=1}^n \frac{2k_i s}{s^2 + \omega_i^2} + Hs$$

$X_C = \frac{1}{Cs}$   $(X_L = Ls)$

